

Pick an instrument for your task. Want one that can diagnose and calibrate itself? Or the one that combines several functions? How about the new breed of battery

powered types that match power efficiency with portability? Do you require an instrument that won't hurt other equipment or you. For more details, see p. 50.

gent metrological microprocessor-based function generators

programmable pulse measurements rugged

DVMs portable function generators

safe intelligent

INSTRUMENTS

'76

scopes impedance measurements modular calculator-based safe battery powered logic analyzers calculator-based

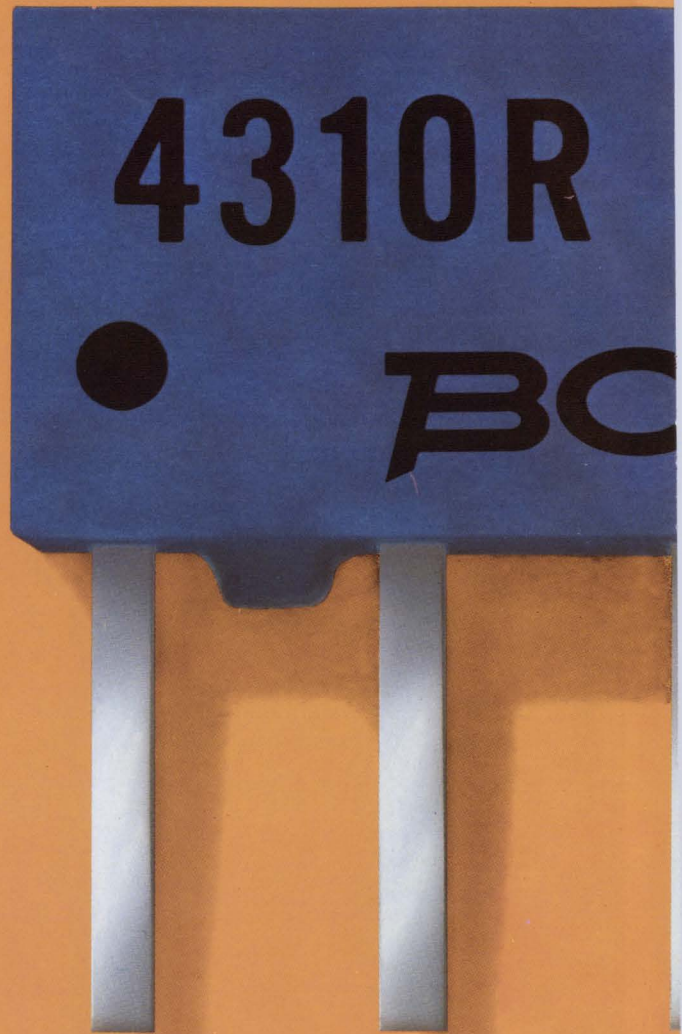
intelligent logic analyzers metrological

interface bus modular computer-based

programmable synergistic scopes impedance measurements microprocessor-based interface bus computer-based scopes impedance measurements modular calculator-based safe battery powered logic analyzers calculator-based metrological intelligent logic analyzers metrological interface bus modular computer-based

Before You Read This Issue . . .
RENEW YOUR SUBSCRIPTION
 Turn to card inside cover

the **DIP** **HIGH** **SIP**



Now in the only full line of super low profile SIP Resistor Networks.

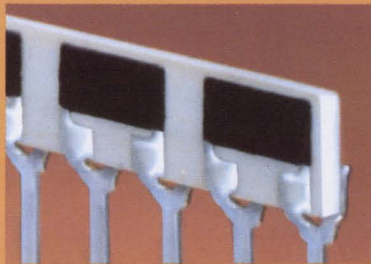
If you haven't designed in Single In-line Package resistor networks because of their high profile, take another look. THE HEIGHT ON BOURNS SIPs IS ONLY .190 INCH! And that's standard for all 6, 8 and 10 pin configurations with:

- 5, 7 or 9 resistors and 1 common pin
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- 12 resistors, dual terminator (8 pin)

Now you can fit the same number of resistors into less area and yet maintain close P.C. Board spacing. Something you can't do when using other SIP networks with .250 or .350 inch high profiles.

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Why specify other than Bourns?

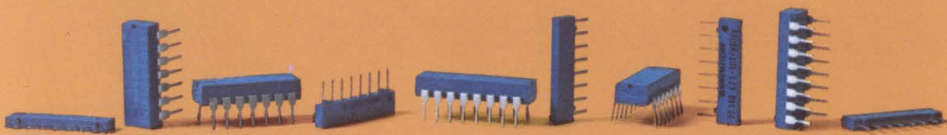


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WATCH THIS SPACE FOR DETAILS

WAVETEK MODEL 172
PROGRAMMABLE SIGNAL SOURCE

UNIT

RCL

AMPL
SPEC

LOAD



CIRCLE NUMBER 2

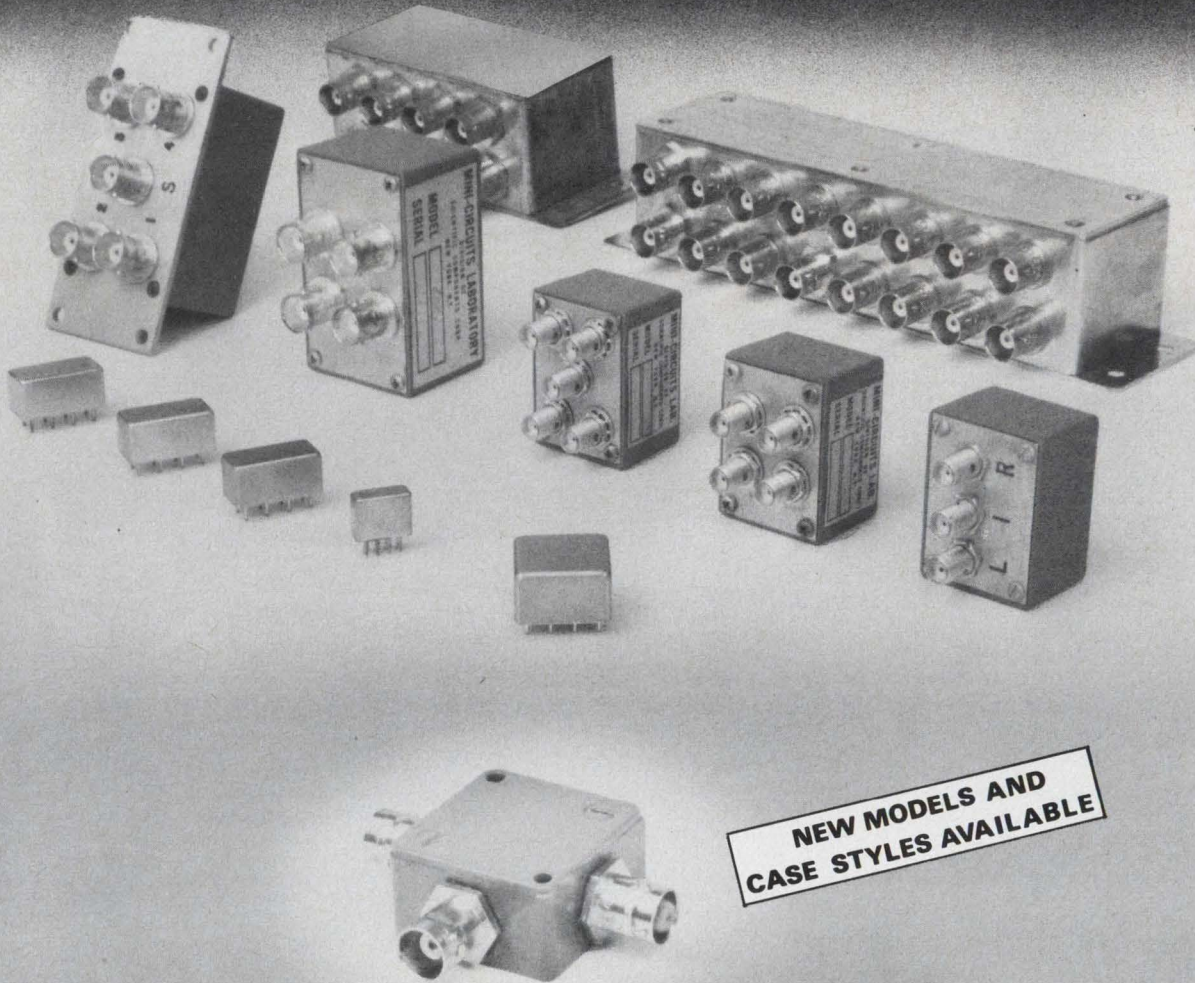
This is the face of our new Model 172 programmable signal source.

It gives you 7 function generator waveforms over a frequency range of 0.0001 Hz to 13 MHz. It's GPIB compatible, has a microprocessor-controlled interface, plus a 5½ -digit synthesizer option.

We'll give you more details in the next installment. Meanwhile, circle the inquiry card or contact us direct. Wavetek, P.O. Box 651, San Diego, CA 92112. Phone (714) 279-2200. Or TWX 910-335-2007.

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Model No.	Freq. range (MHz)	Isol. between outputs (dB) typ.	Insertion loss (dB) (typical)	Unbalance ϕ (deg)	Amp. (dB)	Price (Quantity)
TWO-WAY 0°						
PSC 2-1	0.1-400	25	0.4 above 3dB split	1	0.1	\$ 9.95 (6-49)
ZSC 2-1						\$24.95 (4-24)
ZMSC 2-1						\$34.95 (4-24)
PSC 2-2	0.002-60	40	0.3 above 3dB split	1	0.1	\$19.95 (6-49)
ZSC 2-2						\$34.95 (4-24)
ZMSC 2-2						\$44.95 (4-24)
ZFSC 2-2	10-1000	25	0.6 above 3dB split	0.8	0.08	\$39.95 (4-24)
PSC 2-1W	1-650	25	0.5 above 3dB split	3	0.20	\$14.95 (6-49)
ZSC 2-1W						\$29.95 (4-24)
ZMSC 2-1W						\$39.95 (4-24)
PSC 2-1-75*	0.25-300	25	0.4 above 3dB split	1	0.05	\$11.95 (6-49)
MSC 2-1	0.1-450	30	0.4 above 3dB split	1	0.1	\$16.95 (6-24)
PSC 2375	55-85	35	0.3 above 3dB split	0.05	0.05	\$19.95 (6-49)
ZSC 2375						\$34.95 (4-24)
TWO-WAY 180°						
PSCJ 2-1**	1-200	33	0.6 above 3dB split	2.5	.15	\$19.95 (5-49)
ZSCJ 2-1						\$34.95 (4-24)
PSCJ 2-2	0.01-20	33	0.3 above 3dB split	1	0.05	\$29.95 (4-24)
ZSCJ 2-2						\$44.95 (4-24)
ZMSCJ 2-2						\$44.95 (5-49)
TWO-WAY 90°						
PSCQ 2-90	55-90	30	average of coupled outputs less 3dB	3	1.0	\$19.95 (5-49)
THREE-WAY 0°						
PSC 3-1	1-200	30	J, 4 above 4.8 split	2	0.1	\$19.95 (6-49)
ZSC 3-1						\$34.95 (4-24)
ZMSC 3-1						\$44.95 (4-24)
PSC 3-2	0.01-30	40	0.25 above 4.8 split	2	0.1	\$29.95 (6-49)
ZSC 3-2						\$44.95 (4-24)
ZMSC 3-2						\$54.95 (4-24)
FOUR-WAY 0°						
PSC 4-1	0.1-200	30	0.5 above 6dB split	2	0.1	\$26.95 (6-49)
ZSC 4-1						\$41.95 (4-24)
ZMSC 4-1						\$51.95 (4-24)
ZSC 4-2	0.002-20	33	0.45 above 6dB split	2	0.1	\$64.95 (4-24)
ZMSC 4-2						\$74.95 (4-24)
PSC 4-3	0.25-250	30	0.5 above 6dB split	2	0.1	\$23.95 (6-49)
ZSC 4-3						\$36.95 (4-24)
ZMSC 4-3						\$48.95 (4-24)
PSC 4-6	0.01-40	32	0.4 above 9dB split	0.05	0.05	\$29.95 (6-49)
PSC 4-10	2-175	33	0.6 above 6dB split	0.08	0.08	\$26.95 (6-49)
SIX-WAY 0°						
PSC 6-1	1-175	30	0.75 above 7.8dB split	4	0.2	\$59.95 (1-5)
EIGHT-WAY 0°						
PSC 8-1	0.5-175	30	0.8 above 9dB split	3	0.2	\$59.95 (1-5)
ZFSC 8-1						\$109.00 (1-3)
ZFSC 16-1	0.5-125	37	0.8 above 12dB split	2	0.08	\$174.95 (1-4)

COMMON SPECIFICATIONS FOR ALL MODELS: Impedance all ports, 50 ohms. *Except 75 suffix denotes 75 ohms VSWR:1.1-1.2 typical Nominal phase difference between output ports, 0° **Except J suffix denotes 180° Q denotes 90° Delivery from stock; One week max. P prefix denotes pin models, Z prefix denotes BNC/TNC connector models, ZM prefix denotes miniature-SMA connector models.

For complete specs, performance curves and drawings, see pgs 161-303 of the 1976-77 MicroWaves Product Data Directory.

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CIRCLE NUMBER 3

NEWS

- 21 **News Scope**
- 29 **Washington Report**
- 50 **Instrument '76 special issue**, featuring major trends in instrument technology.
- 52 **Smart instruments**—They've got computing power that boggles the mind.
- 60 **Portable instruments**—The specs are good but the battery life is short.
- 68 **Howard Vollum, Bill Peek and Wim Velsink of Tektronix** discuss scopes.
- 76 **Programmable instruments**—The standard 488 bus is playing a major role.
- 88 **Combined instruments**—They're often better than the sum of their parts.
- 96 **Ulrich Rohde** speaks on American and European engineers.
- 104 **Standards and calibration**—Instruments improve as standards are more accurate.
- 114 **Safe instruments**—Without safety in mind instruments could be hazardous.

TECHNOLOGY

- 35 **MICROPROCESSOR DESIGN**
- 124 **Get on the IEC bus.** Soon to be an international standard for interfacing instruments, the bus brings many benefits—and a few problems too.
- 130 **Measuring capacitor loss:** Are S-parameters any good? They're not, but other methods—like the use of Q-bridges or resonant coaxial lines—are acceptable.
- 136 **Measure the characteristic impedance** of almost any line with this two-load technique, and avoid many of the limitations of traditional methods.
- 140 **Measure pulse-rate ratios** automatically to four-place accuracy. Simple circuit handles steady or random signal rates with ratios greater or less than unity.
- 146 **Don't sweat with thermocouple thermometers.** CMOS analog and digital devices make it easy to design an inexpensive thermometer.
- 152 **Low-cost data-acquisition systems** need not transmit analog signals. Two-chip integrating a/d converters need only two wires for data handling.
- 160 **Consider v/f converters** for data-acquisition systems. They offer high resolution and accuracy when used as analog-to-digital converters.
- 168 **Ideas for Design:** Inverter circuit handles bidirectional signal flow without latching up . . . Voltage-controlled oscillator provides symmetrical triangular and square waveforms . . . Control the data rate of a μ P system with software instructions . . . Use TTY or CRT interchangeably on μ P system . . . Stable constant-voltage supply uses current source to establish reference.
- 178 **International Technology**

PRODUCTS

- 183 **Instrumentation:** DPM building blocks make 93 different instruments.
- 184 **Instrumentation:** Digital integrator reads watt or amp-hours.
- 209 **Modules & Subassemblies:** Compact 12-bit s/d converter cuts weight.
- 221 **Packaging & Materials:** Solderless breadboards handle 600-mil DIPs.
- 198 **Components**
- 204 **Discrete Semiconductors**
- 216 **Data Processing**
- 228 **Integrated Circuits**
- 236 **Power Sources**
- 238 **Microwaves & Lasers**

DEPARTMENTS

- 47 **Editorial:** The old man at the bar
- 7 **Across the Desk**
- 240 **Application Notes**
- 243 **Evaluation Samples**
- 243 **Design Aids**
- 246 **New Literature**
- 248 **Bulletin Board**
- 248 **Vendors Report**
- 252 **Advertisers' Index**
- 254 **Product Index**
- 256 **Information Retrieval Card**

Cover: Cover designed by Art Director, Bill Kelly.

ELECTRONIC DESIGN is published biweekly by Hayden Publishing Company, Inc., 50 Essex St. Rochelle Park, NJ 07662. James S. Mulholland Jr., President. Printed at Brown Printing Co., Waseca, MN. Controlled circulation postage paid at Waseca, MN and New York, NY, postage pending Rochelle Park, NJ. Copyright © 1976, Hayden Publishing Company, Inc. All right reserved. POSTMASTER: Please send form 3579 to ELECTRONIC DESIGN, P.O. Box 13803, Philadelphia, PA 19101.

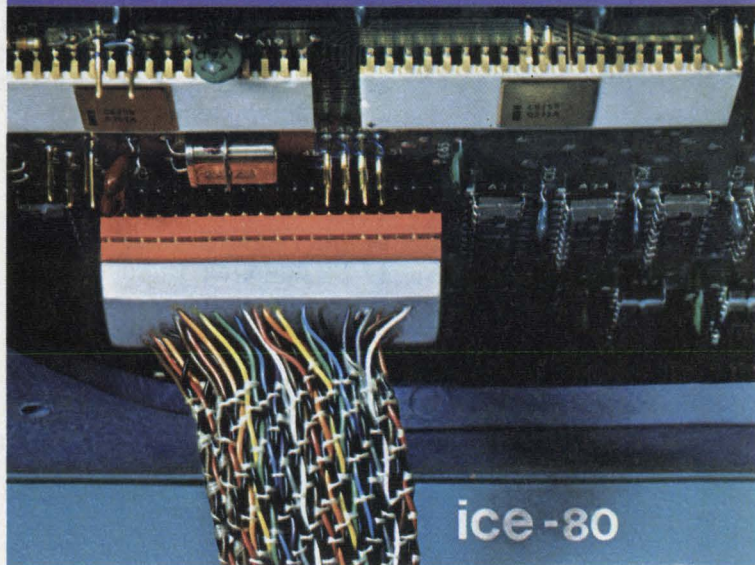
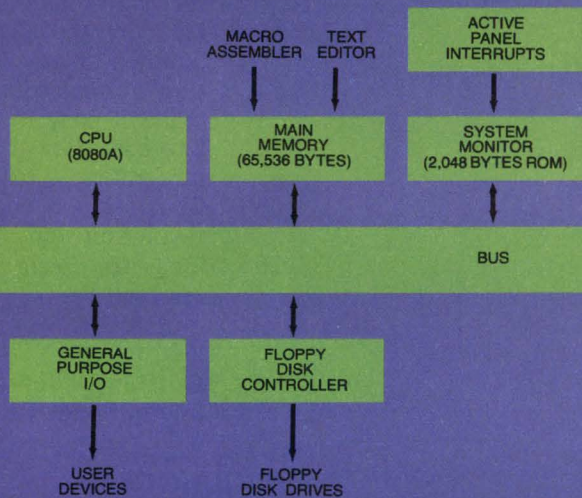
In-circuit emulation product can do while

The dream of design engineers is to develop, debug, and integrate hardware and software in their actual product environment—from day one. Thereby dramatically shortening the development time—and development cost—of their microcomputer-based products.

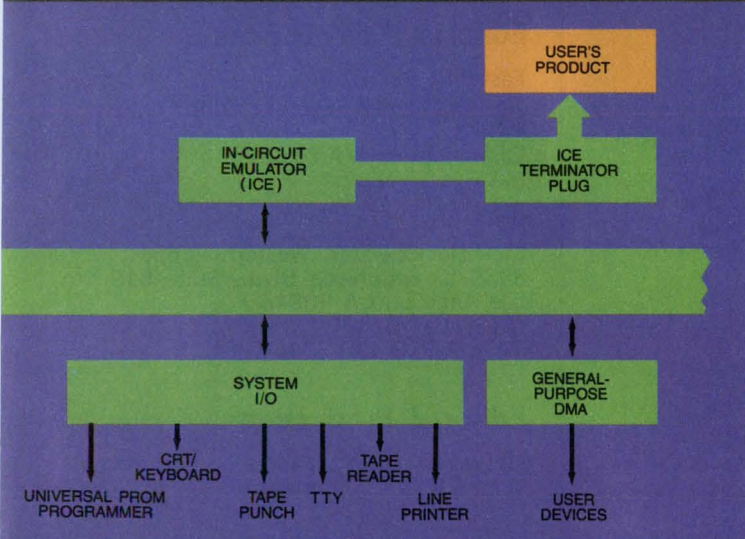
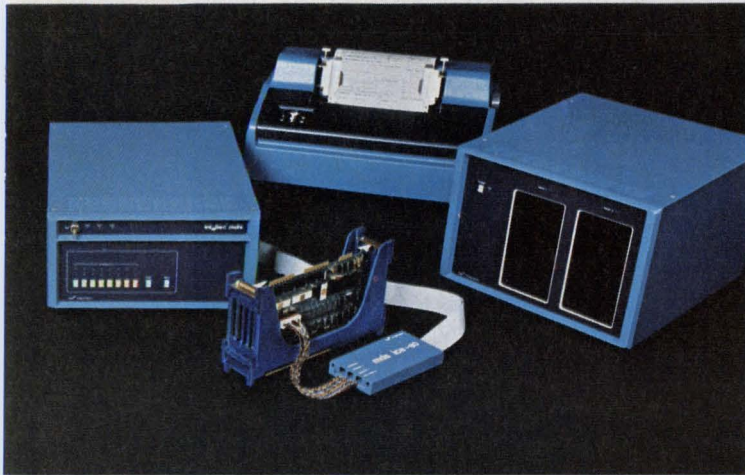
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lets you see what your it's still on the bench.



```

*GO FROM START UNTIL RSLT WRITTEN
EMULATION BEGUN

*DISPLAY CYCLES
STAT-ADR-DATA STAT-ADR-DATA STAT-ADR-DATA S
A2H-1326H-CDH 82H-1327H-E3H 82H-1328H-01H 0

*CHANGE DOUBLE REGISTER SP=13FFH
*BASE HEX
*EQUATE STOP=1333H
*GO FROM START UNTIL STOP EXECUTED THEN DUMP
EMULATION BEGUN
B=01H C=41H D=00H E=00H H=00H L=00H F=56H A=
    
```

The Intellect system includes its own 8080 processor, memory, and a full range of peripherals designed to ease your development task. These include diskette operating system, CRT/keyboard, line printer, universal PROM programmer, high speed papertape reader, the in-circuit emulation modules, (ICE-80 and ICE-30) and interfaces for teletypewriter and high speed tape punch.

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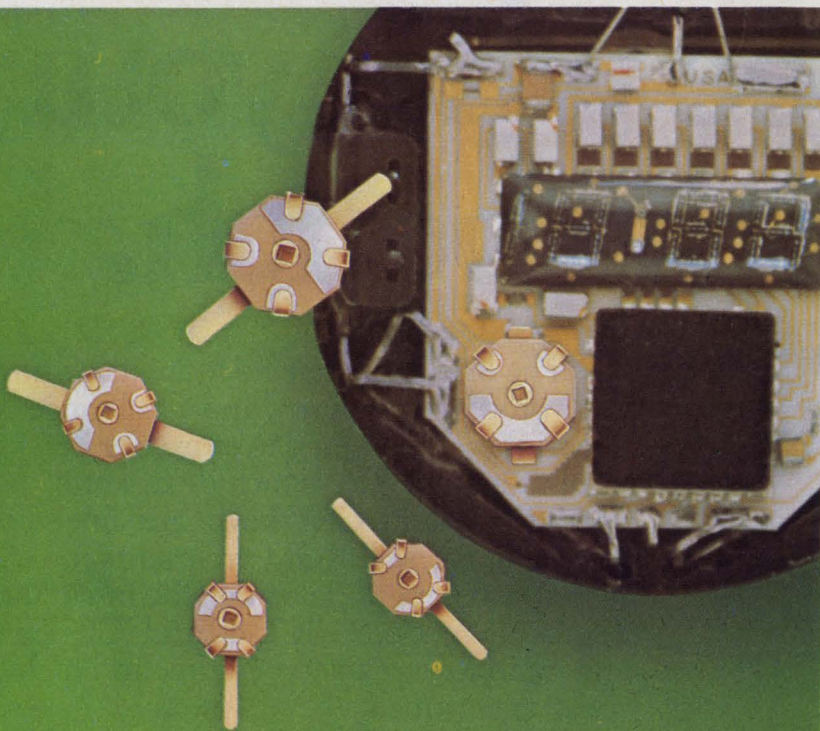
The Intellect system provides the convenience of a complete in-house development system, backed with the quality support, service, training, and documentation you expect from the company that is the leader in microprocessor systems development. And the Intellect system is available for immediate delivery.

If you've always wanted to see how your product works while it's still on the bench, experience an Intellect system for yourself. For a demonstration or for technical information use the reader service card or write: Intel Corporation, 3065 Bowers Avenue, Santa Clara, California 95051.



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CIRCLE 278 FOR TECHNICAL INFORMATION ONLY
CIRCLE 279 FOR A DEMONSTRATION & TECHNICAL INFORMATION



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CIRCLE NUMBER 5

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Across the Desk

Wolfe's Law

Buried deep in some secluded mountain cave, there must be an archive where silent monks guard the profundities of our industry. This is where one should find Murphy's Law (if anything can go wrong, it will) and its corollaries. Here, too, one should find Wolfe's Law, propounded by the Vice-President of Gould Inc. and General Manager of the Centralab Electronics Div. Those less versed in the philosophical underpinnings of our industry should know that Wolfe's Law states that: "It requires more effort to change something than not to change it."

The principal corollaries belabor the obvious:

- The effort expended by the person who wants to change something is the square of the effort expended by the person who doesn't want it changed.

- Success is inversely proportional to resistance.

Engineers, wake up: You are being raped

Recently, it seems, we have been deluged with a flood of Engineering Design Contests. There have been Microprocessor Contests, FPLA Contests, PLL Contests, etc. At first glance, these contests would seem to be a way for the engineer to exercise some creativity, while possibly winning a prize for his efforts. In reality, they are a great rip-off of the working engineer.

Who benefits from these contests? Clearly, only the contest sponsor. The sponsor gains in three ways. First, he obtains—at virtually no cost—an enormous

library of applications data. Second, those engineers submitting contest entries are more likely to use the sponsor's product than the product of a competitor. Third, the sponsor can now attract even more business because he can provide a great wealth of applications literature.

The engineer is getting raped and doesn't realize it. If the engineer charged a consulting fee for the effort that goes into a contest entry, he would likely do better than if he had won first prize. Yet the chance of "getting something for nothing" is enticing engineers to give away their services.

This brain picking would never work in any other profession. Imagine a large law firm asking independent lawyers to prepare a brief on a pending case. The lawyer who prepares the best brief wins a calculator.

Or think of a pharmaceutical company asking doctors to develop a new drug. The best one wins a trip to Florida. How insane that engineers don't realize that these so-called contests amount to the same thing.

If engineers are ever to obtain a truly professional status, they must start acting like professionals and stop giving away their services.

Alan Rosenbaum

*Manager of Computer Products
General Microwave Corp.
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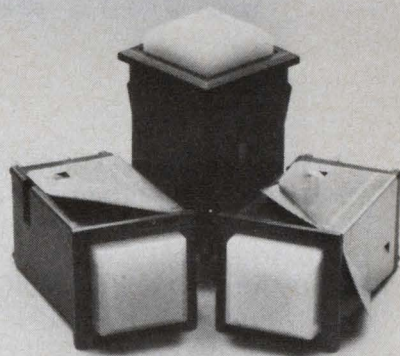
You want to be better, I want you to be better

I was intrigued by your editorial, "We Want to Be Better" (ED No. 17, August 16, 1976, p. 59), in

(continued on page 11)

Electronic Design welcomes the opinions of its readers on the issues raised in the magazine's editorial columns. Address letters to Managing Editor, Electronic Design, 50 Essex St. Rochelle Park, N.J. 07662. Try to keep letters under 200 words. Letters must be signed. Names will be withheld on request.

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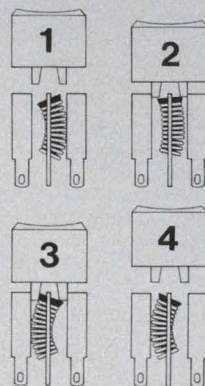
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An incredibly simple design gives you electrical and mechanical characteristics associated with larger switches in a miniature, .625-inch package at an economical price.

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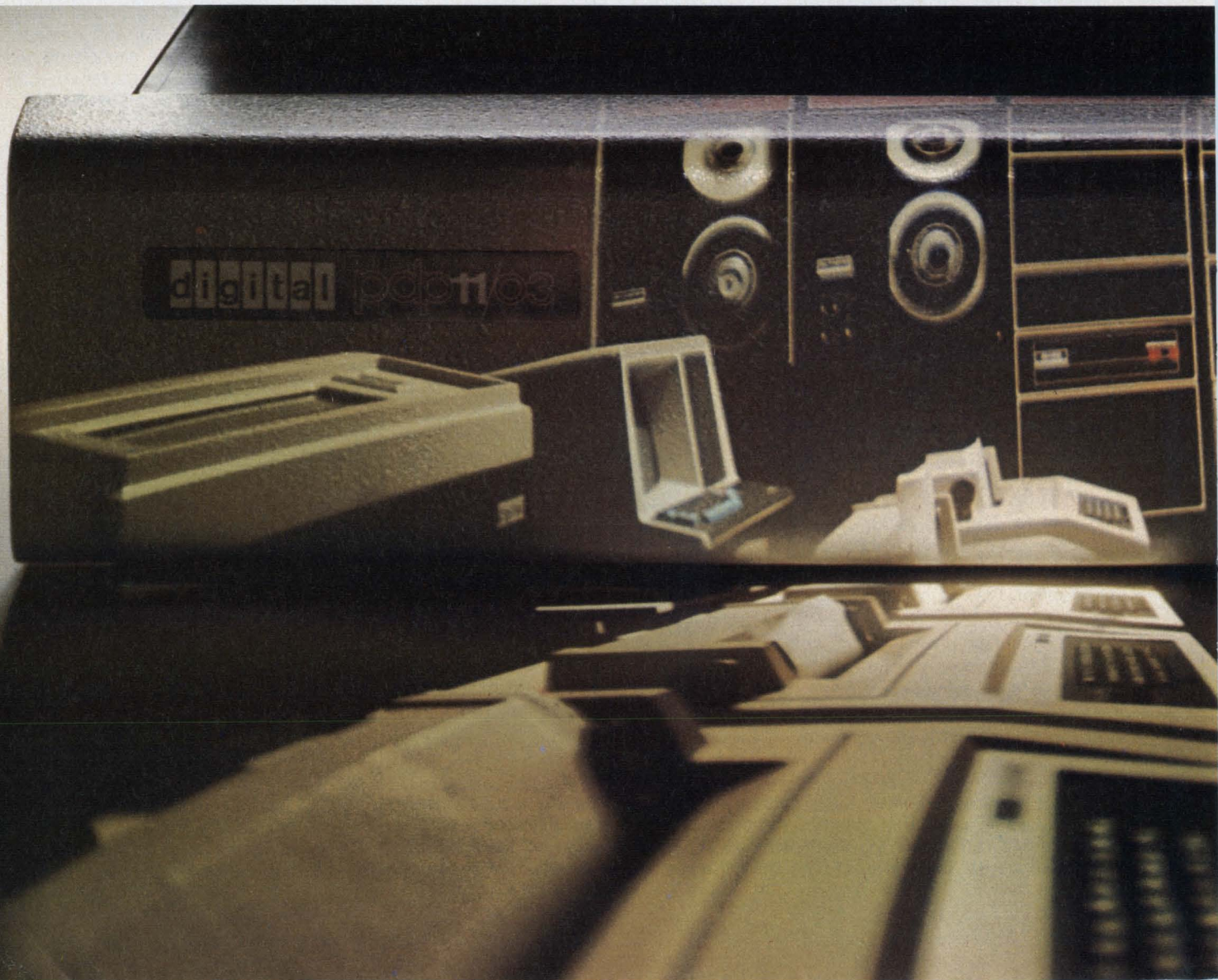
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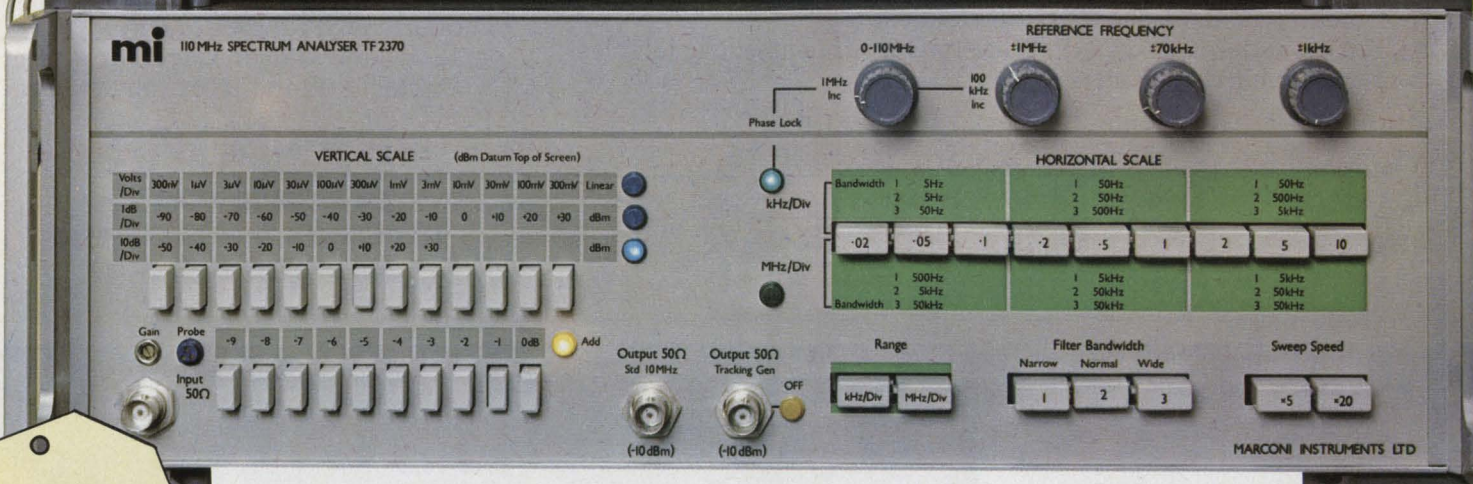
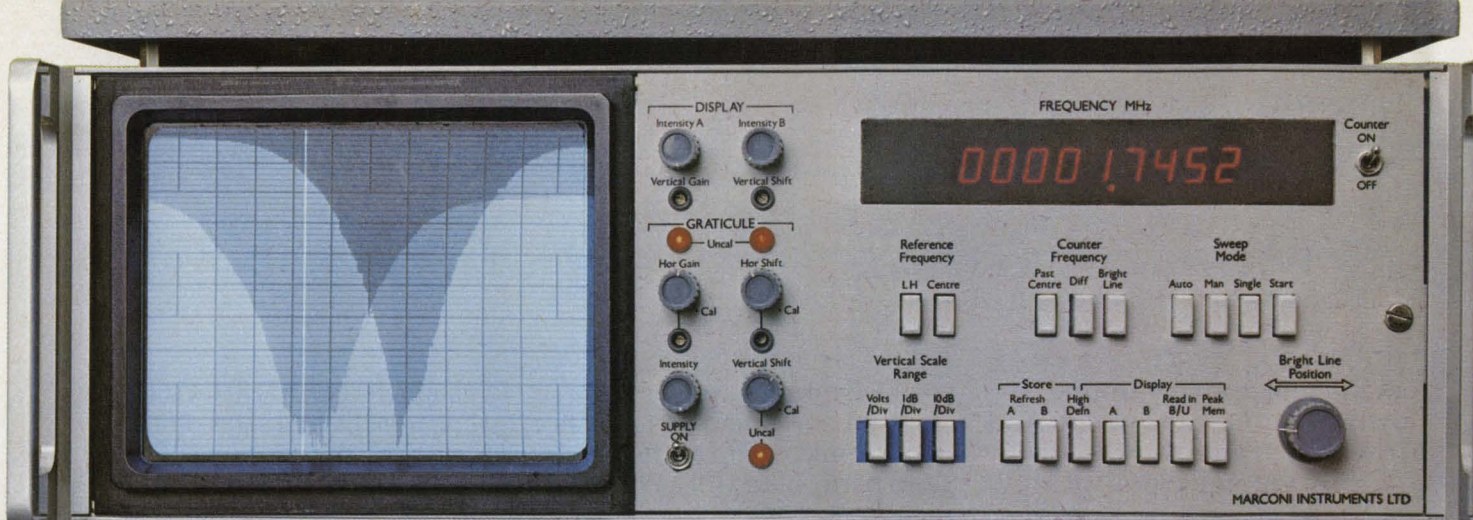
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CIRCLE NUMBER 8

750R

ACROSS THE DESK

(continued from page 7)

which you stressed that ED, unlike some of its competitors, admits to its editorial gaffs. Such honesty is commendable and certainly reinforces the reader's faith in your fine publication.

I wish to call attention to the article on CRTs in the same issue. Your editor wrote, "Almost as diverse a selection of CRTs is available from RCA's Industrial Tube Div., Lancaster, PA, and RCA's Electronic Components Div., Harrison, NJ." Historically, that statement would have been redundant since the Industrial Tube Division in Lancaster was a part of Electronic Components, headquartered in Harrison. But in March 1975, when RCA reorganized its Electronic Components activity, the Industrial Tube organization became an integral part of RCA Electro-Optics and Devices, now an organizational entity within the Solid State Division. It is therefore proper to identify RCA Electro-Optics and Devices, Lancaster, PA, as the CRT supplier.

Walter B. Dennen

Manager, News and Information
RCA
Solid State Division
Route 202
Somerville, NJ 08876

Charlie and Clarence, and Clark and Jack

You may have had a good reason to oversimplify the concept of modern management in your "Scientific Management" editorial (ED No. 18, September 1, 1976, p. 61)—possibly to make a point with a specific segment of your readers. However, I'd appreciate equal time for the other viewpoint.

My position is Senior Engineer. Contrary to the flavor of your editorial, my preference, as a worker, would be the modern concepts. These include extensive group interaction, group participation in management decision making, self-scheduling and personal development.

A manager who claims to use the latest tools, but in fact is using only the latest bookkeeping methods, does not merit the manage-

ment title.

The management team I work for claims to be from the modern school. Nevertheless, the work is done without planning, production-line style, open door policy "with authorization," and one-way communication with the single goal of keeping the boss out of trouble. All the management books I've read place this philosophy in the old school.

Concerning your editorial specifically, you refer to "Charlie" as responsible for his staff, running things smoothly, getting things done and using the best tools. "Clarence" on the other hand is a production pusher with computer-generated numbers to prove his point.

If you would play engineer for a while and list side by side the comparative philosophies from the old and new schools, theory X vs theory Y, oldest vs latest tools, your own management articles possibly, I think you'd find yourself forced to put Clarence in the old school sporting some fancy new gadgets. Charlie would also be old-school.

If you want to meet a new schooler, look at Clarence's replacement, "Clark," who spent the first 2 weeks getting to know his staff, meeting their families, outlining their future objectives, organizing their likes, dislikes, observations, ideas. Clark identified "Chuck" as the group's self-appointed spokesman and asked him to help organize the group's ideas into working projects to iron out any bugs. Production was in fact down because so much time was being devoted to organization and meetings.

Within a week, Clark came to see Jack with a list of things to discuss. Unfortunately, each item had a price tag, some quite high, at a bad time in the economy. But unlike other VPs, Jack was determined to back his middle managers as far as he could until they either could handle the rope themselves or hang from it. After the proposed machine modifications were made, production began at 2000 subassemblies a day with 5 rejects. A week of fine timing brought that to 2500 and usually 1 reject a week. And despite the apparent radical appearance of the get together, Jack himself showed up at the bowling alley to pass out

(continued on page 16)

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CIRCLE NUMBER 9



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reliability wouldn't mean very much if we didn't deliver it in the kind of state-of-the-art products you need.

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Compact Timer/Counters at 80, 520 and 1,000 MHz

Until now, if you needed a high performance timer/counter with all the capabilities and versatility of a lab instrument, you expected a high price. That is, unless you could do without time interval averaging capabilities or if you could get by without trigger hold-off or if you could compromise on triggering capabilities or if you didn't mind the shortcomings of a plastic case. But, that's the way it was with timer/counters. Today, our new PM 6620 series offers performance without compromise in a compact, package at compact prices.

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For immediate detailed information on the PM 6620 series utilize our HOT LINE number - 800 645-3043. N.Y.S. residents call collect - (516) 921-8880., or contact Philips Test & Measuring Instruments, Inc.

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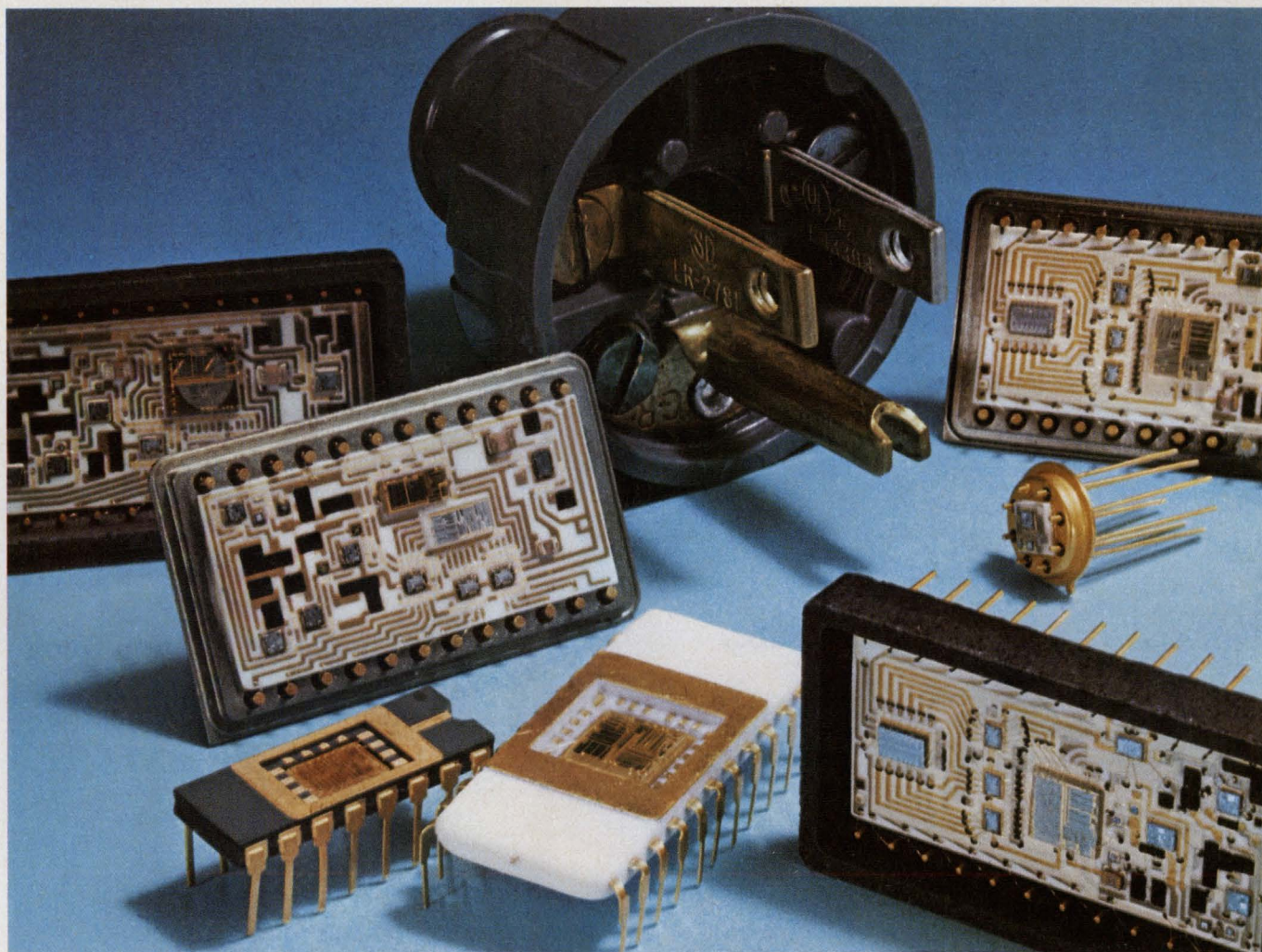
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FOR INFORMATION CIRCLE #282

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ACROSS THE DESK

(continued from page 11)

various awards, a few bonuses to exceptional idea people and offer the entire group one extra week of paid vacation. In six months, Chuck took over as supervisor and Clark became manager of systems engineering.

Come on, George, sign up for some courses in the new school. We don't discriminate against old timers, nor do we believe that old gods can't learn some and contribute some. Just beware of the pseudo-new schoolers.

Bruce Nappi

Misplaced Caption Dept.



My company won't let us fly first class anymore.

Sorry. That's Honoré Daumier's "Third Class Carriage," which hangs in the Metropolitan Museum of Art in New York City.

And it tasted great

I am trying to locate a source for a product I used several years ago. It consisted of a chemical powder, which, when applied with a dampened cloth to bare clean copper, would deposit a plating on the copper similar to a finely tinned surface.

I vaguely recall a name like AMP-ON, but I am not certain.

If you can advise me as to the best way to track down such a product, it will be greatly appreciated. Thank you.

*Peter J. Farrell
Sperry Engineer*

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JOHNSON

CIRCLE NUMBER 13

CIRCLE NUMBER 243 ►

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Someday Issaquah will be famous.

Someday, people will say: "Issaquah, Washington, that's the home of Data I/O!"

But that's "someday." Today, more people remember us for our PROM programmers than for our name. We understand. After all, the 1500 companies who use our machines need programmers—not a name. So here's what's behind "Data I/O."

Our most popular programmer is the Model V. It is already out-selling every other PROM programmer in the world (including the former world champ, the Data I/O Programmer I). It can program all PROMs now available (165 at last count), and it's approved by the PROM manufacturers.

Our Programmer VI lets you program from one to eight MOS PROMs simultaneously with the same, or different programs. (It can program an entire memory board in less than 30 seconds.)

Our new Programmer VIII is a completely portable, microprocessor based unit. You can take it anywhere and easily update it year after year.

Our Programmer X is for Programmable Logic Arrays (PLA's). It features CRT display, multiple inputs and outputs, and error detection through both logical and array verification. It's also microprocessor based.

Our Romulator lets you emulate any PROM configuration on the market today, develop a complete

program and debug it before you ever have to commit it to a PROM.

Data I/O offers a unique calibration standard which lets you calibrate to each PROM manufacturer's specs—before you program—for maximum yields and long term I-C reliability.

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1. Every Data I/O customer receives a quarterly update on currently available PROMs.
2. Through our direct (computerized) mailing program, Data I/O customers are kept constantly up-to-date on PROM specification changes and technological innovations.
3. Nine field offices in the U.S. and 22 distributors worldwide provide our customers with direct sales support, installation, and operator training.

Get the facts

If you would like to know more about our products, or want copies of our quarterly PROM Comparison Chart and PROMBiTS (our periodic technical bulletin on PROM applications and innovations), mail this coupon or call one of our offices. Data I/O Corporation, P.O. Box 308, Issaquah, Washington 98027.

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Biomation's new logic analyzers give you both.

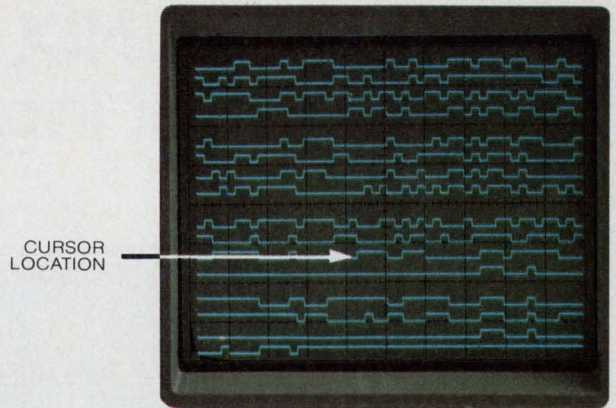
When your job is to interface, integrate and program a complex new digital logic system, you want as much information as you can get.

That's why we're providing a new set of tools which let you display timing information as well as logic word content—in the language of your choice.

Our new 1650-D logic analyzer gives you 16 channels at 50MHz. Our 851-D gives you 8 channels at the same speed. Accessories can now give you a logic state (1's and 0's) display of any 16 stored words; hex or octal translation; and a vector map of memory contents. The 8 and 16-channel logic analyzers feature:

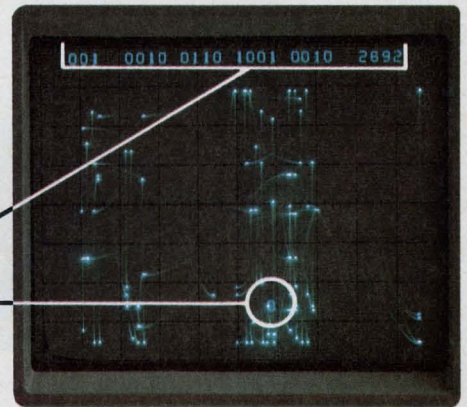
- Pretrigger and delayed trigger recording
- Trigger point can be easily identified
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- Movable display cursor that stays with the data when you switch display modes
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These are complex instruments and we can't give you all significant details here. But please write, call, or use the reader service card. We want to get this useful information into your hands. Biomation, 10411 Bubb Road, Cupertino, CA 95014, (408) 255-9500. TWX: 910-338-0226.



CURSOR LOCATION

Biomation's new 1650-D produces a repetitive display output reconstructing precisely 500 bits per line for a 16-line timing diagram on a conventional oscilloscope or CRT display. Separate selection of individual channel outputs allows viewing of 1, 2...16 channels at one time with automatic vertical expansion.



CURSOR WORD

CURSOR

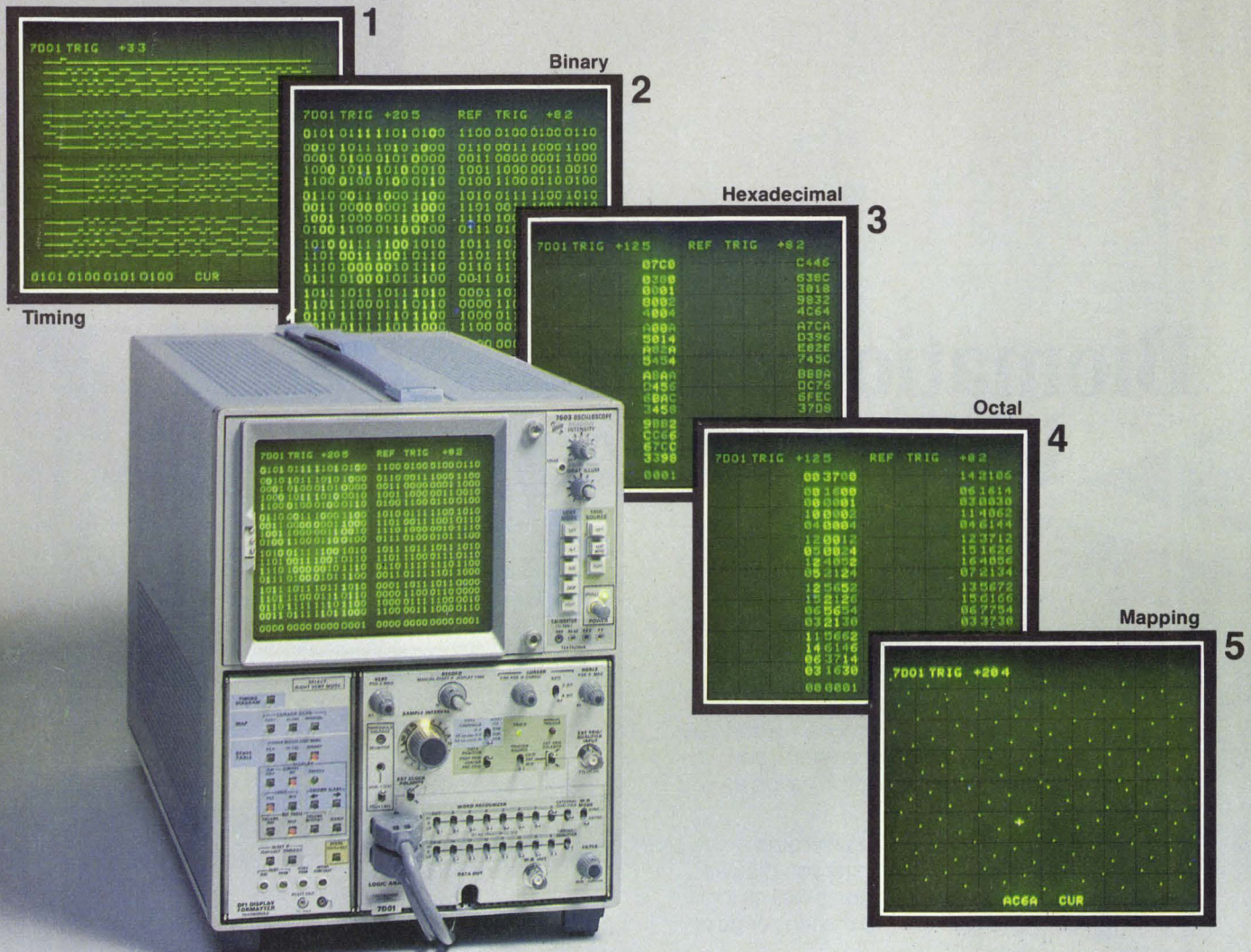
Map—each word in memory is transformed via two DAC's to form a unique dot which characterizes that word. All 512 words of the 1650's memory can be accessed for mapping. The cursor word is circled in the map as well as displayed at the top of the screen in alphanumeric form. The cursor may be moved to any of the points in the map for positive identification of that word. In addition, a map of only 16 words may be selected.

CURSOR WORD	136	1	111	111	110	000	101	177605
	137	0	001	101	011	111	111	015327
	138	0	001	011	010	000	110	013206
	139	1	000	010	010	000	111	102207
RELATIVE ADDRESS	140	1	000	010	010	000	111	102207
	141	0	000	111	110	100	000	007640
	142	1	000	101	010	100	001	105241
	143	0	011	000	010	100	010	030242
TRUTH TABLE	144	1	000	000	110	100	011	100643
	145	0	011	101	010	100	100	035244
	146	0	010	010	110	100	101	022645
	147	0	000	010	010	100	110	002246
HEX OR OCTAL TRANSLATION	148	1	000	000	010	100	111	100247
	149	0	101	010	000	001	011	052013
	150	1	000	000	010	100	111	100247
	151	1	101	100	100	001	000	154410

Logic state—provides memory address location, binary output of the 16 channels and selectable octal or hexadecimal translation. 16 words are displayed at one time with the cursor address location at the top of the screen. Movement of the cursor control allows accessing any 16 words of the entire 512 words stored in the 1650-D. The display control memory can store 16 words while a different set of 16 is selected from the 1650's main memory (or a new recording is made). These two sets of 16 words can then be overlaid on the CRT. Any differences will blink and be easily identified.

biomation
Creating tools for technology

TEKTRONIX now has 5 ways to look at logic.



The New DF1 Formatter

First, we gave you the timing display and binary readout with our 7D01 Logic Analyzer. Now, with the DF1 Display Formatter, which is dedicated to the 7D01, you have five display formats to operate from, all in a 7000-Series mainframe. Now you can convert a timing display into tables of words in Binary, Hexadecimal, Octal ... or a mapping configuration ... whatever your application requires.

A STATE TABLE mode of operation produces standard tables of up to 16 lines of 16-bit words. Using the 7D01's cursor, you can step through these tables word-by-word in Binary, Hex, or Octal. A 17th word is added to each table emerging from the 7D01's memory, to serve as a "key" and indicate you are indeed scrolling correctly through the long memory. The 7D01's fine cursor

control steps the display line-by-line, while the coarse control advances it table-by-table.

One of the most powerful analytical capabilities provided by the STATE TABLE mode is that you can display two tables—a reference table of "proved" data plus a "new" data table drawn from a system under test—on the same crt for side-by-side comparison. New data that is different from the reference data is automatically intensified ... you immediately know faulty data exists, and you know its location.

With the DF1 you can map, not just one, but three ways. The ability to map FAST, SLOW, or MANUAL lets you quickly recognize a word of interest, track it, isolate it, then pinpoint it for detailed analysis. The importance of mapping is derived from the speed with which you can isolate problems.

The logic analyzer package shown (7603 Option 1, 7D01, DF1) starts as low as \$5790. If you already own a 7000-

Series mainframe, add the 7D01-1 (7D01/DF1 combination) for only \$4390. Also consider that your money buys you these important 7D01 features: 1) Word recognition, 2) 16 channel operation, 3) 15-ns asynchronous timing resolution, 4) 4k formattable memory (4, 8 or 16 channels), and 5) High Z probes.

For more information or a demonstration of the DF1, contact a Tektronix Field Engineer near you. Or write Tektronix, Inc., P.O. Box 500, Beaverton, OR 97077.

United States sales prices are F.O.B. Beaverton, OR. For price and availability outside the United States, please contact the nearest Tektronix Field Office, Distributor, or Representative.



FOR TECHNICAL DATA CIRCLE # 241
FOR DEMONSTRATION CIRCLE # 242

NOVEMBER 22, 1976

Mag tape systems plug into IEEE 488 bus

The first magnetic tape systems designed to plug directly into the IEEE 488 standard bus and compatible with IBM and ANSI tape standards use an 8080 microprocessor for full tape control and tape-to-bus interface.

Designed by Information and Applications, Beltsville, MD, the type 4600 systems have an 8080 control box with only 75 chips, according to Scott McPhillips, system designer. "An equivalent IBM type of controller uses about 260 IC's," notes McPhillips.

The microprocessor makes it easy to interpret bus commands from any 488 bus controller such as a calculator or instrument. One bus pair is dedicated to tape data, while another provides a separate channel for tape control and status information, according to McPhillips.

Addressed as a listener, the 4600 records data from the instrument or calculator talking on the bus. Addressed as a talker, it reads back the tape.

"The microprocessor has allowed us to implement everything that a large IBM controller does, including one-track error correction," adds McPhillips. More over, all of the control for the tape drive is in software.

Read errors are eliminated by a system that recovers the data by rereading with different thresholds. If the error persists, the system reconstructs the data with IBM-compatible parity and error-correction codes.

Should a tape defect cause a recording error or even a marginal signal, the data are automatically erased and rewritten further along the tape.

The error-correcting function requires only two pages of the program.



The 4600 mag tape system uses an 8080 μ P for tape control.

Other low-speed, off-line tape systems don't incorporate these read and write error-correction features. They may record compatible-check characters, but they don't make use of them, according to McPhillips.

The microprocessor also provides full read and write data buffering and free format-command processing. The data buffer holds an entire block of data and transfers it over the bus, character by character, whenever the appropriate instrument calls for it.

The 4600 systems are available with 7, 8-1/2 and 10-in. reels that use 0.5-in. wide, 1.5-mil computer tape. The 10-in. reels operate at 45 ips, and the other two at 25 ips. Data-transfer rates are 0 to 3000 byte/s for the large-reel machine and 0 to 2500 byte/s for the smaller ones.

JEDEC package outlines are now available

A complete collection of JEDEC-registered, solid-state package outlines and dimensional information has been issued by the Joint Electronic Device Engineering Council of the Electronic Industries Association (EIA) and the National Electronics Manufacturers Association (NEMA).

"JEDEC Registered and Standard Outlines for Semiconductor Devices" (JEDEC publication no. 95) supersedes and replaces EIA documents 12F, 13, 76 and RS-389.

The 600-page loose-leaf volume includes over 400 package outlines for diodes and transistors, microelectronic devices, uncased devices (such as beam-leaded components), carriers and magazines, gauges and military devices.

Complete dimensional information and detail drawings of all registered and standard package outlines come in both inch and metric versions with manufacturing tolerances. In addition, the volume contains illustrations, symbology and a guide for preparation of drawings. Indices and explanatory data are also provided for quick and accurate reference.

The collection can be ordered from EIA's Standard Sales Office, 2001 Eye St., NW, Washington, DC 20006, \$42.50 per volume. An optional subscription service, which provides new and revised update sheets, is available for an additional \$15 a year.

μ C-based switchboard helps cut phone bills

Promising to cut a large corporation's telephone bill by 30 to 50%, a computer-based system that controls and records a company's outbound, long-distance calls has been announced by Datapoint Corp., San Antonio, TX.

Infoswitch first checks the priority rating of a caller's identity number and tries to select the least expensive route using WATS, FX (foreign exchange), tie lines or other voice-communications facilities. Then, if all these circuits are busy—and the priority number warrants it—the call is put through via Direct Dial.

After the call, Infoswitch records the caller-identity number, the number dialed, the facilities used and the call's duration on magnetic disc.

The heart of this economical system is a dual processor that employs a dedicated microcomputer for high-speed telephone switching and a Datapoint business computer for logging the calls, monitoring the system and generating management reports. A printer can be added for hard-copy output; a magnetic tape can be included for either storing accounting data on a long-term basis or transferring data to another processor.

The switching equipment consists of a Datapoint μ P with a 300-ns cycle, a 16-k ROM program storage, a 4-k RAM temporary storage and a reed-relay switch matrix.

The processor—Datapoint's 5500—uses either diskettes, which store 250,000 characters each, or a cartridge disc system that stores 5-million characters on each disc. Copy is printed out at a speed of 80 copies per second.

Additional phone features include 3-digit code numbers for numbers frequently called and multistage call holding—the computer holds the caller on a low-cost circuit until a line clears. Length of the hold depends on the caller's priority number.

A 6-trunk system costs \$35,000, a one-year lease \$1113. A 55-trunk system costs \$175,000.

Army computer system a super problem solver

A supercomputer with a demonstrated ability to achieve processing speeds of over 800-million instructions per second has been developed by System Development Corp., at its Huntsville, AL operation, with the help of Burroughs Corp. Known as Pepe (for parallel-element processing ensemble), the first system has been delivered to the Army's Ballistic Missile Defense Advanced Technology Center in Huntsville, to carry out ballistic-missile-defense experiments and tests.

Although the Army's Pepe system has a CDC 7600 master computer that is wired to control 288 slave elements, only 11 are operat-

ing to date. Each "slave" consists of three processors sharing a common data memory, and each processor has an arithmetic capability equivalent to a medium-scale scientific computer.

In general, the Pepe system employs parallel processing and associative-data techniques to take on problems so complex that their solutions require inherent parallelism and extensive computational power. Parallel processing allows the system to solve many lengthy scientific computations simultaneously. Associative data retrieval enables Pepe to perform multidimensional file searches.

Besides missile defense, weather forecasting, air-traffic control, image data processing, and signal processing can also benefit from the increased computational power.

While the Pepe system's gate-level logic design and the electrical and mechanical design come from Burroughs, the specifications and architectural design to the register level come from SDC. SDC has developed the Army system's support software and produced the real-time programs, and plans to run the ballistic missile defense experiments and tests.

High-density RAM board has a good memory

A RAM board with a capacity of more than 1.3 Mbits has been developed by Intel Corp., Santa Clara, CA. Unveiled at the recent Mini/Micro Computer Conference and Exposition in San Francisco, the high-density memory board contains 147 packages—80 of which are 16-kbit dynamic RAMs—in a board of area of less than 90 sq. in.

Designed for custom medical applications, the memory array is organized in 16-k words of 80 bits each and includes CRT refresh logic for up to five pixels. (A pixel is the number of bits required to support a single dot on the face of a CRT.)

The very tight package spacing is possible because the board consumes only 70 W when operating and 18 W in standby. Intel 2116 chips provide 400-ns access time and 500-ns cycle time at the board level.

This high-density memory board

costs about 0.4¢ per bit in small quantities and 0.25¢ per bit in large quantities.

Device emits all colors with applied voltage

A new kind of light-emitting device that produces light of all the colors of the spectrum by simply changing its applied voltage has been developed at the Ford Motor Co. research laboratory in Dearborn, MI.

A thin-film device consisting of two layers of metals separated by an insulator, the component is not only compatible with silicon-fabrication technology, but ultimately should become mass-produced at a low cost, according to Shaun L. McCarthy, senior research scientist and creator of the light source with staff scientist John Lambe.

The device fabricated to date employs a 500-Å-thick aluminum layer for one electrode, which is separated from a 300-Å-thick metal electrode—silver, gold, lead, or indium—by an insulating aluminum oxide layer 30-Å thick.

Applying 1.5 V across the device produces radiation at the red end of the spectrum. Increasing the voltage changes the color of the light through the orange into the blue at about 3 V. At 4 V, the optical energy radiated contains quanta of the full spectrum, and white light is visible.

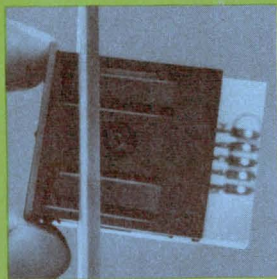
The quantum efficiency of experimental devices is in the 0.001% range, much less than the 0.1% to 2% of off-the-shelf monochromatic LEDs. To excite radiation, the current used by the Ford researchers ranges from about 20 to 100 mA, which corresponds to the range of standard LEDs. But the Ford devices' light output is substantially lower because of their lower-quantum efficiency.

While the potential quantum efficiency of the thin-film devices is estimated to be in the range of a few percent, it is currently restricted by having to couple energy out of the device. The radiation is produced by "inelastic tunneling" of the electrons through the insulating barrier.

The frequency of the emitted light is related to within a few tenths of a percent of the voltage.



Intro- ducing our new



thumbwheel switch

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CIRCLE NUMBER 17



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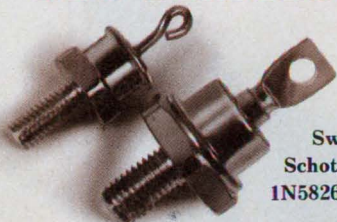
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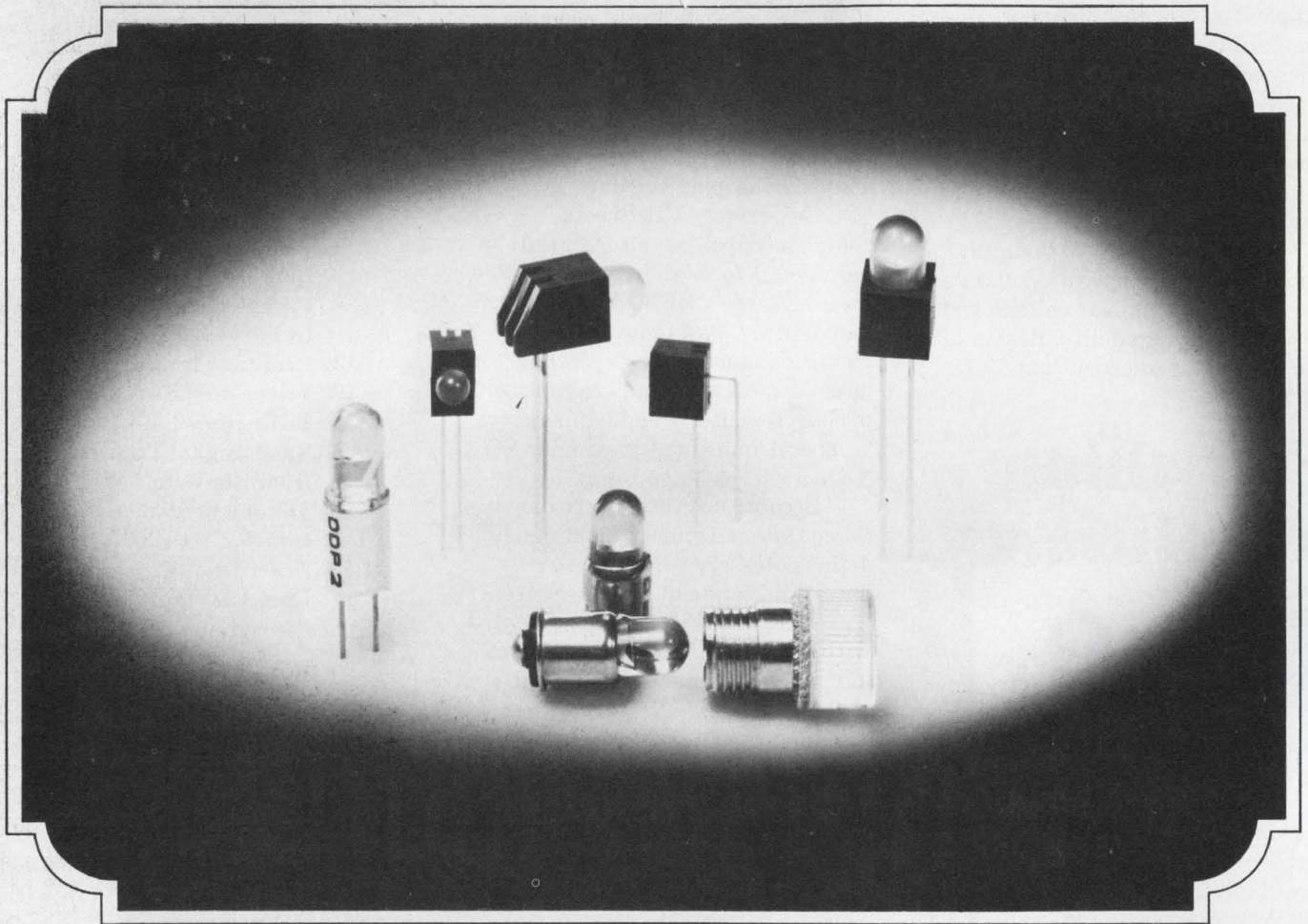


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CIRCLE NUMBER 20

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Washington Report

Electronic warfare to get more DOD attention

Procurement of electronic-warfare (EW) systems by the Defense Dept. will average at least \$500-million annually over the next five years, said Dr. Malcolm Currie, director of defense research and engineering, at a meeting of the Association of Old Crows at the National Bureau of Standards, Gaithersburg, MD.

Two of the principal EW projects planned during this period are the Navy's Tactical Airborne Signal Exploitation Systems (TASES) and the Air Force's Compass Hammer program, which will take the lead in developing airborne electro-optical countermeasures. The two services will join forces in the Compass Go program to develop a common internal jammer for the Air Force's F-16 air combat fighter and the Navy's F-18 naval strike fighter, as well as any future fighters.

In the past, EW systems have been almost an afterthought in the development of new aircraft and other weapons, according to Currie. But a recent Pentagon directive, 46003, stipulates that electronic counter countermeasures (ECCM) be specifically considered in the design of every new military system.

"ECCM must become an integral part of our planning—not a patchwork, subsequent add-on," said Currie.

Present plans call for research and development for electronic warfare to increase 10% a year from its present base of about \$250-million over the next five years.

More airports to get Category III ILS

Eight more U.S. airports will be upgraded to Category III instrument landing systems under a Federal Aviation Administration program to provide all-weather landing capability at key airports.

Category III operations require ILS guidance signals to permit landings without visual reference to the ground when the ceiling is zero and visibility on the runway is 700 feet.

The landing system uses solid-state components and includes a dual-channel localizer, dual-channel glide slope and three dual-channel marker beacons. A far-field monitoring system detects any shift in localizer-course alignment.

The system will be produced by Wilcox Electric Inc., Kansas City, MO, according to the terms of a \$3.7-million FAA contract. Deliveries will begin in late 1977 at a rate of two a month to New York Kennedy, Chicago O'Hare, Houston International, Kansas City International, Detroit Metropolitan, Seattle-Tacoma International, Los Angeles International and Portland International airports.

Four airports are already equipped with Category III equipment: Washington Dulles, Atlanta International, San Francisco International and

Denver Stapleton.

Under an earlier \$8.7-million contract to Wilcox, the FAA's largest single purchase of instrument-landing systems, the company will deliver 122 Category-I ILS units to smaller airports in early 1978. Category-I ILS requirements call for visibility of half a mile and the ability of the pilot to descend to a "decision height" of 200 feet, where he can see the runway and decide whether to land.

Missile guidance to use satellite data

A missile-guidance system that will use the future Navstar global positioning satellite to guide the missile to its target is being developed at the Air Force's Armament Development and Test Center at Eglin Air Force Base, FL.

Small antennas on the missile's surface will receive position information from the Navstars at frequencies between 1.2 and 1.5 GHz (L-band), which will help update the inertial systems during the mid-course portion of the missile's flight.

The missile-guidance system is expected to be applied first to the GBU-15 glide bomb, a winged version of the television-guided "smart bombs" used in Vietnam, then to a number of other new tactical weapons, say officials at Eglin.

Hughes Missile Systems Group and Teledyne Systems have been funded about \$1-million each for the first year of the three-year development program. By mid-1978, breadboard hardware should be produced for captive flight testing at Eglin on the F-4 fighter. Concurrently, the Air Force is developing an airborne computer for the new guidance system under its Digital Guided Weapons Program.

Weather radio growth predicted

By 1980, the National Oceanic and Atmospheric Administration's weather-radio service will serve 90% of the U.S. population with more than 300 transmitters, predicts an Administration spokesman.

Limited originally to boaters and fishermen in the mid-1960s, the network not only provides storm and flood warnings via 100 stations, but is also, since 1975, the only Government-operated radio system designated by the White House to warn against nuclear attack. Signals are broadcast at 162.40, 162.55 and 162.475 MHz, and the average effective radius is about 40 miles, according to NOAA.

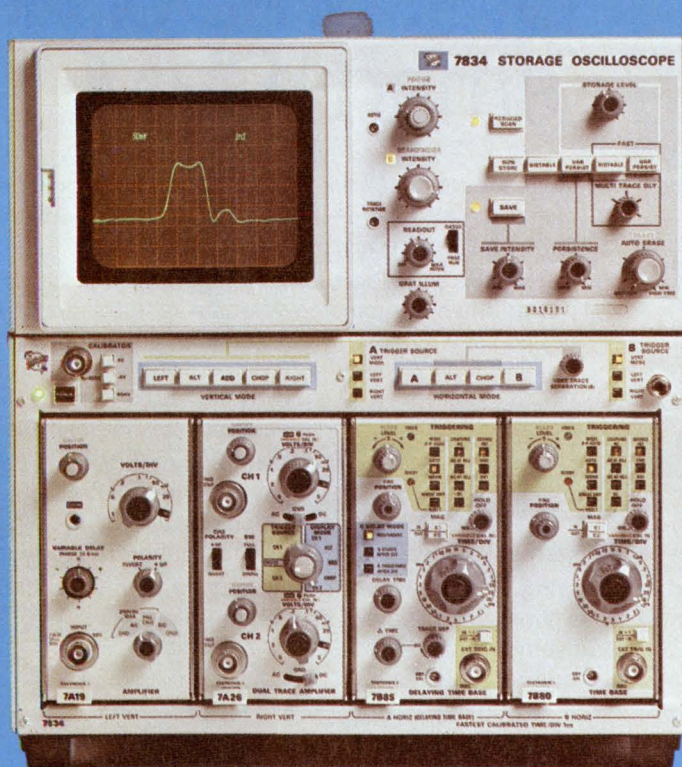
Capital capsules: Nippon Electric has been chosen by Intelsat to develop a 14-GHz mixer/intermediate-frequency amplifier with state-of-the-art microwave integrated circuitry for communications-satellite applications. . . . Despite a crash in a flight test on Oct. 4, the Air Force's Air-Launched Cruise Missile (ALCM) development and pilot production are expected to be carried out concurrently next year to push up the initial operational capability date from December, 1981 to January, 1979. The inertial platform is being blamed for the crash, not the terrain contour-matching guidance. . . . The Air Force's Avionics Laboratory plans to develop an infrared search-and-track system for continental air defense. . . . Texas Instruments and Honeywell are in the final competition for the AAQ-9 common forward-looking infrared (FLIR) to be used in the Pave Tack pods of the Air Force RF-4. The winner should be selected around the beginning of 1977.

Announcing a breakthrough in

FAST

PULSE ANALYSIS

A storage oscilloscope that captures 1.4 ns rise time.



Superior Performance. A stored writing speed of 2500 cm/ μ s, enabling you to capture single-shot rise times to 1.4 ns, 3.5 cm high, at full reduced scan amplitude (or 900 ps 2.25 cm high). System bandwidths from 160 to 400 MHz, depending on plug-ins selected. Four storage modes . . . bistable and variable persistence, FAST bistable and FAST variable persistence . . . to cover a wide range of storage applications. Auto-erase for automatic display updating. A save control for 30 times longer viewing. Gated readout, which prevents the blooming that tends to occur between sweeps with nongated readout. Adjustable multi-trace delay for varying the crt view time prior to storing the next sweep when using FAST transfer mode.

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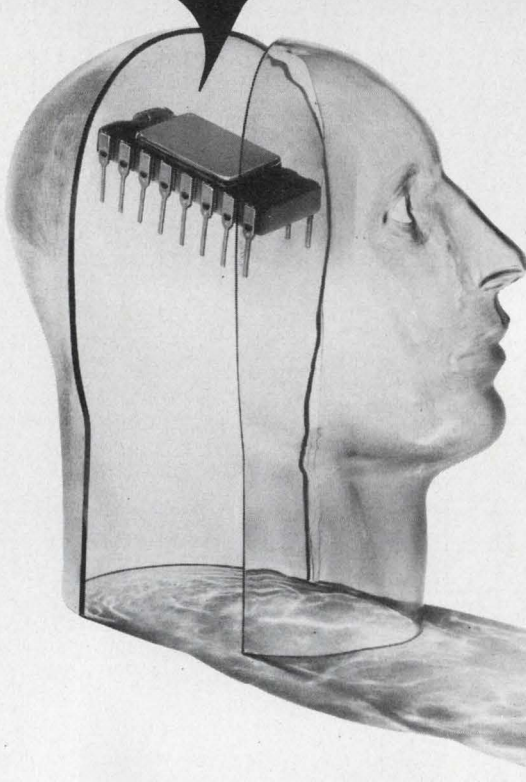
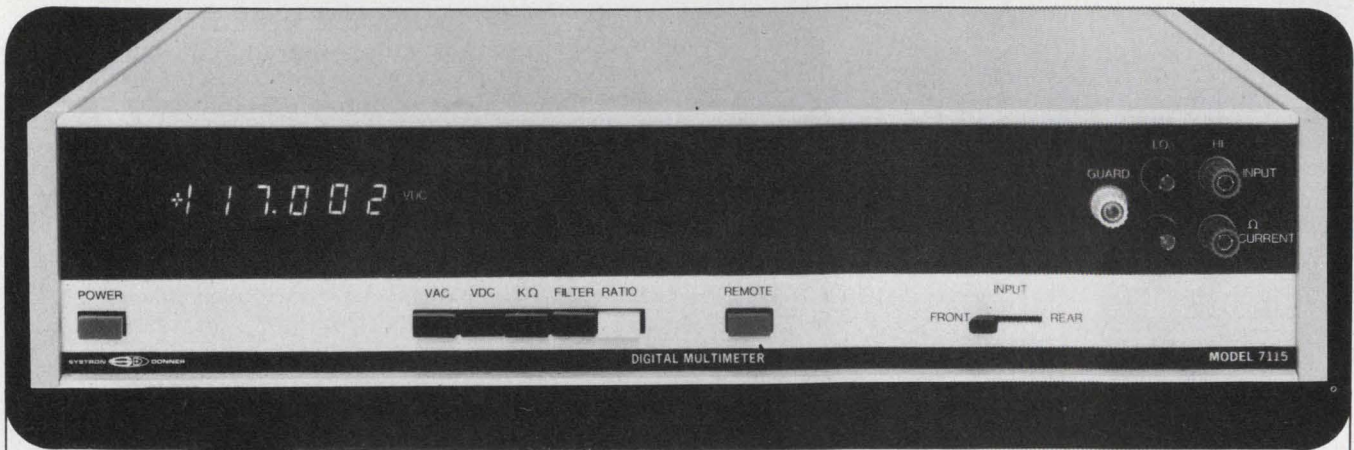
Future Expandability. The 7834 represents a breakthrough in oscilloscope technology. It follows the 7633 mainframe which introduced the then-highest stored writing speed of 1000 cm/ μ s. The 7B80 and 7B85 time bases, establishing a convenient delta delay measurement technique. The 7D01 Logic Analyzer and DF1 Formatter transforming the oscilloscope into a logic state—logic timing analyzer with a choice of 5 display modes.

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FOR TECHNICAL DATA CIRCLE # 289
FOR DEMONSTRATION CIRCLE # 290



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CIRCLE NUMBER 25

Microprocessor Design

Can you evaluate μ Ps by examining their register architecture?

Recently introduced μ Ps contain many more internal data registers than the earlier ones. Some of them have over 64 registers and are apparently very powerful. But often the number of registers is not as important as how easily the registers can be addressed and their data manipulated, according to one μ P vendor. So with differing considerations in mind, how does the user evaluate the different register architectures and decide which μ P to use? Opinions vary.

"The types of operations that you can perform on registers, through the instruction set, decides whether one set of registers is more useful than another," says Mark Eliot,

manager of applications at Zilog, Los Altos, CA.

"The simplest instruction would move data into and out of the registers. The Z-80 can move data to and from registers directly addressed as part of the instructions. Another instruction type permits registers to serve as pointers to memory—to hold addresses of memory locations.

"Other instructions let the registers perform ALU operations such as add, subtract, logic or increment," Eliot says.

"I think that evaluating μ Ps by looking at their registers is pretty much nonsense," retorts Lionel Smith, applications engineer at Intel,

(continued on page 36)

Industrial microcomputer system doubles as development tool

A microcomputer system that is flexible enough to do prototype development and still inexpensive enough to serve as an OEM industrial controller has been developed by Logical Services. At the heart of the Servant microcomputer system is an 8080A-based CPU.

Some key features of the Servant 8 system include a light pen and an oscilloscope-drive output in addition to a full complement of front-panel controls and indicators. The light pen and an oscilloscope make it possible to examine and modify the contents of registers and memory locations without the use of a terminal.

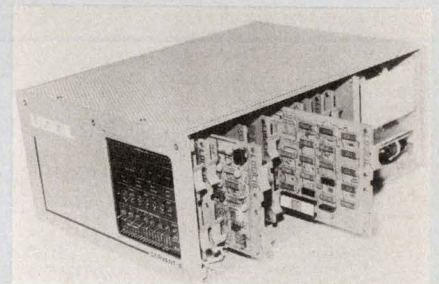
There are seven condition switches that allow breakpoint insertion in programs to permit examination of registers and memory locations.

Software for the operating system consists of a monitor program that can be automatically accessed when power is turned on. Also available are an assembler, a debug routine, a text editor and specialized macro and application programs.

Among the optional plug-in modules currently available are: a 16-channel analog input, 8-bit output circuit; an IEEE Standard ASCII bus interface; and a universal breadboard that permits customization.

Price of the basic development system, which includes the CPU, control panel, 4-k RAM, a TTY interface, chassis and ROM software, is \$2495. Individual module prices start at \$50 for the breadboard card and go up to \$350 for the control panel card. Delivery of all units is from stock.

Logical Services Inc., 711 Stierlin Rd., Mountain View, CA 94043. (415) 965-8365.



MICROPROCESSOR DESIGN

(continued from page 35)

Santa Clara, CA.

"The only way you can really evaluate what an architecture can do for you is to try it out on some applications. A machine that has lots of internal memory is a beautiful machine if your applications require it," Smith adds.

"But if you have to go to external locations, and you don't have the addressing modes to get at the data, you are going to end up with a cumbersome system."

On the other hand, he says, "A machine that has a lot of addressing capability and registers but needs to access only a few variables would be a case of overkill. I don't think there is any way of just looking at register architectures and coming to a decision based on that alone."

CMOS μ P comes in a console with display and keyboard



Now you can get RCA's CMOS μ P in a console with a hexadecimal keyboard and four-digit LEDs for inputting and displaying data. The console, dubbed the UC1800 from Infinite, Inc., is available in kit form (\$249.95) or assembled (\$495). The unit consists of a separate CPU board and display, keyboard, and switch control modules that plug together with flat cables.

The 5.5 \times 8.5 in. CPU board contains the μ P, all control logic, a regulated power supply, and a 72-contact rear-edge connector for system expansion.

The display module contains a voltage regulator, decoder and the seven-segment LED readouts. It measures 6.75 \times 2.75 in.

The keyboard model contains hex keyswitches and encoding logic. The switch module contains additional pushbutton switches that control the UC1800.

With the console, you get a 200-page manual and debug software so you can examine memory and modify programs.

*Infinite, Inc., Dept. INR, P.O. Box 906, 151 Center St., Cape Canaveral, FL 32920.
(305) 783-9600.*

CIRCLE NO. 507

New bipolar chip eases system interrupt control

Hardware control of the priority interrupt inputs to a microprocessor system are now possible with a new bipolar LSI chip introduced by Motorola. The device, called a Priority Interrupt Controller (PIC), eliminates the software interrupt-polling routine in systems containing eight or multiples of eight I/O devices.

Functionally, the PIC can change the interrupt vector, reserved in memory for hardware interrupts, into one of eight alternate vectors assigned to the I/O service routines. It modifies the low-order bytes of the reserved interrupt address. The second, third, fourth and fifth LSBs of the system address bus are used as inputs to the PIC; a bit pattern of 1100 (5th LSB to 2nd LSB, respectively) is required to initiate the vector translation.

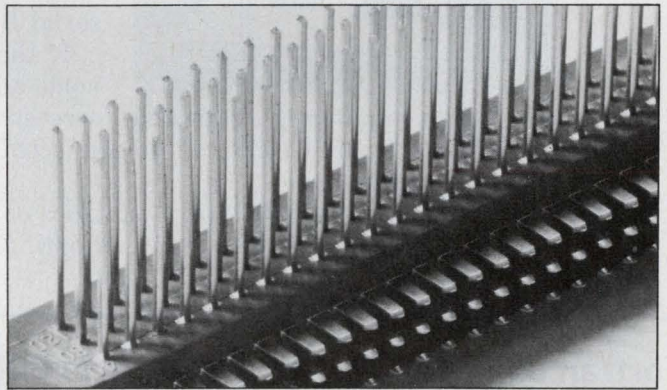
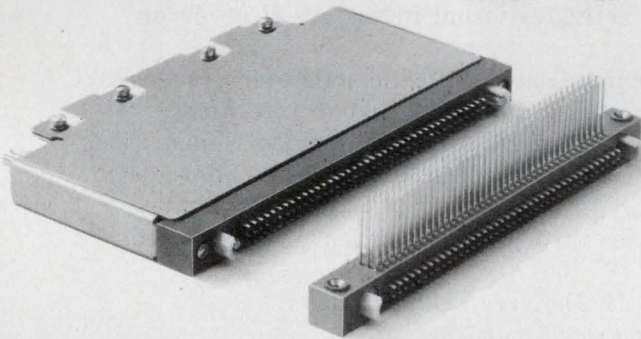
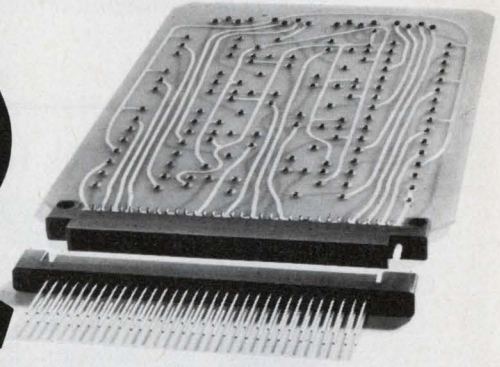
The interrupt output of each I/O device is normally connected to one of eight prioritized latching inputs on the PIC. When enabled, each interrupt will cause a unique bit pattern to be generated and substituted for the 5th through 2nd LSB of the original interrupt vector. These eight alternate vectors are used to start the interrupt subroutines for the I/O devices.

A mask, which is programmed via the 5th through 2nd LSBs of the address bus, can be used to inhibit any or all of the interrupts at the eight inputs.

An output from the PIC, called the $\overline{\text{STRETCH}}$ signal, is available to lengthen a system clock cycle when accessing slow memories. When unselected, the PIC is transparent on

(continued on page 38)

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CIRCLE NUMBER 26

MICROPROCESSOR DESIGN

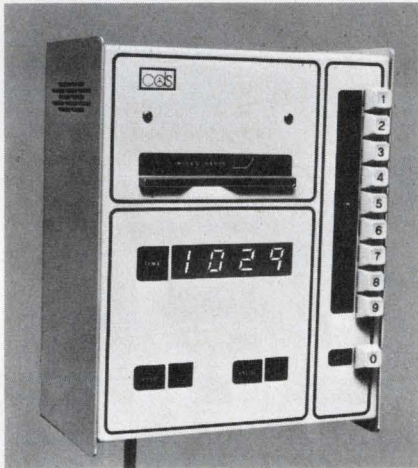
(continued from page 36)

the address bus and will not affect the reserved interrupt vector. The PIC is offered in both ceramic and plastic 24-pin DIPs; the price is \$7.50 (100-999 qty.) for the plastic version.

Motorola Semiconductor Products, Inc., P.O. Box 20294, Phoenix, AZ 85036. (602) 962-2151.

CIRCLE NO. 508

μ P-controlled time clock remembers data until queried



A 6800 μ P-controlled time clock keeps track of employee attendance and other information, then relays the data to a central computer.

The Smart Clock first reads up to 16 digits of Hollerith-coded data from an employee's plastic ID badge or IBM card. Then the employee punches in five more digits via pushbuttons. The terminal stores this information, as well as the time, in its own battery-powered memory. It checks each transaction for validity, sounds an alarm and activates visual indicators if an error has occurred.

The unit communicates with the computer via RS-232C serial lines or with a 600-baud modem interface.

If the central computer breaks down, the Smart Clock holds all the accumulated data, up to 14,000 characters,

until the computer is again able to receive data.

Up to 64 Smart Clocks can be connected in series through one RS-232C, ASCII-coded, 20-mA current loop.

The unit price is \$1600 for quantities of 10 to 24. Delivery takes 45 days. Coastal Data, 1592 N.W. 159 St., Miami, FL 33169. (305) 625-7123.

CIRCLE NO. 509

Fortran compiler does its thing on an 8080 system

A Fortran compiler is reportedly the first to be resident on an 8080 system. The FORT/80 compiles a subset of ANSI Fortran IV, which produces 8080 machine-language object code.

It requires 16 kbytes of memory: 12 k for the compiler and the remainder for work space.

The object code produced by the FORT/80 can be linked to additional machine language subroutines to make a complete program.

Symbolic names containing 1 to 31 characters may be used. However, only single and double-byte integer arithmetic is permitted.

A library of useful subroutines and functions comes with the compiler, including absolute values (ABS), random 8-bit numbers (RANDU), and the square root of positive and SQRT integers (SQRT).

The software is supplied either on a floppy disc or on paper tape, and costs \$750.

Unified Technologies, Inc., 4800 Dundas St. W., Suite 209, Islington, Ont. M9A 1B1. (416) 236-1159.

CIRCLE NO. 510

Micro Capsules

A new version of a popular software language, called Basic Etc., is optimized for business and game programming. It comes from Binary Systems Inc., Richardson, TX. . . . An 8-bit μ P that contains ROM, RAM, I/O and clock chip will be introduced by General Instruments, Hicksville, NY. The PIC-1650 fits in a 40-pin DIP. . . . A \$60 prototyping kit from Intel Corp., Santa Clara, CA, contains chips for a 4-bit system. It has a 4040 μ P, 4269 keyboard/display interface, and EPROM, RAM and I/O chips.

DARLINGTON

POWER TRANSISTORS

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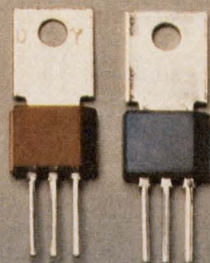
NPN - HIGH GAIN - 1/2 AMPERE

GE TYPE	P_T $T_C = 25^\circ\text{C}$ Max. (W)	V_{CE0} Min. (V)	h_{FE} @ 5V, 200 mA		COMMENTS
			MIN.	MAX.	
D40C1	6.25	30	10,000	60,000	<ul style="list-style-type: none"> • Very High Gain - 60k typical; High input impedance - 50k ohm typ; 1.2 watts P_T @ 25°C ambient. • Applications: IC Interface audio output, touch switch, oscillator, buffer, high power transistor driver, relay replacement.
D40C2	6.25	30	40,000	-	
D40C3	6.25	30	90,000	-	
D40C4	6.25	40	10,000	60,000	
D40C5	6.25	40	40,000	-	
D40C7	6.25	50	10,000	60,000	
D40C8	6.25	50	40,000	-	



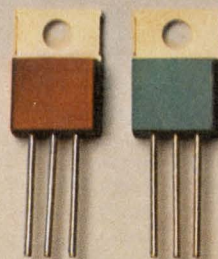
COMPLEMENTARY - 2 AMPERES

GE TYPE		P_T $T_C = 25^\circ\text{C}$ Max. (W)	V_{CE0} Min. (V)	h_{FE} @ 5V, 200 mA MIN.	COMMENTS
NPN	PNP				
D40K1	-	10	30	10,000	Typical Applications: <ul style="list-style-type: none"> • IC Interface • Driver • Regulator • Touch Switch • Lamp Driver • Audio Output • Relay Substitute • Servo-Amplifier • TO-202 Package
-	D41K1	10	-30	10,000	
D40K2	-	10	50	10,000	
-	D41K2	10	-50	10,000	
-	D41K3	10	-30	10,000	
-	D41K4	10	-50	10,000	



COMPLEMENTARY - 10 AMPERES

GE TYPE		P_T $T_C = 25^\circ\text{C}$ Max. (W)	V_{CE0} Min. (V)	h_{FE} @ 5V, 5 Amps MIN.	COMMENTS
NPN	PNP				
D44E1	-	50	40	1000	Typical Applications: <ul style="list-style-type: none"> • IC Interface • Relay and Solenoid Driver • Regulator • Inverter Power Supply Switch • Audio Output • Relay Substitute • Oscillator • Servo-Amplifier • TO-220AB Package
-	D45E1	50	-40	1000	
D44E2	-	50	60	1000	
-	D45E2	50	-60	1000	
D44E3	-	50	80	1000	
-	D45E3	50	-80	1000	



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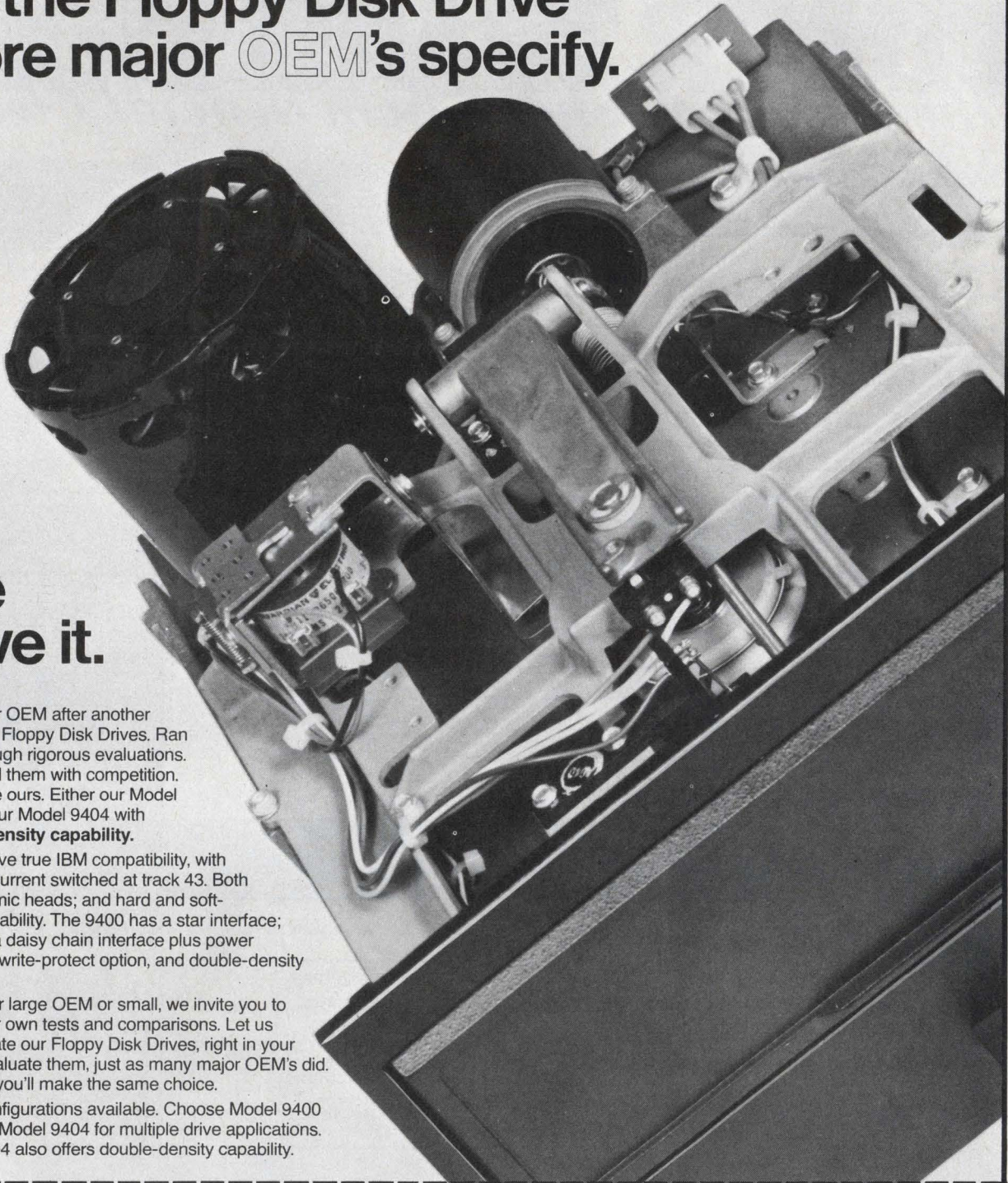
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Whether large OEM or small, we invite you to make your own tests and comparisons. Let us demonstrate our Floppy Disk Drives, right in your facility. Evaluate them, just as many major OEM's did. We know you'll make the same choice.

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Today we
supply the spark
for America's
defense.

Connections were much simpler 200 years ago. Torch the fuse and the cannon fired.

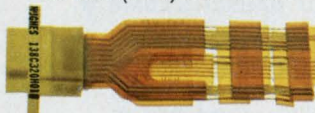
Supplying the vital spark that makes a modern weapon system do its job is a lot more complicated.

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Our high-rel connections have to be the best. They're used in systems like Phoenix, Maverick, Lance, Minuteman, AWACS, F-14, F-15, Space Shuttle, Viking, Sonobuoy, F-4, A-7, Condor, Standard Missile, F-18, AAH, Cruise Missile, F-8, Trident, Hobo, Sprint and many more.

To learn how we can serve your interconnection needs, contact Jack Maranto or Dave Cianciulli: Hughes Connecting Devices, 17150 Von Karman Ave., Irvine, CA 92714.

Or call (714) 549-5701.

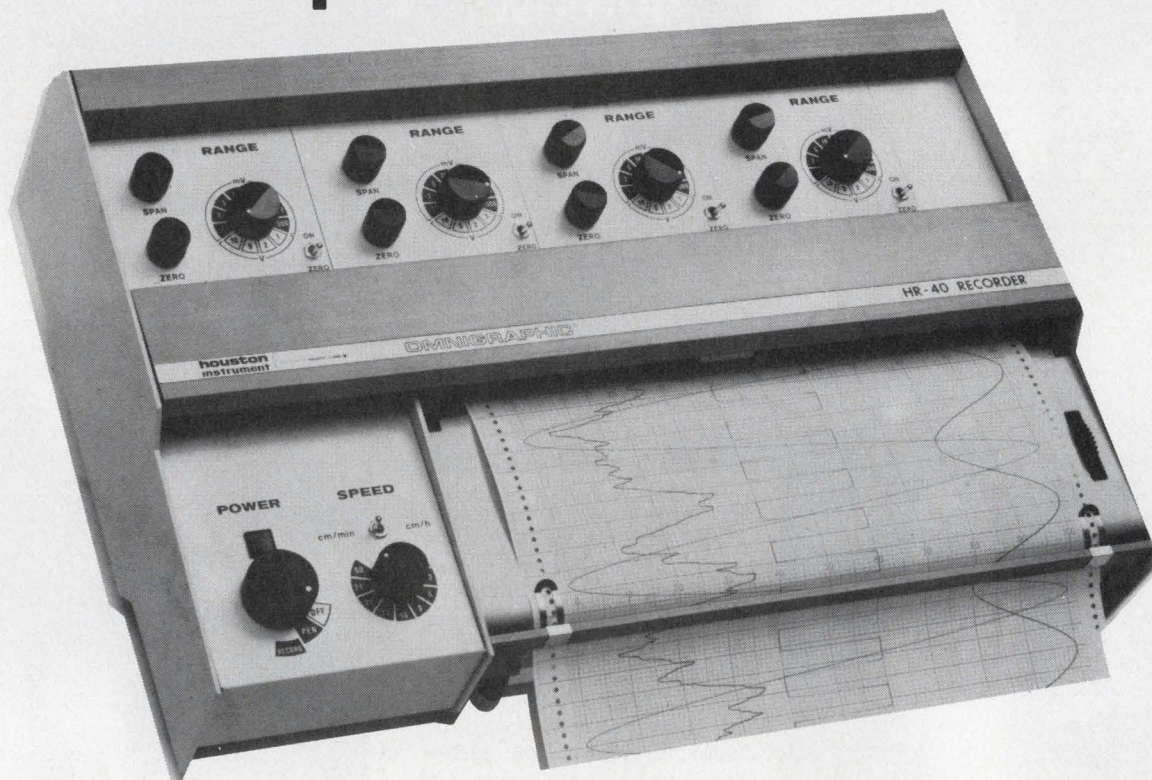


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CIRCLE NUMBER 29

HR-40

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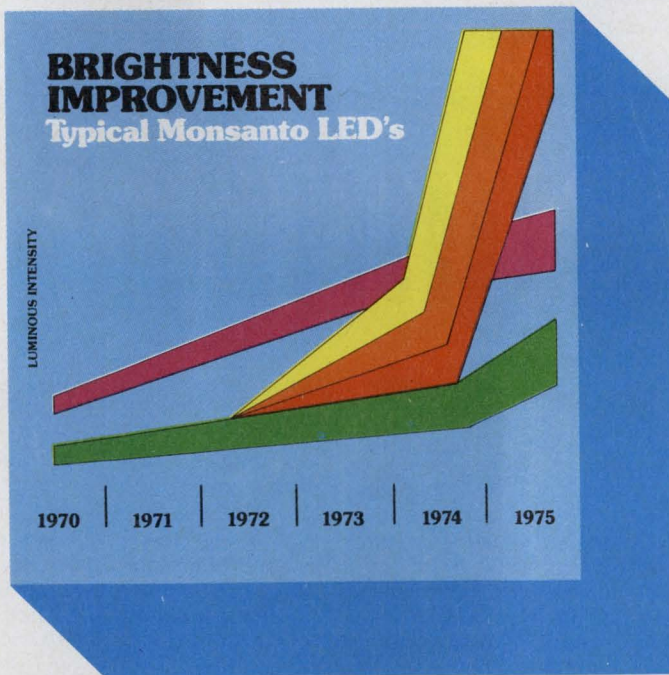
"the recorder company"

O.K., you guys, back to the old drawing board.

Just when you've made all your panel lamp decisions Monsanto comes along with LED lamps so light-efficient, with choice of color, that you'll have to take another look. They'll give you the same light with less power, or more light with the same power — whichever will do your application the most good.

They're the result of our patented nitrogen doping process for GaAsP on GaP substrates. We don't think you can find a better LED lamp, anywhere.

They come as T-1 and T-1 $\frac{3}{4}$ replacement lamps in standard red, bright red, green, yellow and orange. All those colors will give you great flexibility in design. And you'll get still more flexibility from their two lens choices and two lead lengths.



Model Number	Color	Size	Luminous Intensity	Viewing Angle
5174B*	Orange	T-1	5.0 mcd	90°
5274B*	Green	T-1	1.0 mcd	90°
5374B*	Yellow	T-1	4.0 mcd	90°
5774B*	Red	T-1	5.0 mcd	90°
5152**	Orange	T-1 $\frac{3}{4}$	40.0 mcd	28°
5252**	Green	T-1 $\frac{3}{4}$	15.0 mcd	28°
5352**	Yellow	T-1 $\frac{3}{4}$	45.0 mcd	28°
5752**	Red	T-1 $\frac{3}{4}$	40.0 mcd	28°

*Models are also available with 1" lead lengths, low profile (.138" high) lens, or 180° viewing angle.

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It used to be that some sockets demanded filament lamps in spite of their failure and replacement problems. But now you may find all the brightness you need in our long-life LED lamps.

In short, Monsanto LED's can add value to your product. Because of their long life, high reliability, and low power requirements.

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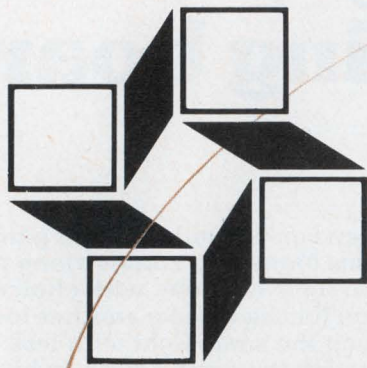
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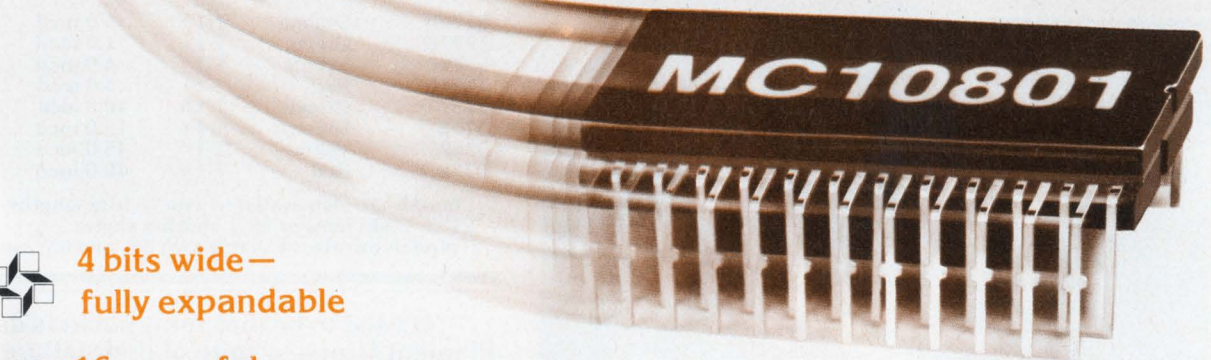
ED-1 © Monsanto Company Electronics Division, 1976

CIRCLE NUMBER 31



M10800

The world's fastest LSI processor family introduces...



**4 bits wide—
fully expandable**



**16 powerful
microinstructions**



Control cycle 52 ns[†]



**4 on-chip
subroutine levels**



**Instruction or
subroutine repeat**



**Standard MECL* LSI
from the ECL leader**



**8 on-chip registers —
including expandable
4 X 4 LIFO**

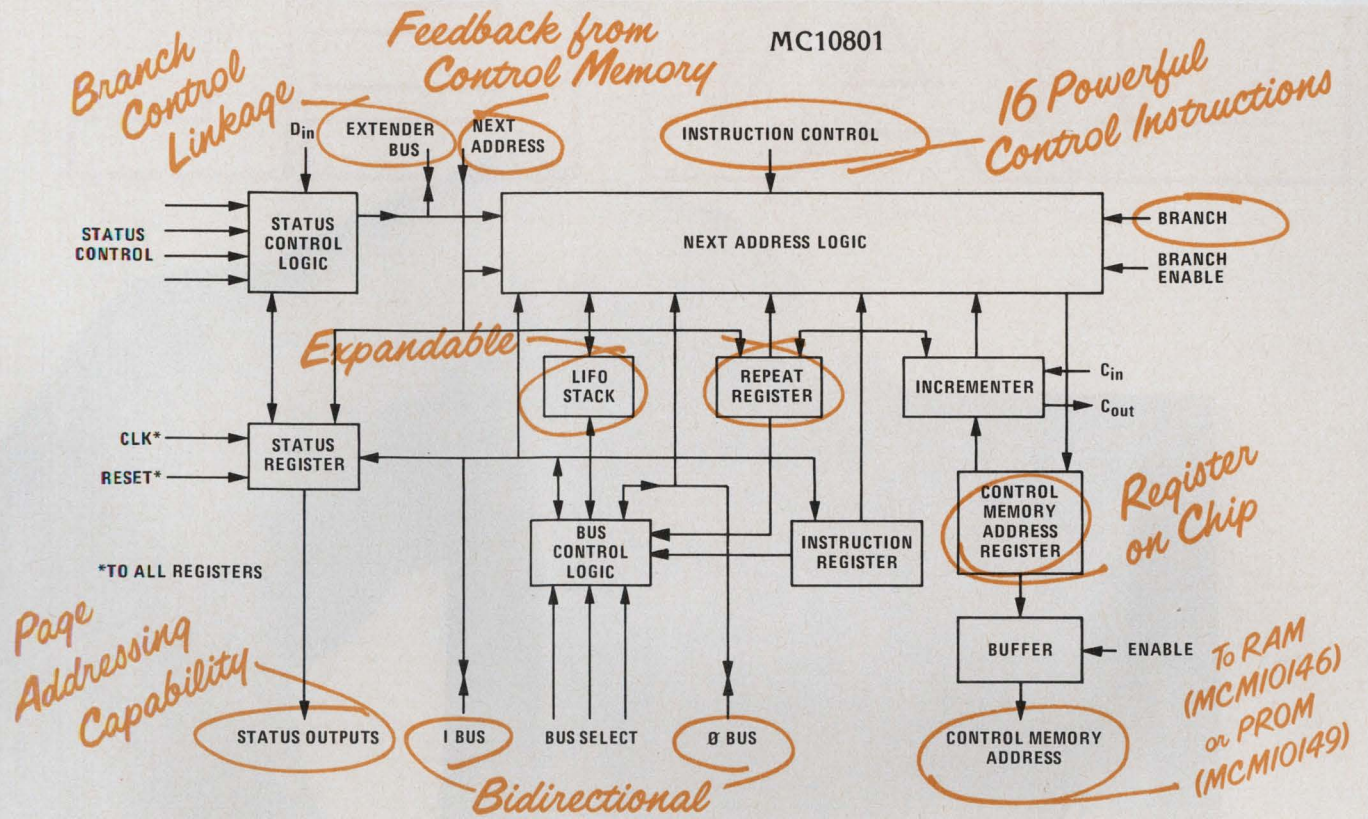
Speed alone would place the MC10801 in a microprogram controller class by itself, but with this remarkable MECL LSI building block, speed is just the beginning.

Its 16 microinstructions and on-board registers make the MC10801 the most powerful microprogram controller as well as the fastest. Maximum system flexibility is ensured by five data ports. Generation of the next control memory address is possible from any of seven different sources; either I or O bidirectional bus, next address field, incrementer, either repeat or instruction register, or LIFO stack.

When the MC10801's four

on-chip subroutine levels are not sufficient, expanding the LIFO stack via the I and O buses accomplishes nesting of more than four levels.

And there's still more. The repeat register permits big savings in control memory, particularly in large multiply or divide routines. Repeat capability for an instruction or subroutine is 2^{4n} , with "n" as the number of 10801s in the system. So with just two, you get 256 repeats. The number 256 points out another MC10801 feature, Page Addressing. Using the status register, multiple pages of 256 words can be addressed,

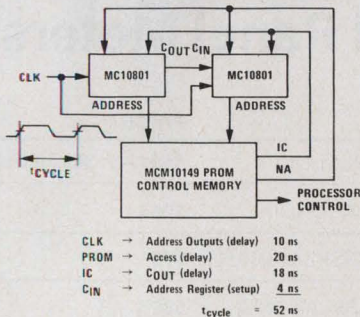


the world's most powerful microprogram controller.

†Control Cycle Speed Calculation

(logic delays - typical)

The MC10801 is the fastest microprogram controller by any measure, but nothing demonstrates that fact better than a system speed calculation like this.



again with only two units in most systems.

We could go on, but you get the idea. Just a final word about

M10800 Family Product Availability

MC10800	Now
MC10801	Now
MC10802	2nd Qtr '77
(Timing Function)	
MC10803	1st Qtr '77
(Memory Interface)	
MC10805	2nd Qtr '77
(Bus Translator)	
MC10806 (32 X 9 Dual Addressable Register)	2nd Qtr '77
MC10808 (Expandable 16-Bit Shifter)	2nd Qtr '77

prices. Our introductory MC10801 price (100-up) is just \$50.00, and we've already been able to cut our MC10800 price 40%, to \$30.00.

Whether your processor application is in disk controllers, radar and guidance, video or speech processing, minicomputers, signal processing, or whether you simply want to emulate your favorite instruction set... the performance of the MECL LSI M10800 Family mandates your consideration, now.

MC10801 Control Instructions

- INC - Increment
- JMP - Jump to N.A. Inputs
- JIB - Jump to I Bus
- JIN - Jump to I Bus and Load Instruction Register
- JPI - Jump to Primary Instruction Register
- JEP - Jump to External Port (O Bus)
- JL2 - Jump to N.A. Inputs and Load Instruction Register
- JLA - Jump to N.A. Inputs and Load Address into Repeat Register
- JSR - Jump to Subroutine
- RTN - Return from Subroutine
- RSR - Repeat Subroutine
- RPI - Repeat Instruction
- BRC - Branch to N.A. Inputs on Condition otherwise Increment
- BSR - Branch to Subroutine on Condition otherwise Increment
- ROC - Return from Subroutine on Condition otherwise Jump to N.A. Inputs
- BRM - Branch and Modify Address with Branch Inputs (Multiway Branch)

For data, circle the reader service number or write to Motorola Semiconductor Products, Inc., P.O. Box 20912, Phoenix, AZ 85036. For real action, contact your favorite authorized Motorola distributor or Motorola sales office.



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DM-350A1	3-1/2	115/230 VAC	UNIPOLAR, XFMR-ISOLATED, DISPLAY ONLY	\$79
DM-350A2	3-1/2	115/230 VAC	BIPOLAR, XFMR-ISOLATED, DISPLAY ONLY	\$89
DM-4000	4-1/2	+5VDC @ .6A	OPTOISOLATED RATIOMETRIC AUTO ZERO XTAL LINE FILTER	\$219 less BCD \$239 with BCD
DM-4300	4-3/4	+5VDC @ .6A	OPTOISOLATED RATIOMETRIC AUTO ZERO XTAL LINE FILTER	\$235 less BCD \$255 with BCD
DM-2000AR	3-1/2 DIGITS AUTORANGING OVER 3 DECADES	+5VDC @ .8A	AUTOMATIC RANGING OVER $\pm 200\text{mV}$, $\pm 2\text{V}$ $\pm 20\text{V}$ FULL SCALE	\$169 less optoisolation \$218 with optoisolation



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CIRCLE NUMBER 33

The old man at the bar

Jack and Charlie were having one or two while watching the old-timer drink his lunch. "What do you suppose keeps that guy going?" Jack wondered aloud. "He's at least 80." "Well," Charlie began, pausing half a second to give the question the cogitation it deserved, "it's got to be the booze. Look at him. He's just finished his fourth martini, and he's still going strong." Then, getting philosophical, Charlie added that contrary to the advice of people concerned with health—even doctors—alcohol keeps you young. The living proof (80, at least) was lunching (or lurching) at the end of the bar.



"I don't know," Jack mused. "I think it's the womanizing. Heck, that guy's here every day with a different gorgeous gal. That's got to keep a guy going. It would keep *me* going."

"No," Charlie asserted. "It's got to be the smoking. I've never seen a guy smoke so much. He burned up half a dozen cigarettes in the last hour, and now he's on his second cigar. I guess tobacco must keep you young."

Before the discussion was allowed to die, Charlie approached the old gentleman. "Excuse me, pop," he said graciously. "To what do you attribute your venerable age?" And when the man muttered, "Well, son, mainly to the fact that I was born so long ago," Charlie chuckled, then tried again. "I mean, old-timer, how old are you?"

"I'm 29," the old man wheezed.

Well, everybody got a large charge out of the story when Bill told it at lunch. But some began to wonder if we don't all make similar mistakes. Too often we spend our time developing plausible theories for facts before the facts are all in. We try to discover *why* a circuit behaved a certain way before we determine *if* the circuit behaved that way. We sweat out the solution to a problem only to discover that the problem never existed. So we end up doing penance for sins that haven't been committed. And we offer theories to explain why Joe did something when, in fact, he didn't.

Jumping to conclusions is risky business.

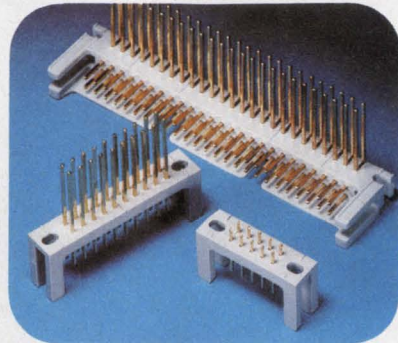
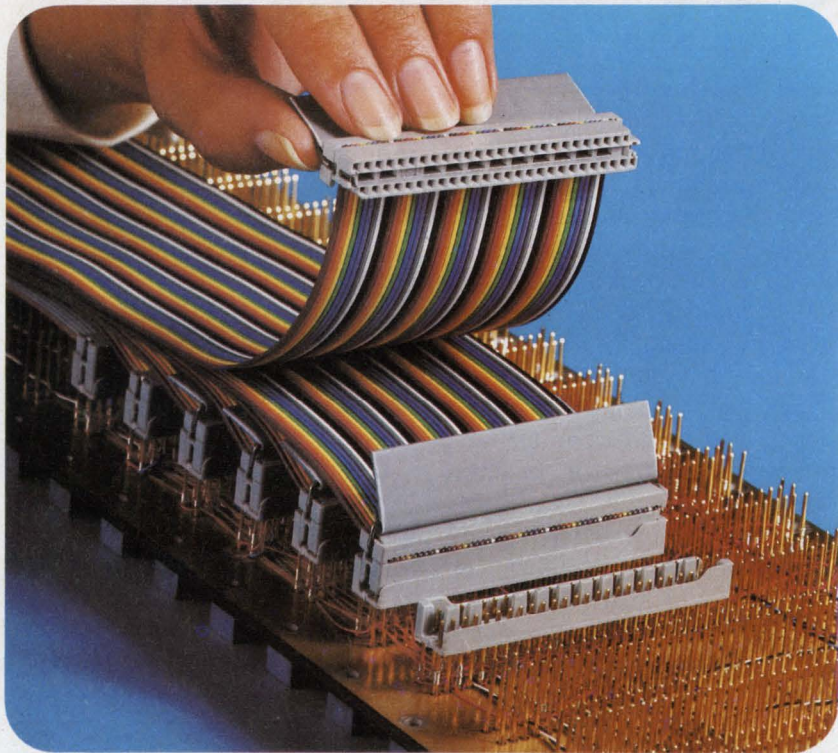
GEORGE ROSTKY
Editor-in-Chief



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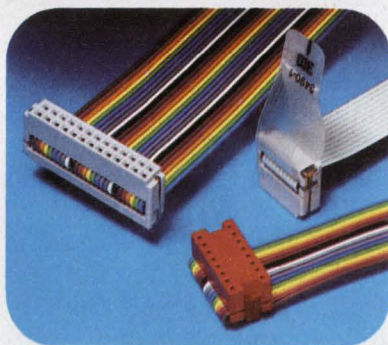
Want simpler backplane connections? Come to the source.



There are several more things you can get only from 3M. The broadest range of flat cables and complete system components. Best off-the-shelf availability. Proven performance. And the unmatched experience of the people who pioneered this reliable mass termination system.

"Scotchflex" is a registered trademark of 3M Co.

Now, a unique Scotchflex brand Socket Connector and Keying Header system lets you interface directly with backplane wire wrap pins and provides for easy, positive polarization and keying. The header design allows for thousands of unduplicated polarizing combinations without loss of backplane pins. The 50-position connector mates with .025" square pins on .100" x .200" grid spacing. Header allows space for and protects two layers of wrap below it. System also provides polarizing keys and strain relief handles.



Need some other ways to simplify wiring and increase circuit density? 3M's Scotchflex line offers you a broad choice of mass terminating socket connectors, plus wire wrap or solder tail headers to suit your specific design problem. Keying capability is also provided.

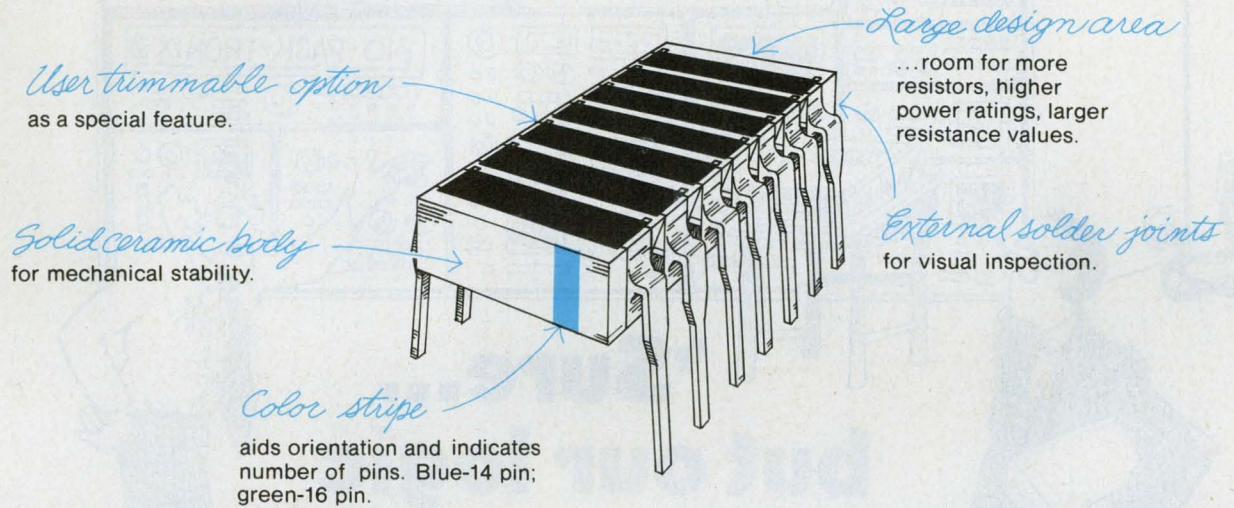
Scotchflex[®] systems from 3M. The source.



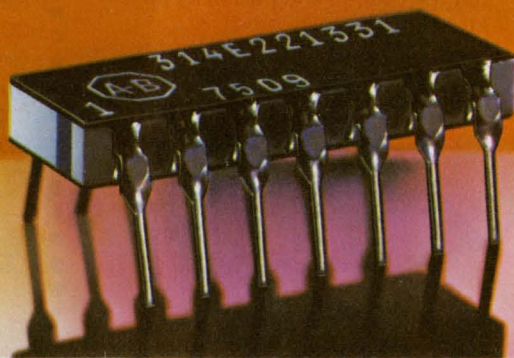
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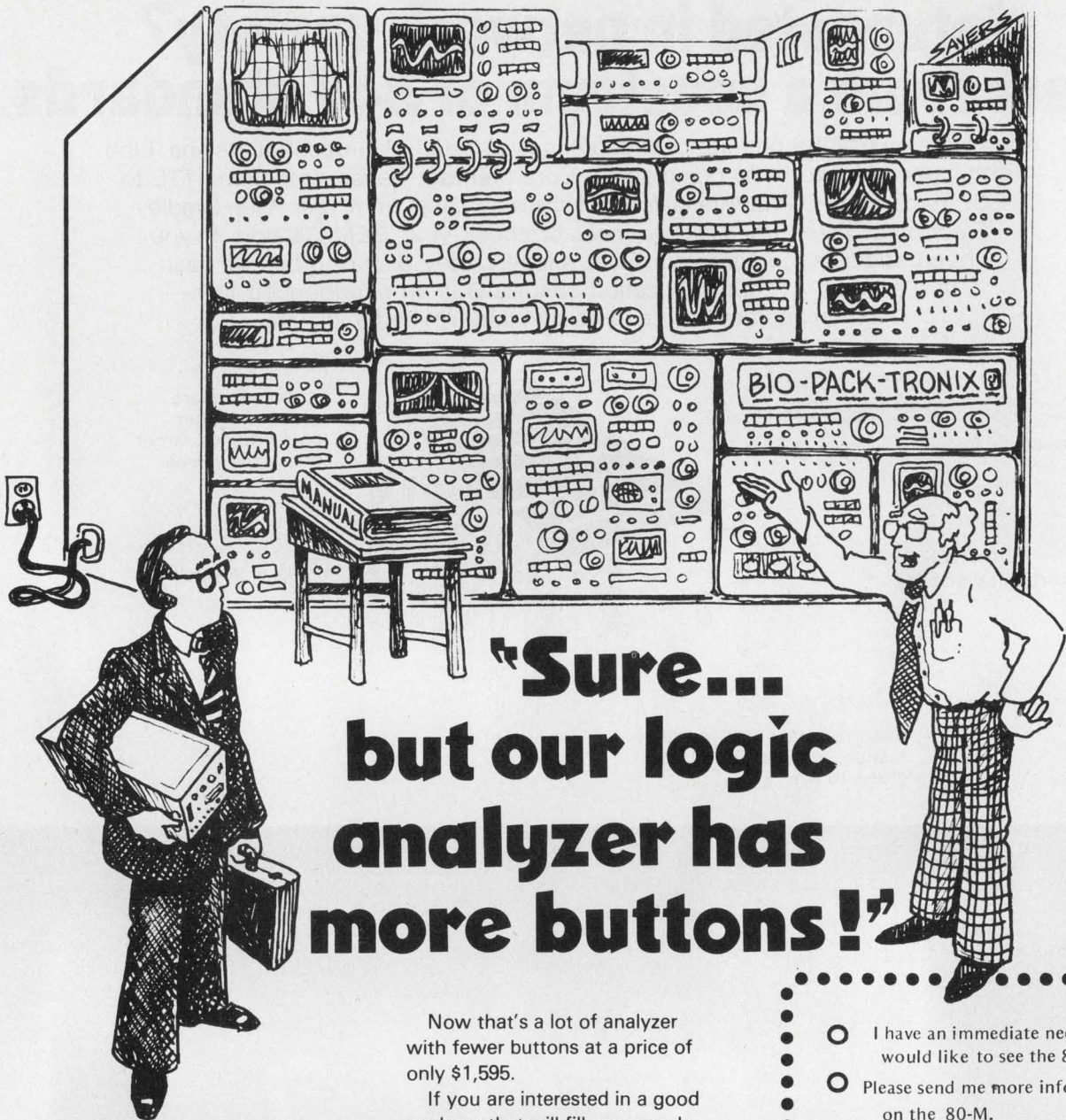
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CIRCLE NUMBER 191

EC111



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but our logic
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True, but more buttons do not make a better analyzer. The 80-M Logic Analyzer from Digital Broadcast Systems can do many of the things the more expensive analyzers can do, such as, "snap shot" eight channels of digital logic, store the information in a 1K per channel memory and play it back on your scope or CRT. The 80-M has spike detection, real time and memory operation, eight bit word recognition, 10MHz operation and much more.

Now that's a lot of analyzer with fewer buttons at a price of only \$1,595.

If you are interested in a good analyzer that will fill your needs with easier operation, circle the reader service card number or fill out the coupon and mail to us for faster response.



- I have an immediate need and would like to see the 80-M.
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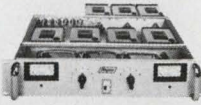
CIRCLE NUMBER 192

POWER MINI'S FOR LOGIC OR OP AMPS



Terminal strip input/output connections on these miniature power modules eliminate the need for sockets or soldering. They mount in an area only 3.5" x 2.5". Ratings: 5 volt models to 2.5 amps, 15 volts to 5 amps. Other models from 1 to 75 volts, all with 3-day shipment guaranteed.

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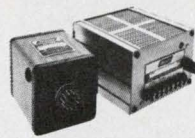
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For applications requiring power supply with unusually high isolation, such as for powering strain gage or other transducer circuits, Acopian offers models with ratings from 5 to 36 volts. Input-output isolation: 10,000 meg-ohms minimum, 1 pF maximum. Guaranteed 3-day shipment.

POWER FOR RELAYS AND DISPLAYS



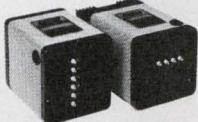
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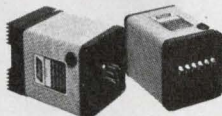
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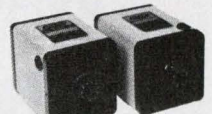
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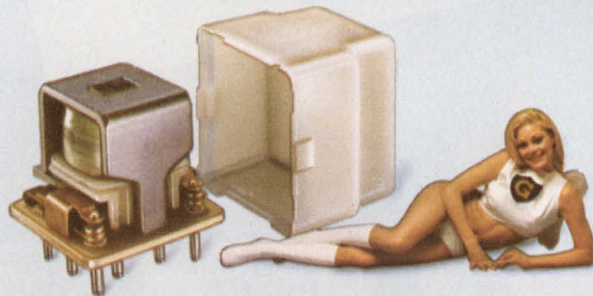


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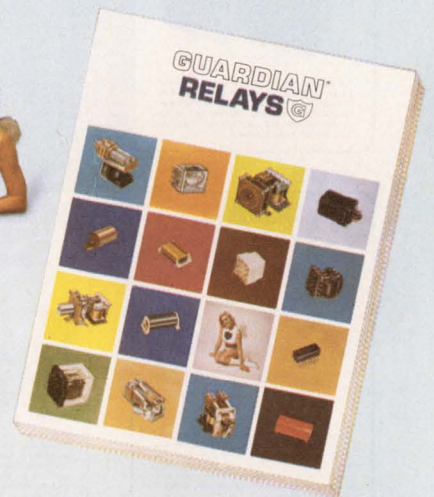
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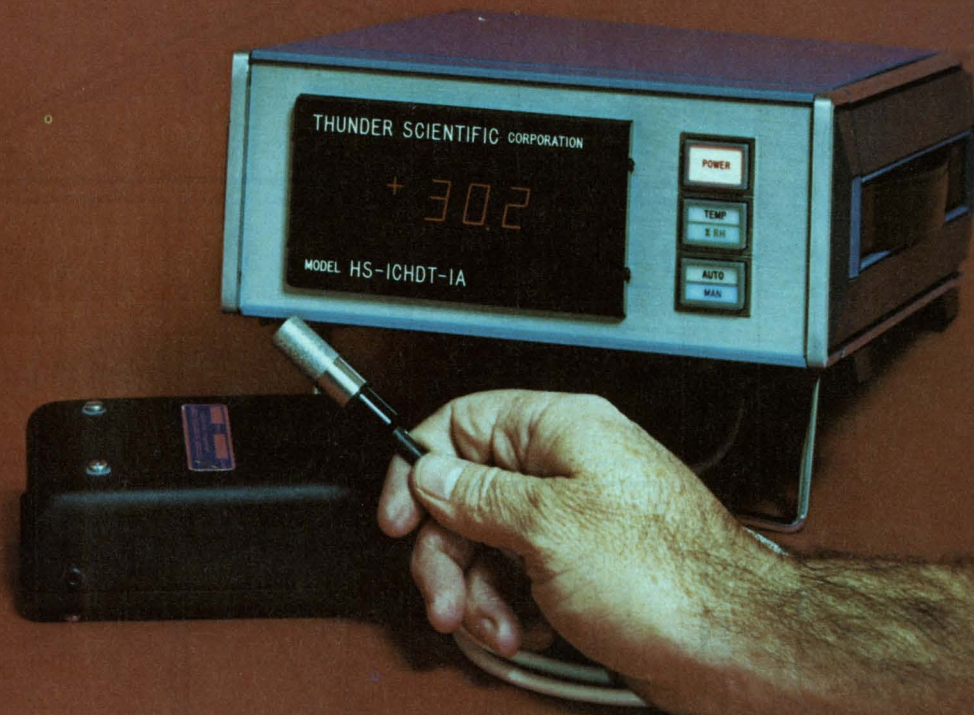


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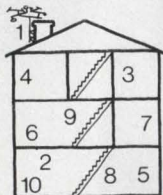
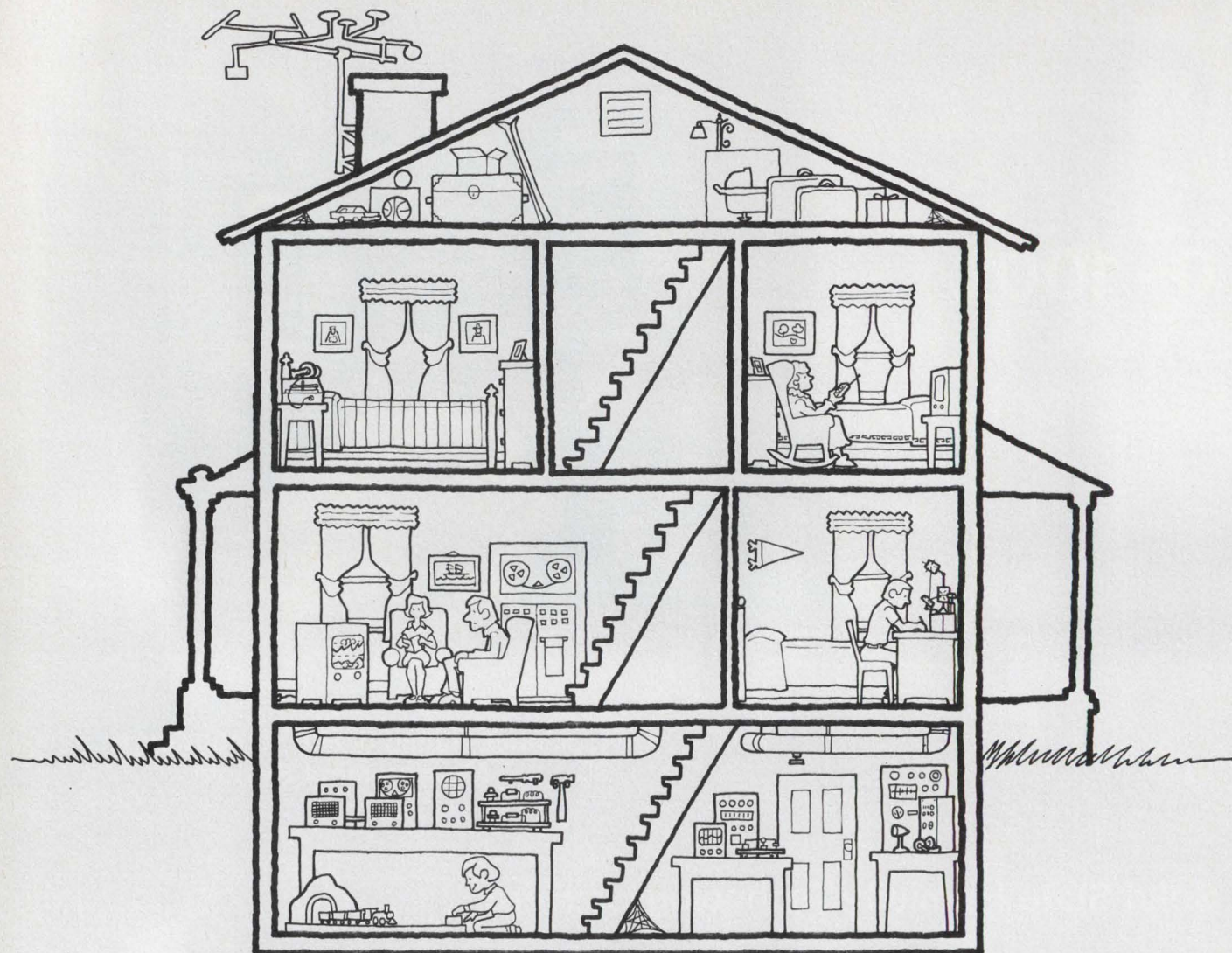


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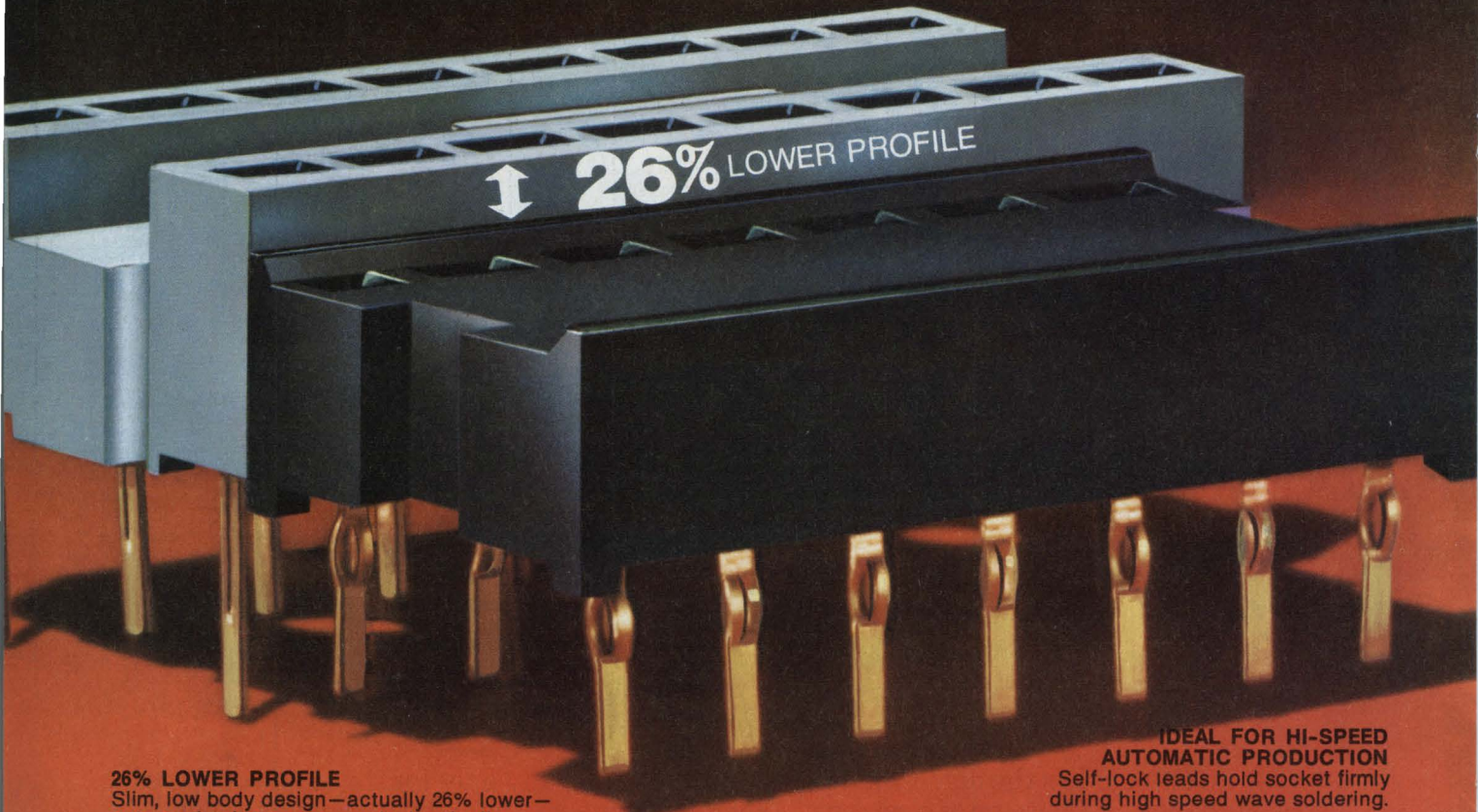
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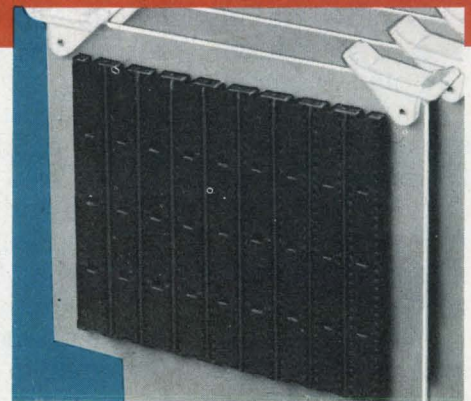
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CIRCLE NUMBER 35

INSTRUMENTS '76



**Today's instruments
are smart,
versatile
and safe**

Contents

Brainy instruments are taking top honors with computer power that boggles the mind	52
Portable instruments: The specifications are fine, but their batteries are still short-lived	60
Howard Vollum, Bill Peek and William Velsink of Tektronix speak on the future of scope	68
The IEEE 488 bus is playing an important role in programmable instrument systems	76
A combined instrument is one that often provides capabilities that exceed the sum of its parts	88
Ulrich L. Rohde of Rohde & Schwarz speaks on European and American engineers	96
Calibration devices are better because the basic standards are more precise	104
Instruments designed with safety in mind may be hazardous to your health	114

Smart instruments may have arrived, but they have brought problems with them. One of these is pinning down a definition of what smart means. To some a smart instrument means one that has memory, while to others it means the unit has a calculator chip or a microprocessor in it.

But a "brainy" instrument is not necessarily better than its "dumb" predecessor. Like the 21-transistor radio that used transistors for everything from diodes to resistors, instruments often contain a microprocessor simply for its promotional value.

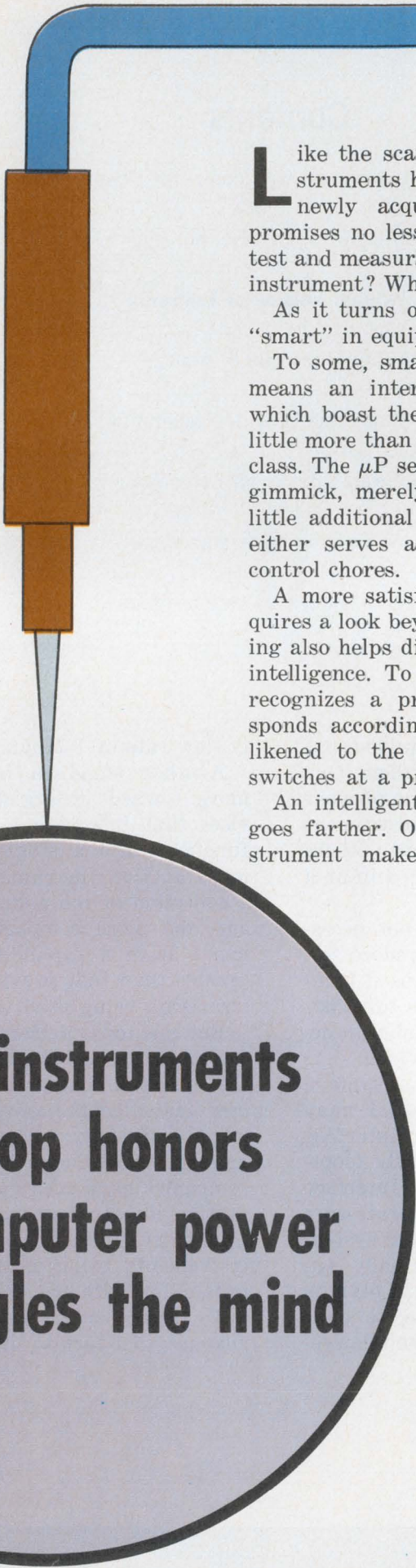
But some instruments *do* take advantage of the added power a μP affords. And many of these use the μP to provide an interface between the instrument and the newly adopted IEEE Standard 488 Digital Interface Bus. The combination of microprocessors and the 488 bus is leading to a total system capability far beyond that originally envisioned for the bus. For example, it permits distributed computing systems to be built where processing can be done at the relative-

ly slow rate of 1 Mbyte/s.

Another trend in instrumentation is a move toward synergistic instruments, devices that integrate a variety of different functions into a single unit. Unlike other multifunction instruments that are simply a collection of individual units in one package, the more compact synergistic instruments have a capability that is generally greater than that provided by individual instruments being used together.

But are today's instruments safe? Manufacturers are going all out now to answer that question. The first thing one notices on new instruments is warning labels everywhere, especially where there is high voltage or even where there might be. Some companies have even gone to the extreme of putting illuminated warning labels on their equipment. These are particularly helpful on instruments being used by someone who is unfamiliar with the equipment.

To really appreciate these instrument changes, just turn to this special section.



Brainy instruments take top honors with computer power that boggles the mind

Like the scarecrow in the Wizard of Oz, instruments have finally acquired a brain. The newly acquired smartness or intelligence promises no less than to revolutionize the entire test and measuring industry. But what is a smart instrument? What is an intelligent one?

As it turns out, it's just as difficult to define "smart" in equipment as it is in people.

To some, smart means memory. To others, it means an internal μP . Yet some instruments, which boast the use of those ICs, appear to do little more than conventional instruments of their class. The μP seems to be there strictly as a sales gimmick, merely to replace existing logic, with little additional benefits. In other cases, the μP either serves as an interface or does internal control chores.

A more satisfying definition of smartness requires a look beyond form to function. Such probing also helps distinguish between smartness and intelligence. To some, then, a smart instrument recognizes a preprogrammed situation and responds accordingly. Smart, in this case, can be likened to the on-off response of a relay that switches at a predefined level.

An intelligent instrument, on the other hand, goes farther. One viewpoint: An intelligent instrument makes decisions based on previous actions; it can manipulate information, crunch numbers, then choose an action based upon the results.

More than a few instrument designers see programmability as a key aspect of smartness—that is, the equipment can go through a sequence of operations under external control. For example, a user can "key-board in" numbers and tell the smart equipment to use the values in one of several ways. Or the human operator can be replaced by a minicomputer or some other controller.

The impact of microprocessing

Features like self-diagnosis, automatic calibration, autoranging and automatic zero don't necessarily make a machine

Stanley Runyon
Senior Associate Editor



Slide the calculator-like keyboard out of the front panel, and you'll know immediately that the Dana 9000 is dif-

ferent. The world's first microprocessing timer/counter measures at the push of a button.

smart. These functions were around when μ Ps weren't. And in spectrum analyzers, at least, arithmetic with standard TTL logic predates the LSI microprocessor concept.

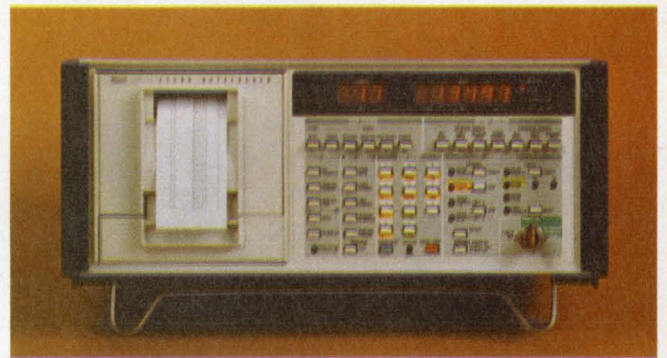
Whatever distinctions are made between smartness and intelligence, two things are immediately clear:

1. Microprocessors have just begun to have an impact on instrumentation.
2. The features and capabilities now possible are more than can be handled reasonably from both an economic and a user's viewpoint—even at this early stage of application.

The advantages of digital processing over analog have been known for some time. But now, with the availability of low-cost computers on a chip, the processing can be moved inside the instrument. Theoretically, at least, whatever a mini can do externally, a μ C can do internally.

For the user, the immediate benefits of digital processing include a reduction in physical size, and capabilities and features hitherto impossible or uneconomical. The user also gains more functions and features per dollar, and easier instrument interfacing.

All is not roses for users, however. Although the potential exists in μ P-based equipment to clear up front-panel clutter and make an instrument easier to use, just the opposite can occur.

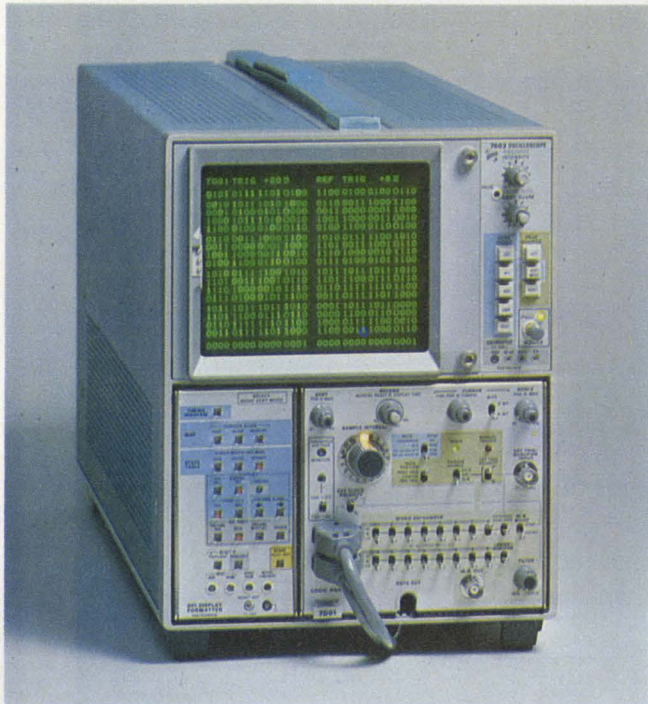


Microprocessor control brings new power to data loggers. With the Fluke 2240A, you can mix voltages, thermocouples and thermocouple types on adjacent channels.

A cursory survey of existing instruments uncovers at least one high-IQ box with nothing up front but a power switch; at the other extreme sits an instrument with 50 pushbuttons and half as many indicators.

Although comparing the two extremes is a bit unfair, the two pieces of equipment do serve to demonstrate the possibilities.

Ease of use isn't easily pinpointed from front-panel design. A blank front panel might signal nothing more than a remotely programmable instrument; 40 pushbuttons might be easier to use than 40 rotaries—but not necessarily. Once a button is punched, in some cases, the user is



Check a μ P-based system with a μ P-based system. The DF1 display formatter boosts the capabilities of the Tektronix 7D01 logic analyzer.



Interactive digital plotting is a new concept brought to realization by the microprocessor. The Tektronix 4662 digitizes and transmits its pen position.

stuck with the entered number. Or the sequence of pushing is crucial—the wrong order brings weird results. Other limitations of smart instruments center around price or speed or reliability.

The price of brain power

Even though costs are dropping, the user must still pay a premium to own a μ P-based instrument, because the cost of development is tacked

Graduates from the college of knowledge

Intelligence has touched practically every class of measuring equipment today, and the honor roll gets longer each year. Those with digital processing power include the following:

Counters: Dana Laboratories Series 9000 Micro-processing Timer/Counter; Ballantine Laboratories 5500B Universal Counter/Timer.

Data loggers: Fluke Summa II Series; Doric Scientific Digitrend; E² Thermodot DDF-200 (turns a DMM into a smart data acquirer); also units from Acurex and Esterline Angus.

DMMs and voltmeters: Systron-Donner 7115 DMM; Hewlett-Packard 3455A; Fluke 8500A; Keithley 6900; Data Precision 7500.

IC testers: Offered by Fairchild, Hewlett-Packard, Mirco, Testline and others.

Impedance bridges: Boonton Electronic 76A; GenRad 1657; Electro Scientific Industries 296.

Oscilloscopes: Nicolet Explorer; Hewlett-Packard 1722A; Norland 2001; Tektronix Digital Processing Oscilloscope.

Signal sources: Fluke 6010A Synthesized Signal Generator; Fluke 6011A Signal Generator. Wavetek 172 Programmable Signal Source.

Others: Rohde & Schwarz Automatic Radio Test Set; California Instruments CP70 Calculating Processor; GenRad 2230 Component Tester; Moxon Microcomputer Gauging System.

on. Speeds of smart instruments are still restricted, and until μ Ps get much faster, these restrictions will remain a fact of life.

What about reliability? With brainy instruments at present just babes in swaddling clothes, reliability figures are hard to come by. But, reportedly, complaints aren't.

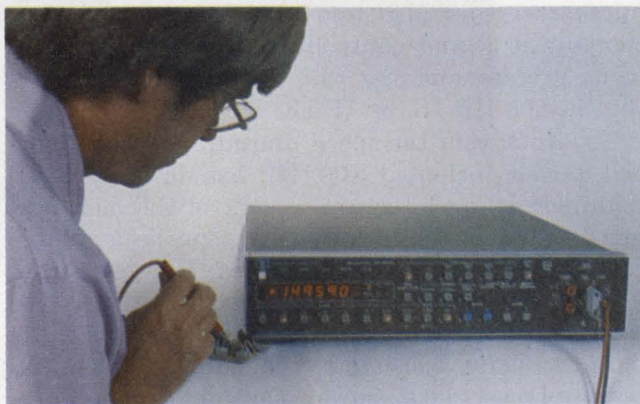
Incongruously, a greatly accepted virtue of LSI is the seemingly contradictory promise of greater reliability with increased complexity. That premise may be true. But if the user can't fully test a chip, how can he be sure of its reliability? If he can't pin down all possible states at all possible temperatures and voltages, what then? And if the user marries a μ P to a 4-k RAM plus 4 k of ROM or PROM. . . .

Counterpoint to the question of reliability is the increasing use of self-testing and self-diagnosis, brought about by dedicated LSI and μ Ps. If reliability doesn't increase, then serviceability certainly will.

The designer of smart equipment—once he's



Is this the harbinger of tomorrow's instrument? In the Fluke 8500A, measurement and control modules sit on a computer-like bus structure.



Two μ P's in the Hewlett-Packard smart DMM control measurements, compute correction factors, handle the HP-IB interface and perform mathematics.

passed the learning period—can enjoy a newfound freedom of design flexibility. As software or firmware takes over from hardware, the options to do any single measuring job or internal control function are practically limitless. But there are new headaches, too.

Design decisions now include how to partition the product—that is, what to do in software, what to do in hardware. Which RAM, ROM or PROM to use, and which new memories or μ P's will soon appear are questions a designer must continually answer to maintain his product's competitive edge. And the increased difficulties in evaluating and testing LSI components are a new source of insomnia to already beleaguered engineers.

Marketers of smart instruments must also play a lead role in deciding which of all the possible features are important, what the front-panel should look like, and what performance will appeal to potential customers. In fact, many of the basic design decisions now fall squarely in the marketer's lap, not the designer's.

Still, designers are to be envied for several reasons:

1. μ P-instruction sets are now powerful enough to produce the most complex algorithms

when the sets are combined with ROM-stored programs and data-handling RAMs.

2. One μ P can take over all control jobs, from refreshing a display to managing data output to interpreting controls.

3. Discrete operations, in many cases, can replace analog processing, with all its inherent problems.

Analog takes a back seat

One instrument that typifies the advantages of the new technology is the Fluke 8500A DMM. More a measurement system than a DMM, the 8500A is designed around a computer-type bus structure, with individual modules for measurement and control residing on the bus. Even the Fluke unit's unusual front panel can be considered a limited-use peripheral that occupies one slot of the bus.

Control is handled by an 8080 μ P, and the major operating characteristics are defined by software, not hardware.

Filtering noisy signals—ever a problem in measuring equipment—is implemented digitally in the 8500A by averaging many readings taken at a sample rate synchronized with the line frequency. Advantages: less hardware, the ability to program the number of samples per reading and, most important, greater noise rejection at operating speeds faster than analog circuits.

Other analog functions are ripe for simplification or even elimination. Circuits for tweaking or compensation (zero or offset) are candidates for the former category. Comparison, integration and sample-and-hold functions can all be performed digitally—as is done in GenRad's 1657 Digi-bridge.

The 1657 is a μ P-based automatic bridge that measures R, L, C, D and Q in less than 1/3 s. A sample-and-hold function is achieved in the bridge with software, not hardware, and errors are stored and minimized by digital techniques. The μ P also computes and makes decisions—it directs both the instrument and the user to achieve optimum ranging.

Besides speed, the Digi-bridge user also enjoys maximum resolution, repeatable results and low cost. With component count two-thirds less than conventional circuitry, the 1657 sells for \$995. Without the μ P, says GenRad, the equivalent bridge would cost about \$6000.

Another bridge with the new look is the Electro-Scientific Industries 296. Because of the internal μ P, the 296 can be programmed for limit comparison (up to 10 values), can display percentage or absolute deviation and can be con-



Computer power brings a new dimension to everyday optical measurements. Gamma Scientific's CR-1A is an intelligent radiometer with programmable response.



Turn your DMM or DVM into a smart data-acquisition system with the DDF-200 control unit from E² Thermocorp, Carpinteria, CA. The unit handles up to 20 inputs.

trolled through the IEEE 488 bus.

Still another instrument—the Gamma Scientific CR-1A computing radiometer—further demonstrates the power of internal digital processing.

Checking light with delight

Anyone who has made light measurements knows the problems of making adjustments for drifting zeros and dark currents. With the CR-1A, zero offset, dark current and ambient levels are digitally and automatically subtracted out. With eight keyboard-programmable constants, the user can punch in, update or change correction factors to shape response at various wavelengths. Each of eight registers stores a 3-1/2-digit number, a 1-1/2-digit exponent with sign and selected dimensional units.

The CR-1A takes further advantage of the μ P with a self-calibrating algorithm, digital signal averaging and autoranging, among other features.

Self-calibration is a growing trend that may soon be a feature of all measuring instruments.

The designers of one smart instrument, Hewlett-Packard's 3455A digital voltmeter, have taken special pains with the "auto cal" feature of the unit. The user unplugs a removable reference, makes four adjustments, then plugs the reference unit in again. The meter then checks its own dc and ohms circuits and corrects for errors.

Controlling the calibration process and computing correction factors in the HP unit is, of course, a μ P—one of two in the instrument. The two microprocessors also take care of mathematical computations and controlling both the measurement process and the unit's programmability—that is, the HP-IB, or IEEE 488 interface.

To circumvent the speed limitations of commercial, serially oriented μ Ps, HP has designed a μ P with parallel architecture to control the measurement functions. Such μ Ps may soon be available commercially from other sources. But one problem designers face with such architecture is the increase in support chips as the μ P grows more parallel. Thus, speed may be gained at the expense of cost, size, power consumption and reliability. Somewhere along the line, compromises will have to be made.

A new force in μ P testing

Those who design with μ Ps must also decide how to test the little buggers. To that end, μ P or logic analyzers have appeared on the market, some μ P-based themselves. One of the μ P-based analyzers is HP's 1611A.

In appearance, the keyboard-controlled 1611A resembles a programmable calculator with a CRT display. In operation, the internal 8080 controls the keyboard, tests for trigger points, keeps hierarchical order and performs other housekeeping chores.

What makes the 1611A smart? Software does much of the work according to HP—counting events, measuring execution time, looking up tables for mnemonic readout, and performing other computations. Thus the 1611A relieves the user from much of the test burden. In effect, the 1611A fights fire with fire: Software checks software; a μ P tests a μ P.

Other manufacturers recognize the power of the μ P as the basis for equipment meant to test other μ P-based equipment. Two such tools are the E-H Research Labs 1330 and the Tektronix DF1. In the guts of the Tektronix DF1 display formatter sits a μ P, along with four ROMs and nine RAMs, one RAM serving as a scratchpad memory.



The new look in signal generators: Fluke's 6011A stores frequencies and amplitudes and lets the user edit or modify the output from a keyboard.

When used with the company's 7D01 logic analyzer, the DF1 turns any 7000-series scope into a measuring tool that displays timing diagrams, logic maps and state tables in binary, octal or hexadecimal codes.

Using a SC/MP μ P, the 1330 offers a wide variety of triggering criteria to perform both logic timing and state analysis.

Not only can smart equipment lift a load from its user, it can even do the same for other smart equipment—a host computer, for instance. Consequently, more and more peripherals are undergoing brain “transplants.” Conversely, with μ Ps combined with the IEEE 488 standard interface, measuring instruments—when connected in a system application—are beginning to look more and more like peripherals.

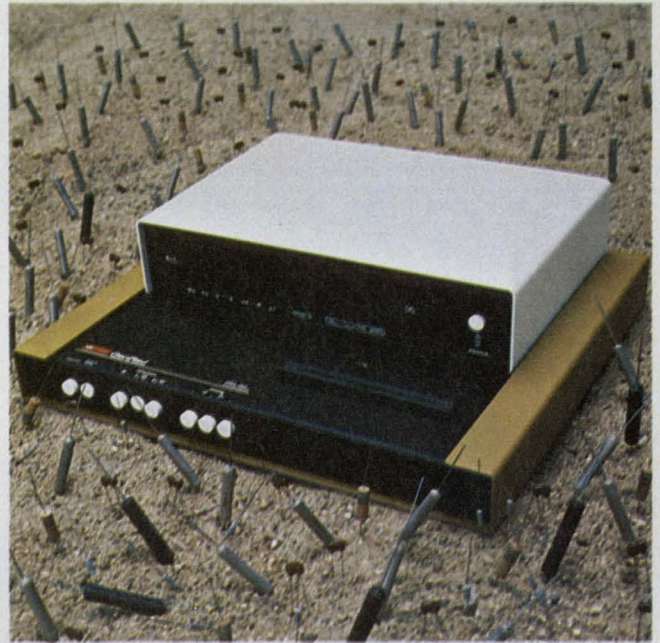
One “peripheral” is smart enough to speak for itself. The Tektronix 4662 interactive digital plotter—the first with built-in processing, thanks to the MC6800 μ P—prints alphanumeric characters as well as draws whatever curve, plot or schematic the host processor dictates.

But give a machine a brain, and what happens? It talks back. The 4662, through use of an X-Y joystick, can send back current pen coordinates and other information.

Thanks again to the μ P, the 4662 can work at high speeds, with acceleration, deceleration and vector generation all handled by the 6800. And the plotter can rotate or scale characters, change plot size and self-test its internal buffers.

With this kind of performance now being squeezed out of a design tool (the μ P) that's barely five years old, the question arises: What next? New μ Ps and memories are coming, with on-board complexities and functions that signal even more radical changes in instrument design.

Is the Fluke 8500 voltmeter, with its internal



Microprocessor-directed ranging removes the guesswork in this automatic bridge, the GenRad 1657. Maximum resolution is always achieved on the readout.

bus structure and functional modularity, the forerunner, the symbol of things to come? Perhaps. But the Fluke design raises more questions than it answers.

Are instrument designs all heading toward a common finale, focusing on a single, universal instrument capable of becoming anything a user would like merely by a change in programming or the dropping in of a few memory chips? One instrument—the RS-432 data and timing generator from Interface Technology, Covina, CA—already permits the user to program the μ P section to control the word-generator section.

Or will instrument systems dominate, with clusters of dedicated (perhaps even dumb) equipment chatting away at each other over remote lines, busily measuring, chewing up data, spitting out final results?

Perhaps some other, hitherto unknown, concept will prevail. In the more immediate future, more “conventional” intelligence can be expected to show up in yet untouched or barely influenced equipment—small, low-cost portable DMMs, scopes or spectrum analyzers. Signal generators have just begun to show the effects of the μ P. Wavetek's 172 13-MHz synthesizer, for example, uses a μ P to simplify programming, to handle formatting and to permit keyboard numeric entry of frequencies. And dynamic RAMs or PROMs in the 172 store programs or subroutines.

Other sources are sure to follow. Whatever happens, it will be exciting to watch. ■■

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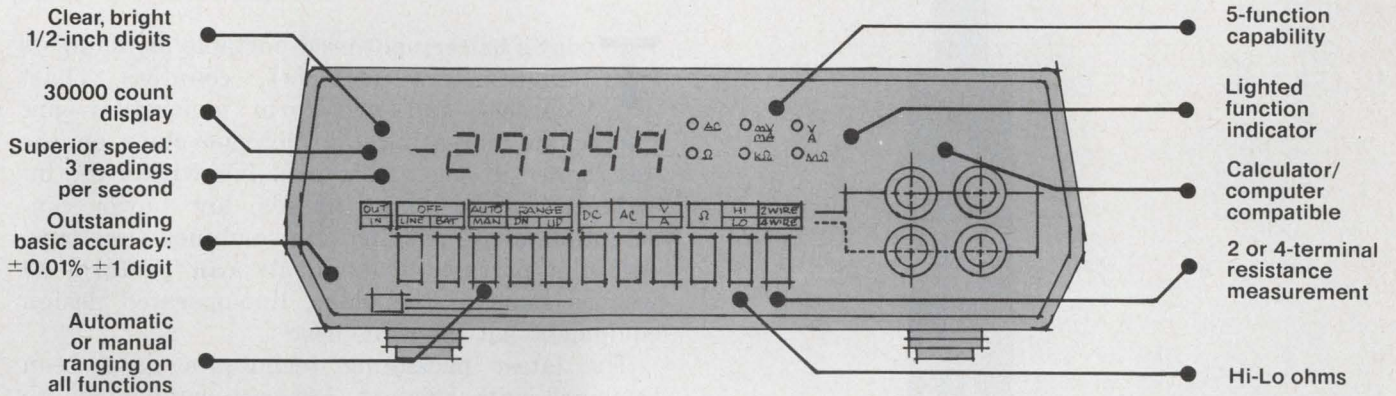
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FOR DEMONSTRATION, CIRCLE 36
FOR TECHNICAL DATA, CIRCLE 37



Portable instruments: The specs are fine, but their batteries are still short-lived

Today's battery-powered portable instruments—multimeters (DMMs), counters, chart recorders and waveform generators—are finding an increasingly prominent place on the designer's lab bench. Complex ICs within the instruments ensure high speeds, low power consumption, dense packing and combined functions. And the portable instruments can perform as well as some of the older, line-operated design equipment—at the same cost.

The latest packaging techniques have been combined with efficient, low-cost components to improve the general circuit design and the resultant savings in production costs have been passed on to the user.

The new portables contain the following custom or standard LSI circuits or specialized MSI:

- Entire analog-to-digital converters on one or two MOS chips.
- Complete four-to-eight decade counting circuits in a single package.
- Single-chip instrumentation amplifiers and low-power op amps.
- Specialized control circuits that do all the "internal housekeeping" for the instrument.
- High-efficiency switching regulator circuits.
- Battery-level indicators.

Battery-powered portables are no panacea, however. They often have a limited battery lifetime, a restricted operating temperature range and a high susceptibility to surrounding electrical fields. However, some new battery designs are overcoming these common power limitations.

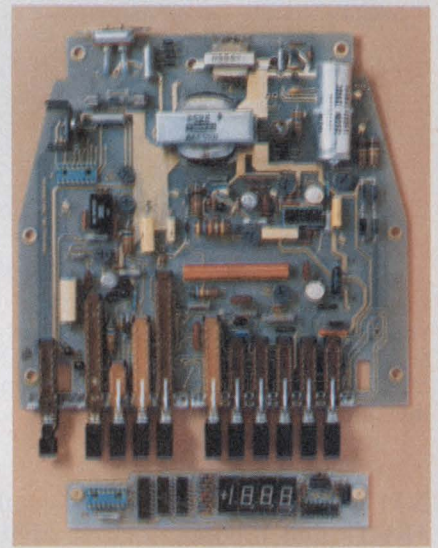
ICs cut parts, cost & power

MOS LSI circuits, with their high packing densities, have enabled instrument designers to reduce the number of components needed. Custom MOS circuits still predominate in use among instrument manufacturers, although many of the new off-the-shelf circuits (probably last year's custom circuits) are starting to offer designers the functions necessary to build their instruments.

Dave Bursky
Associate Editor



Delivering true rms ac readings in addition to ohms and dc, the 7003 DMM by Systron-Donner can operate for up to six hours from its internal battery pack. Inside the



DMM, a single-chip a/d converter takes three readings per second that are displayed on a 3-1/2-digit, 0.4-in.-high light-emitting diode display.

Single and multiple-chip a/d converters in PMOS, CMOS and I²L technology reduce the size and power requirements of DMMs. Converter circuits, such as those developed by Analog Devices, Norwood, MA; General Instrument, Hicksville, NY; Intersil, Cupertino, CA; Motorola, Austin, TX; Siliconix, Santa Clara, CA; and Teledyne Semiconductor, Mountain View, CA, require only 100 to 200 mW. Many of these circuits are designed for single-supply operation, and so eliminate the drain caused by a dc-to-dc converter to get the second supply level. (For more information about a/d converters, see the Focus on data converters" in ED No. 19, September 13, 1976, p. 68, and the special report on monolithic a/d and d/a converters in ED No. 13, June 21, 1976, p. 28).

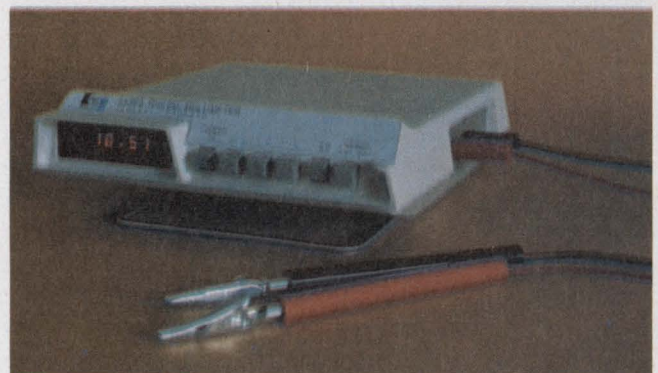
Almost every DMM manufacturer incorporates one form of these IC a/d converters in his meter—and if he hasn't found one suitable, he has designed his own. Hewlett-Packard, Palo Alto, CA, for instance, has designed a special conversion circuit and thin-film resistor network for its 3476B DMM. At a cost of \$275, with the built-in battery pack, the meter offers V and I on ac or dc and ohms, autoranging, autopolarity and a special range-hold feature.

HP's special circuit is a hybrid consisting of an NMOS control chip and a tantalum-nitride-on-sapphire resistor network. The control chip contains the counters, buffers, display scanner, 3500 bits of ROM program storage and all analog switches. The resistor chip contains 19 laser-

trimmed resistors matched to within 0.02%.

Another DMM, the Danameter from Dana Laboratories, Irvine, CA, has only two ICs—a digital CMOS circuit and a bipolar analog chip. This DMM is one of a few using liquid-crystal displays instead of LEDs or gas-discharge digits. Going this route keeps power requirements to a bare minimum—the Danameter can operate with a 9-V battery for about a year. Weston in Newark, NJ, also offers a DMM with an LCD readout.

Making wide use of CMOS, Logical Technical Services in New York has developed the Model 12T, a combination DMM and thermometer, for \$259. The unit fits in the palm of the hand, much like the hand-held DMM developed by Hewlett-Packard several years ago. The 12T uses not only digital-CMOS devices to cut power drain, but also tri-technology products like RCA's (Somerville,



Using a specially designed hybrid circuit, the 3476B DMM developed by HP measures ac or dc voltage and current and ohms. Batteries provide an eight-hour life.



You can operate this scope and over a dozen other models from almost any voltage because Philips has incorporated a high-efficiency switching supply that eliminates the power transformer.

NJ) CA3130 op amp, which combines MOSFETs, JFETs and bipolar devices. MOSFETs on the op amp's front end provide high input impedance; the JFETs provide the current source; the bipolar devices in the middle provide gain; and the CMOS output provides up to 20 mA to within several millivolts of the power supply or ground level.

Power consumption is dependent on the number of readings taken per second—a factor often overlooked when portable DMMs are evaluated or designed. The slower the conversion and counting circuits operate, the less power consumed.

When monitoring signals that change at several hertz, DMMs designed for line operation will always have an edge over battery-powered units. For example, most portable DMMs, like the Logical 12T or the Hewlett-Packard 3476B, take only two or three readings per second, while line-operated units often take five or more readings. Slow, periodic fluctuations can easily be missed if the meter's converter is too slow.

Other portable DMMs have been recently introduced: the 8030A and 8040A 3.5 and 4.5-digit DMMs by Fluke, Mountlake Terrace, WA; the Model 248 4.5-digit DMM by Data Precision, Wakefield, MA, and the 172 and 173 30,000-count DMM by Keithley Instruments, Cleveland. In addition to the normal V/I/R functions, Fluke's 8030A has a diode-test capability and can run for eight hours on a single charge. The 8040A has an autoranging capability and does true rms-ac measurements at frequencies up to 20 kHz. Data Precision's Model 248 also has true rms capability. Similar to Data Precision's older 245, the 248 also makes use, internally, of a custom digital circuit originally designed for the company's inexpensive Model 175 DMM to do all the display control.

LSI counting circuits, such as the MK50395



Packing a bandwidth of 0.02 Hz to 2.2 MHz, Exact's Model 119P function generator delivers 10-V pk-pk into a 60- Ω load. The generator can operate from any 12-V-dc source, an internal battery or the ac line.

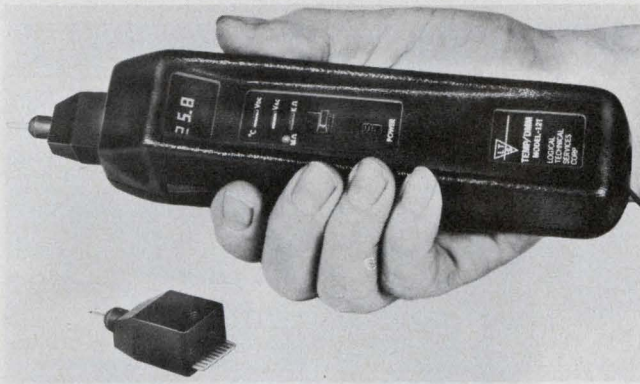
series of six decade counters from Mostek, Carrollton, TX, the ICM 7208 seven-decade unit from Intersil can form the heart of many compact, battery-operated frequency counters. These circuits can replace as many as 15 to 20 MSI devices and draw only about 200 mW.

Several companies are using this approach to make inexpensive, but very compact, frequency counters—but not all. "Non Linear Systems, Del Mar, CA, looked at this approach and decided not to use it," says Roland Johnson, chief engineer. "We decided we could get even better performance by using low-power Schottky TTL and CMOS to build our FM-7 seven-digit frequency counter." The FM-7 and its four rechargeable batteries all fit in a 4.5 x 6.5 x 9.6-cm ($\approx 2 \times 2.5 \times 4$ in.) case. The FM-7 can handle input frequencies from 10 Hz to 60 MHz (100 mV rms sine-wave sensitivity) and has an accuracy of ± 1 digit \pm time-base accuracy.

While most of the portable counters have similar accuracy specs, input sensitivities vary from model to model. Most portables have sensitivities of 10 to 100 mV rms, whereas lab-bench units often have sensitivities down in the microvolt region—direct measurement of rf is commonplace.

Portable instruments with combined functions are on the rise. Both HP and Vu-Data offer portable oscilloscopes with built-in DMMs or frequency counters. Tektronix, Beaverton, OR, goes so far as to use the CRT screen of its Model 213 1-MHz scope to display the reading. The entire combined scope/DMM weighs only 3.7 lb and can operate for 3.5 hours with internal batteries. Inside the 213, Tektronix uses several custom circuits to do the display generation and control all the timing. Very-high-efficiency switching circuits are used to provide the acceleration voltages.

Philips, which has gone to great lengths to make an efficient switching regulator, now in-



With over 150 components crammed into a hand-held DMM/thermometer, Logical Technical Services' Model 12T offers autoranging, autopolarity and 0.1% accuracy (V dc). The 12T provides a 3-1/2-digit answer and meas-

cludes its regulation circuit in almost every scope it sells. The circuit permits the Philips scopes to be used from almost any ac voltage source ranging from 90 to 270 V at 46 to 440 Hz or any dc source from 100 to 200 V. Power consumption, depending upon model, ranges from 20 to 30 W, and unit weights average about 20 lb.

Function generators demand power

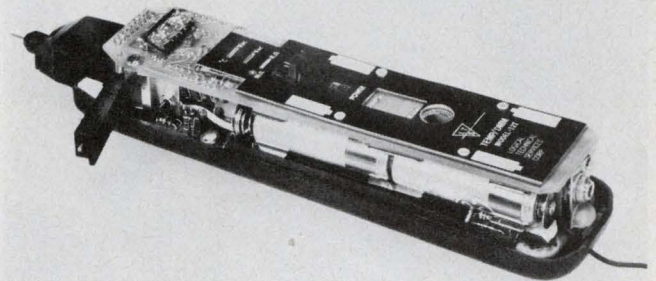
Generating signals in portable packages takes a bit more than simply measuring them. Only a few manufacturers offer any signal source with a self-contained battery pack. With its Model 30, Wavetek, San Diego, CA, is probably the best known. But pressing Wavetek is Exact Electronics, Hillsboro, OR, with its Model 119P.

The Model 30 operates from a single 9-V transistor radio battery and delivers sine, square and triangle waves over a 1-Hz-to-100-kHz range. It can deliver 5-V pk-pk into a 600- Ω load (or about 41 mA, maximum). Of course, delivering that much current will drain the battery pretty quickly, so a \$25 rechargeable battery option is available for the \$150 instrument.

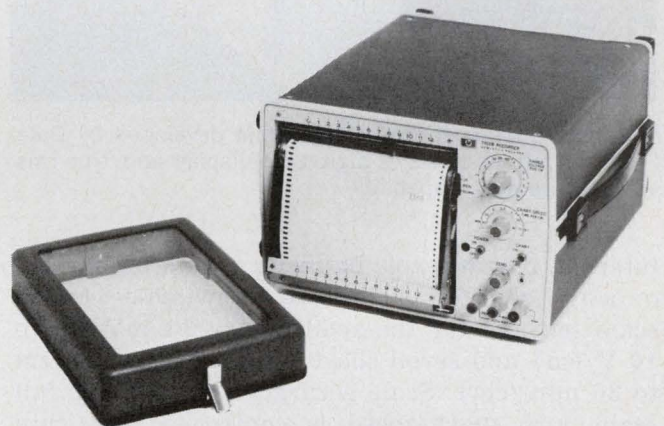
Although Exact's 119P is larger than the Model 30 and costs about twice as much—\$295—it offers more than 10 times the frequency range and twice the output voltage. The 119P spans 0.02 Hz to 2.2 MHz, delivers 10-V pk-pk into a 600- Ω load, and has a variable-time-symmetry adjustment.

While the battery-powered function generators deliver signals, the portable chart recorders can keep signal records. The go-anywhere recorders are available from such companies as Gulston, East Greenwich, RI; Hewlett-Packard in San Diego; Lab Data Control, Riviera Beach, FL, and Esterline-Angus, Speedway City, IN.

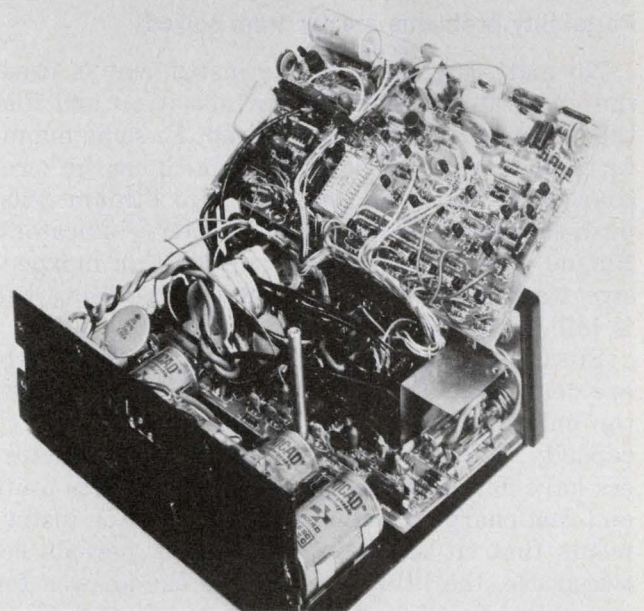
The HP 7155B runs from ac (85 to 130 V, 48 to 440 Hz), external dc (10.5 to 36 V) or from



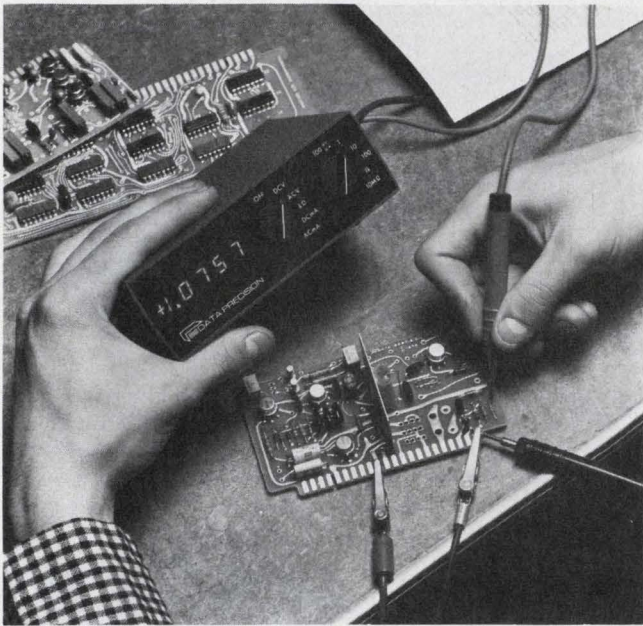
ures resistance from 1 Ω to 19.99 M Ω , dc volts from 1 mV to 750 V, ac volts from 200 mV to 750 V and temperature from -55 to 153.5 C. The NiCd batteries permit approximately 3-1/2 hours of use.



Capable of operating in any position, HP's 7155B chart recorder offers 16-input voltage ranges and 7 chart speeds. It can run for 9 hours off the internal batteries.



Although originally aimed at the hobbyist market, the IM2202 designed by Heathkit has an accuracy of 0.5% on dc and 1% on ac, which makes it suited for many lab-bench applications.



The just announced Model 248 DMM developed by Data Precision offers a 4-1/2-digit LED display and true-rms ac measurement capability.

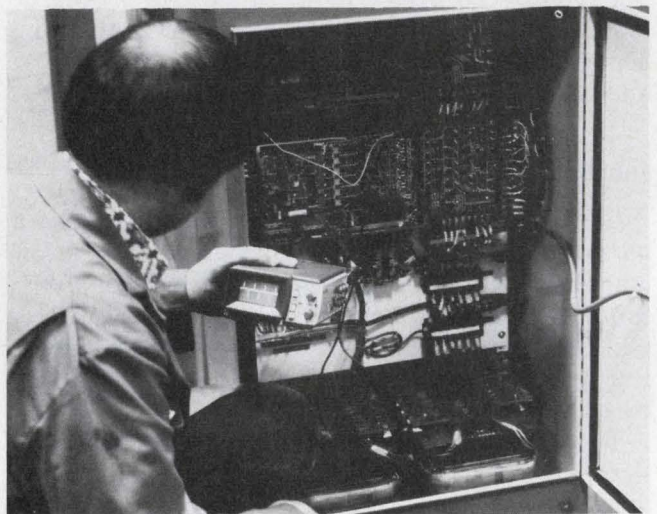
internal, rechargeable batteries (up to nine hours on a full charge). There are 16 switch-selectable scale settings for the span (from 0.1 mV/cm to 10 V/cm) and seven chart speeds (from 10 s/cm to 30 min./cm). Scale accuracy is $\pm 0.4\%$ of full scale, and chart speed is controlled to within $\pm 1\%$. This "Cadillac" of portable recorders goes for a stiff \$1400 and \$1700 with the internal, rechargeable battery pack.

Portability problems are far from solved

No matter which portable instrument is used, the greatest annoyance is to turn it on and find the batteries either weak or dead. So some manufacturers are incorporating "quick-charge" rechargeable batteries, long-shelf-life lithium cells, push-to-read controls and low-battery indicators. But no vendor has yet come up with an inexpensive way to determine how much operating life is left in a battery.

Since instrument manufacturers apparently are doing all they can to cut power consumption, the only other alternative is to increase battery capacity. To this end, many battery manufacturers have developed the sealed gel-electrolyte units and fast-charge nickel-cadmium cells. For instruments that sit on the shelf for long periods between use, the lithium battery is the answer for improved shelf-life. It has a shelf-life of 5 to 10 years. The lithium batteries are also the same size as carbon-zinc, but offer twice the voltage.

Specially designed circuits and batteries are



Combining both a DMM and a scope into a small, handheld package, Tektronix' Model 213 uses the CRT to display the DMM reading.

starting to eliminate some of the guesswork in determining available battery life. Several low-power comparators from Intersil can be externally set to trigger whenever the battery voltage drops below a predetermined level. Once triggered, the circuit can be used to drive a LED indicator.

Battery manufacturers have developed several cells that have abrupt voltage drops when about 70% of their expected life has passed by. The drop is abrupt enough to trigger a circuit that can drive an indicator. Other batteries such as "super-fast"-charge NiCds nearly eliminate the problem. With charge times as short as 15 minutes—and typical NiCd charge times ranging from 4 to 16 hours—these new NiCds appear ideal for portable applications. ■■

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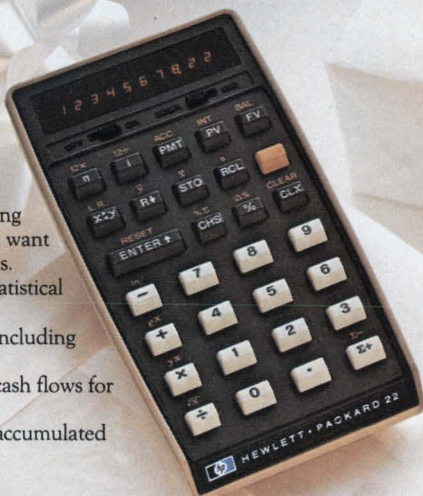
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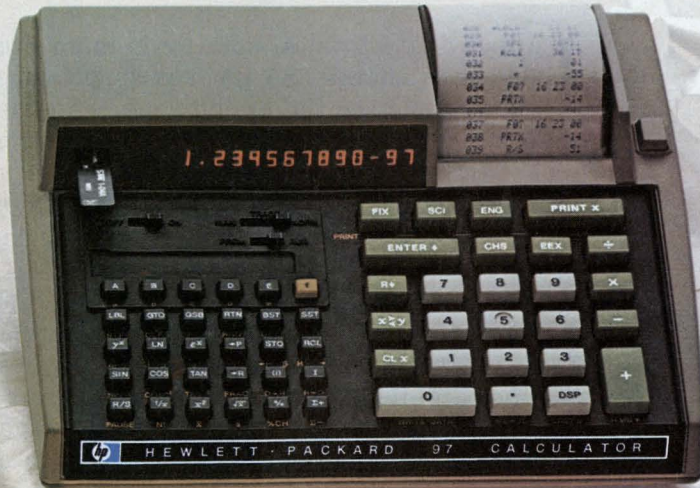
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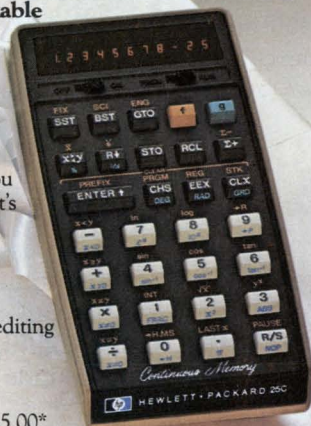
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- Selectable display modes: fixed point and scientific notation.

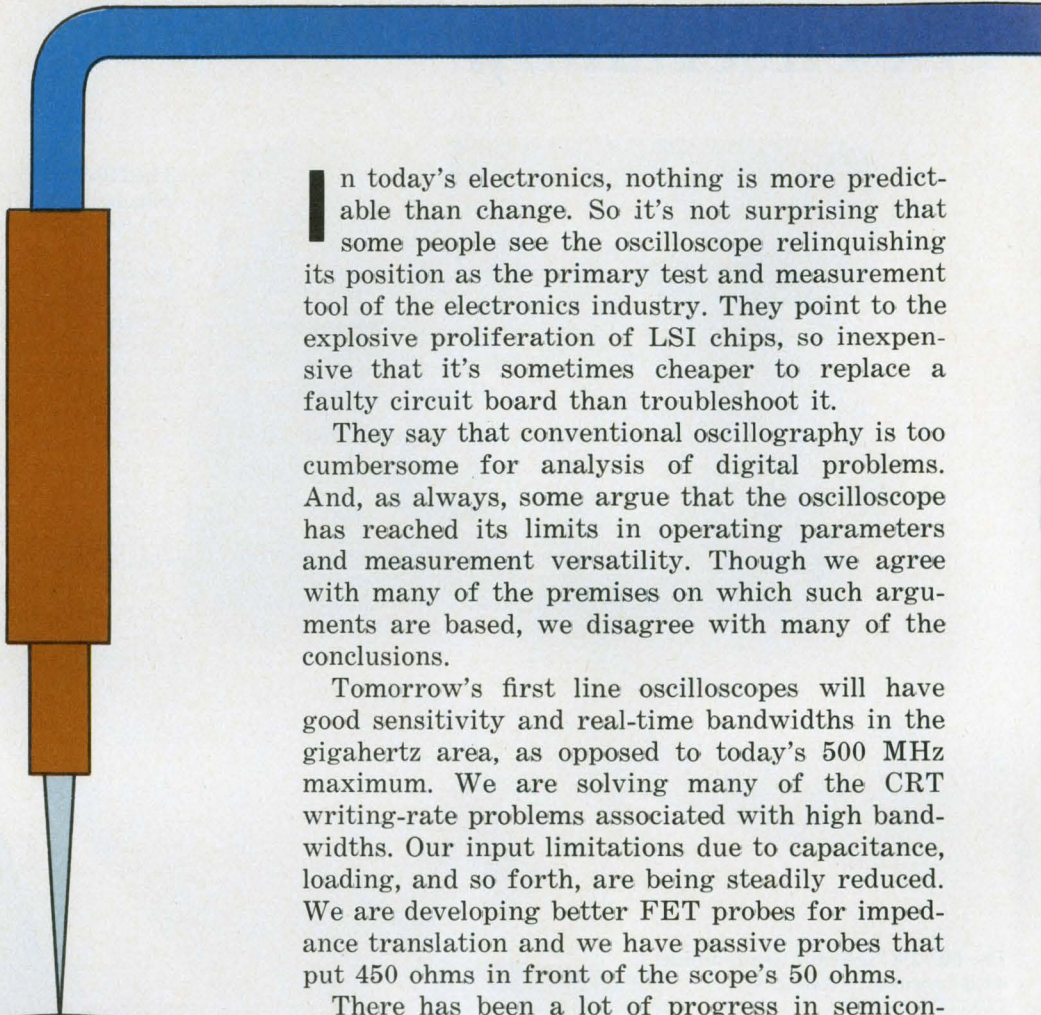


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CIRCLE NUMBER 39



In today's electronics, nothing is more predictable than change. So it's not surprising that some people see the oscilloscope relinquishing its position as the primary test and measurement tool of the electronics industry. They point to the explosive proliferation of LSI chips, so inexpensive that it's sometimes cheaper to replace a faulty circuit board than troubleshoot it.

They say that conventional oscillography is too cumbersome for analysis of digital problems. And, as always, some argue that the oscilloscope has reached its limits in operating parameters and measurement versatility. Though we agree with many of the premises on which such arguments are based, we disagree with many of the conclusions.

Tomorrow's first line oscilloscopes will have good sensitivity and real-time bandwidths in the gigahertz area, as opposed to today's 500 MHz maximum. We are solving many of the CRT writing-rate problems associated with high bandwidths. Our input limitations due to capacitance, loading, and so forth, are being steadily reduced. We are developing better FET probes for impedance translation and we have passive probes that put 450 ohms in front of the scope's 50 ohms.

There has been a lot of progress in semiconductor technology in terms of gain-bandwidth product, impedance transfer function and noise reduction. And when today's 7-7.5 GHz IC processes (which make 1-GHz scopes possible) reach their expected limits at about 10 GHz f_t , we can turn to gallium arsenide, gallium phosphide or other compounds now in development.

Computer-aided design has come along at a fortunate time, too. In the days of discrete circuits, it wasn't too useful because you couldn't put in all the strays.

If you added the strays with CAD, the problem became too complex, and if you didn't your circuit wouldn't work. But with ICs, the strays are smaller and more predictable. And we can work not only with surface

**Howard Vollum,
Bill Peek
and Wim Velsink
of Tektronix
Speak on
The Future of
the Scope**

George Rostky
Editor-in-Chief



Chatting with a visitor are (l-r) Bill Peek, Wim Velsink and Howard Vollum. In the background are the 511,

Tek's first oscilloscope, dating from about 1946, and the 7834, a superspeed storage scope, just introduced.

geometries, but also in the third dimension, designing resistivities along with metal patterns and mask layouts.

Of course higher bandwidths present triggering problems, but we see progress along this line, too. One of the basic departures from the historical approach for greater stability is the use of high-speed ICs, as opposed to tunnel diodes. And faster amplifiers with shorter delays have made it possible to use shorter delay lines with better performance.

Sensitivities in the millivolt region can be anticipated, even at the higher bandwidths. Amplifier noise is the limiting factor here, but semiconductor technology has made great strides in reducing this problem.

Obviously none of these developments would mean much without parallel advances in CRT technology. We've made great progress in this area too. CRTs with bandwidths of 3 to 4 GHz and deflection factors of 1 to 2 V/cm in both vertical and horizontal are a present reality, with photographic writing rates up to 3 cm/ns. You can actually see a single-shot trace with the naked eye. And we haven't reached the limits yet.

Research is pointing away from the mesh scan-expansion CRT toward designs that will give us

the nice crisp spot sizes we used to get with instruments like the 547—about 7 mils. And we'll eventually see these new CRTs in wide-bandwidth portables, where finer traces are much in demand.

Looking at the CRT as a display, we see an increased use of alphanumeric. We'll see new kinds of information displayed—information that will help the scope user do his job. It may be an instruction on what to do next, or a coded display—one/zero, hex, maps, signature, etc. A programmed logic analyzer might show you a picture for so many seconds and then ask you what you wanted next. Or a scope might instruct you to hook up this probe at this point and then tell you whether the reading is good or bad.

The storage scope is really coming of age, too. Ideally, we'd like to make every oscilloscope a storage oscilloscope.

Storage almost always works to your advantage. It lets you compare things, eliminates flicker and eases photography tremendously. Because you have a stationary picture of known brightness, there's no hassling—you know you're going to get it. If storage could be incorporated basically into every oscilloscope, even if it cost a little

more, probably everybody would use it.

Of course there were good reasons in the past for not doing this. But today we are getting to the point in storage technology where we can store as fast a signal as we can get on a conventional CRT. The new 7834 is spec'd at 2500 cm/s—fast enough to store a signal at its rated 400 MHz bandwidth. And our future advances in stored writing speed are expected to keep pace with bandwidth advances.

Storage is still the cheapest way to memorize a waveform. In spite of the many cheap A/D converters available, you still need a digital memory to take advantage of them.

The future of the sampling oscilloscope is less clear. One of the problems is that the sampling scope is useful only with repetitive waveforms, and there just isn't a multiplicity of fast, repetitive waveforms that people want to look at.

Really fast waveforms are usually single-shot, and the few exceptions can usually be handled by other techniques. Then, too, there has been a race between samplers and real-time scopes for a long time, and though real-time scopes haven't actually won it, in terms of being able to do everything the sampling scope can do, they have covered enough of the applications so that sampling has taken a back seat. And sampling has always had a problem in terms of the operator's confidence that what he sees is what is really there. Sampling scopes aren't easy to use, and there are modes you can get into that give a picture completely different from the real one. False triggering, for instance, and other operator traps. You might say that sampling scopes won the battle but lost the war.

Actually today's sampling scope is easier to use than it was in the past. The computer people, as they get into higher and higher speeds, will be using sampling techniques for some waveform analysis, especially in CPUs and communications links, where the highest speeds are encountered. To do this though, they'll have to program the computer to run in a repetitive mode in most cases.

Sampling techniques will also be used for a good while in time-domain reflectometry instruments like the Tektronix 1502 and 1503 portable TDR cable testers. This application is a natural for sampling. You generate a repetitive pulse and send it down a coax line, then display the reflection to determine the nature of any discontinuity or anomaly. You also measure the elapsed time between pulse and reflection and convert this to distance. With sampling techniques

Howard Vollum



Charles Howard Vollum has been involved with oscilloscopes since 1933, when he designed and built one for the radio-repair work that helped finance his education at Reed College in Portland, Oregon. In March 1941, five years after graduating with a BS in Physics, Howard was drafted into the infantry. December of that year saw him commissioned 2nd Lieutenant in the Signal Corp and sent to England to work on high-resolution radar, in a lab directed by Sir John Cockcroft, the first man to split the atom. Working on a display for a 0.1 μ s radar, he became expert in wideband video-amplifier and fast-sweep techniques.

In 1946, when Howard left the Army, the fledgling oscilloscope market was dominated by one company, the big electronics companies having decided the oscilloscope didn't merit significant investment. Howard, though, saw a need for a scope that could measure (not just display) electrical waveforms. With a small group of newly released veterans he formed

you achieve the gigahertz bandwidth necessary for resolution measured in inches, at a relatively low cost.

The other dimension of sampling lies in its use in A/D converters—rapid acquisition and retention of a bit of information, long enough to convert it to digital information. We'll see a lot of development continuing in that area.

So much for the idea that the oscilloscope has reached its technological limits. Now let's look at the argument that it's becoming obsolete in the

Tektronix. The first product, the Type 511, a 10-MHz, triggered-sweep, calibrated scope using many of the wartime technological advances, was an immediate success.

Today Tektronix occupies more than 500 beautifully landscaped acres in Beaverton and Wilsonville, Oregon, employs more than 13,000 people, and reported over \$360 million in sales for fiscal 1976. The oscilloscope still accounts for the largest part of these sales, although Tektronix does a flourishing business in other electronic test and measurement instruments, TV monitors and signal processors, and a growing family of computer peripherals.

Despite his success, Howard remains a soft-spoken, mild-mannered individual, with an active concern for the welfare of his employees and a youthful enthusiasm for progressive ideas. He shuns public attention and attributes the success of Tektronix to the "wonderful, hard-working people" who work with him.

Nevertheless, he has been honored many times by his community, his country, and his peers in the academic and business worlds. He received the Legion of Merit with Oak Leaf Cluster for his contributions to military electronics projects during WW II. He has honorary doctorates in Science, Law and Humane Letters, is an honorary member of the ISA, and received a Medal of Achievement Award from the Western Electronic Manufacturer's Association. He is a Fellow of IEEE and received its Morris Leeds Award in 1973. He has received several distinguished service awards from various colleges, universities and institutes, and is a trustee or board member of three local colleges and one of Portland's largest hospitals.

Howard is married and has five children, ranging in age from 10 to 24 years. In his home, he has installed a full-size pipe organ, which he plays, he says, not nearly as well as his 22-year-old son. His other hobbies include photography and hi-fidelity magnetic recording.

world of the cheap integrated circuit and the smart microprocessor.

There is no doubt that the scope of today is in for some significant changes. But wherever electronics goes, you find the oscilloscope follows.

Remember the old fears that the computer would put everyone out of work? The idea that the oscilloscope will join the unemployed is no

more apt to see realization.

As we see it, there will be two main thrusts to future scope development. One is the use of intelligence. It's in this area that the microprocessor will have its greatest impact. What form this will take isn't clear yet. There are plenty of real opportunities here, but also a lot of problems to be solved and decisions to be made.

The other thrust will be toward cost reductions. We expect some severe price competition in segments of our product line. There is strong demand for a multifunction, 50 MHz, 5-mV, dual-channel, delayed-sweep oscilloscope at a lower and lower price. The situation may develop into a repeat of the minicomputer business. Today minis are not getting much faster, but you can get for \$2375 what you paid \$15 K for when DEC first came out with the PDP-11 series. We haven't seen much of this in the oscilloscope business in the past, but it's probably going to be with us in the next 10 years.

But let's get back to the intelligent scope. Right away we run into a whole chain of considerations. You see, so much depends on how the oscilloscope is to be used.

In the lab, for instance, you don't often know in advance what you want to do with a waveform. You just see what's there, and that leads you to step two and on to step three and so on. It's not a predetermined situation. So, except for very broad mathematical manipulations like FFT, signal averaging, etc., it is difficult to predict in advance what digital processes you are going to need—and you can't build enough of them into a scope to cover every contingency.

On the other hand, there are significant application areas—servicing and production mainly—where the need is well defined. Like measuring rise time, time delay, time between pulses, etc. The scope could be programmed to make these measurements automatically and provide a read-out on the CRT. Then if something came out wrong, the same scope could be used to troubleshoot the device.

It's in this area that the microprocessor will have its biggest impact. But we'll still have the problem of deciding what we want the scope to do. This means we'll probably have to provide custom programming software. Or we'll have to make it awfully easy for the customer to do his own programming. Probably we'll do both, in different kinds of instruments.

Some portable scopes may be designed for specific service applications. That is, a computer manufacturer may design a set of computers and

Wim Velsink



Wim Velsink has been in the front lines of R&D at Tektronix for most of the 16 years he has worked there. After taking his BSEE from Hogere Technische School in 1960, and short stints with Philips and Siemens and Halske in the Netherlands, Wim came to the U.S. He started with Tektronix as a design engineer in the accessories division in 1963, became Project Manager, Advanced Circuitry, in 1965 and Manager, Advanced Project Development, in 1966. One of his more important responsibilities in this position was the development of the 7000 series oscilloscope line. Wim is now Director of Tektronix Laboratories, General Manager, New Ventures Division and Manager, Advanced Display Techniques Development. He became a vice president in 1973.

Wim is a bachelor and an outdoorsman who relishes the many opportunities for skiing, hiking and camping in Oregon.

we'll provide a scope that is identical to last year's model, except that there'll be new cards with PROMs or ROMs and a special service manual for that set of computers and peripherals.

In other scopes we may provide the basic arithmetic functions and a few others that you can operate on a waveform with. You could multiply voltage and current to get instantaneous power, or integrate a current waveform to get charge. These capabilities are useful to a design engineer. And a lot of single-value functions would also be useful—rise time, aberration amplitude, period of aberration ringing, pulse-width, integral under the curve, and many others.

These kinds of functions are valuable in characterizing and documenting circuits, aside from testing them in production or incoming inspection. This kind of a scope would eliminate much of the present drudgery, say, in integrating a waveform. Now the operator must measure the

waveform, digitize it point by point, then feed it into a computer, or use his calculator.

But building these functions into a scope isn't as easy as it seems. At first glance, it looks as if you'd only have to sample the waveform at a couple of points, measure the difference digitally, and show the readout on the screen. With this information, plus an examination of the waveform, you'd have a measurement you knew was valid. And this technique wouldn't be complicated or expensive. Actually it's not that easy.

We've found that many times it's just as easy to digitize the whole waveform and store it for viewing as it is to remember the two points and then try to correlate them back to the waveform position. Even the time required to turn the Z-axis on and off creates all sorts of problems in circuit and CRT design.

So let's say we digitize the input signal. By what method? Well, with A/D conversion, if we want to stay within reasonable costs and power requirements we need emitter-coupled logic.

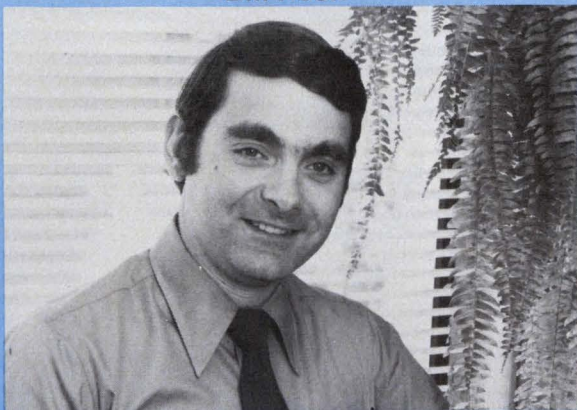
This means a word rate of about 25 MHz or below, which gives us a 10-MHz scope at best. Or we can use scan-conversion techniques, as we did with the 7912. There's virtually no bandwidth limitation here, and you don't need a repetitive signal as you do with sampling. The principal limitation of the scan converter is in the length of the memory. How long a waveform can it remember? You're also limited to one sweep, at least presently, and the cycle between sweeps is relatively long compared to sweep time.

Of course, this limitation applies to all scopes. The only way to get around it is through continuous A/D conversion, and here you run into bandwidth limitations again. Even at a 25-MHz word rate, you fill a memory awfully fast. So you have to let the waveform run through the memory, decide what time slot you're really interested in, and pre- or post-freeze it, depending on the application.

This, incidentally, is one thing you can't do with the scan converter. Of course in the next five years we'll see the word-rate go up by an order of magnitude. We'll also see relatively low-speed scan converters being used as less costly A/D converters. Charge-coupled devices will probably play a big part in this.

One nice thing about scan conversion is the opportunity it affords in the display area. You can get any number of traces on one display in different colors if you have a scan converter in each channel and a color tube. And alphanumeric CRT readout could be color-coded to correspond

Bill Peek



Bill Peek came to Tektronix as a design engineer in 1962. A graduate of Oregon State University, he received his master of engineering degree in 1968. In 1975 after holding various managerial positions in circuit- and instrument-design groups, Bill was promoted to the post of General Manager of the Laboratory Instrument Division. This division is responsible for design, production and marketing of Tektronix Laboratory oscilloscopes, the TM 500 line of test and measurement instrumentation and the new family of logic analyzers.

Bill likes to go camping with his wife and two young sons, and also enjoys woodworking, a hobby that came in handy when he built his own home a few years ago.

to the color of the trace it applied to. This would really make a readout a lot easier—reduce operator error and generally make the scope easier to use.

In any event, once A/D conversion becomes a standard item in waveform analysis, a whole spectrum of operations is opened. Relatively, you have all the time in the world to decide what you want to do with the stored waveform—how you want to display it, what kind of information you want to add to it or get from it, etc.

One thing is clear. We're not going to have a universal scope that's the equivalent of a hand-held calculator.

There are too many differences in customer needs and too many limitations on digital conversion techniques to make that possible. There is no doubt that new instruments will supplant the oscilloscope as the principal troubleshooting tool in *some* applications. We've recognized this by entering the logic analyzer field. There is a possibility that within the next 10 years, due to the

tremendous impact microprocessors will have on all areas of industry, logic-analyzer sales may equal those of oscilloscopes.

Or a new instrument may appear that is even more suitable for the design, test and service of microprocessors. But eventually you still have pulse aberrations and timing relationships to troubleshoot, and power-supply circuits to debug in your microprocessor circuit. You're going to have a whole array of EEs designing controllers for sewing machines, washing machines, automobile carburetion and braking systems, etc.

Electronics, especially the microprocessor, is penetrating new areas every day—areas previously dominated by mechanics, hydraulics, fluidics, etc. And the oscilloscope will follow, maybe not as the principal, but nevertheless as an indispensable troubleshooting tool. For although a logic analyzer or similar instrument may tell you *what* is wrong, it takes a scope to find out *why* it's wrong.

Incidentally, when it gets down to servicing in these new areas, a few people are skeptical that a car mechanic may be using an oscilloscope to troubleshoot a microprocessor. Well, perhaps he won't. But the trouble may not be in the microprocessor itself. It may be in the wiring or in the connections, at the inputs and outputs of the device. Probably most of the problems will be of this kind. Diagnosing these problems will require a fair level of sophistication, and this brings up an interesting point.


Some years ago, when radio and television were coming along there was serious consideration given to the proposition that they would never be a success because there wouldn't be a group of people who could service them. With color television, it was considered impossible. Yet there are now thousands of people who are doing it. And auto mechanics aren't all that different from other people. Look at the military. They have to maintain all sorts of complex, sophisticated electronic equipment. People rise to a challenge in their profession or vocation. In the future it may be a common sight to see an auto mechanic with a special-purpose oscilloscope, finding out what's wrong in an electronic device.

In any event, we believe the oscilloscope has a bright future. Its general configuration, operating parameters, and variety of functions will change to meet the needs of our advancing electronics technology. But its primary function as a basic diagnostic tool will remain. Such tools have a way of staying with us. Remember that in spite of the millions of dollars expended each year on sophisticated medical diagnostic equipment, the physician still carries his stethoscope. ■■

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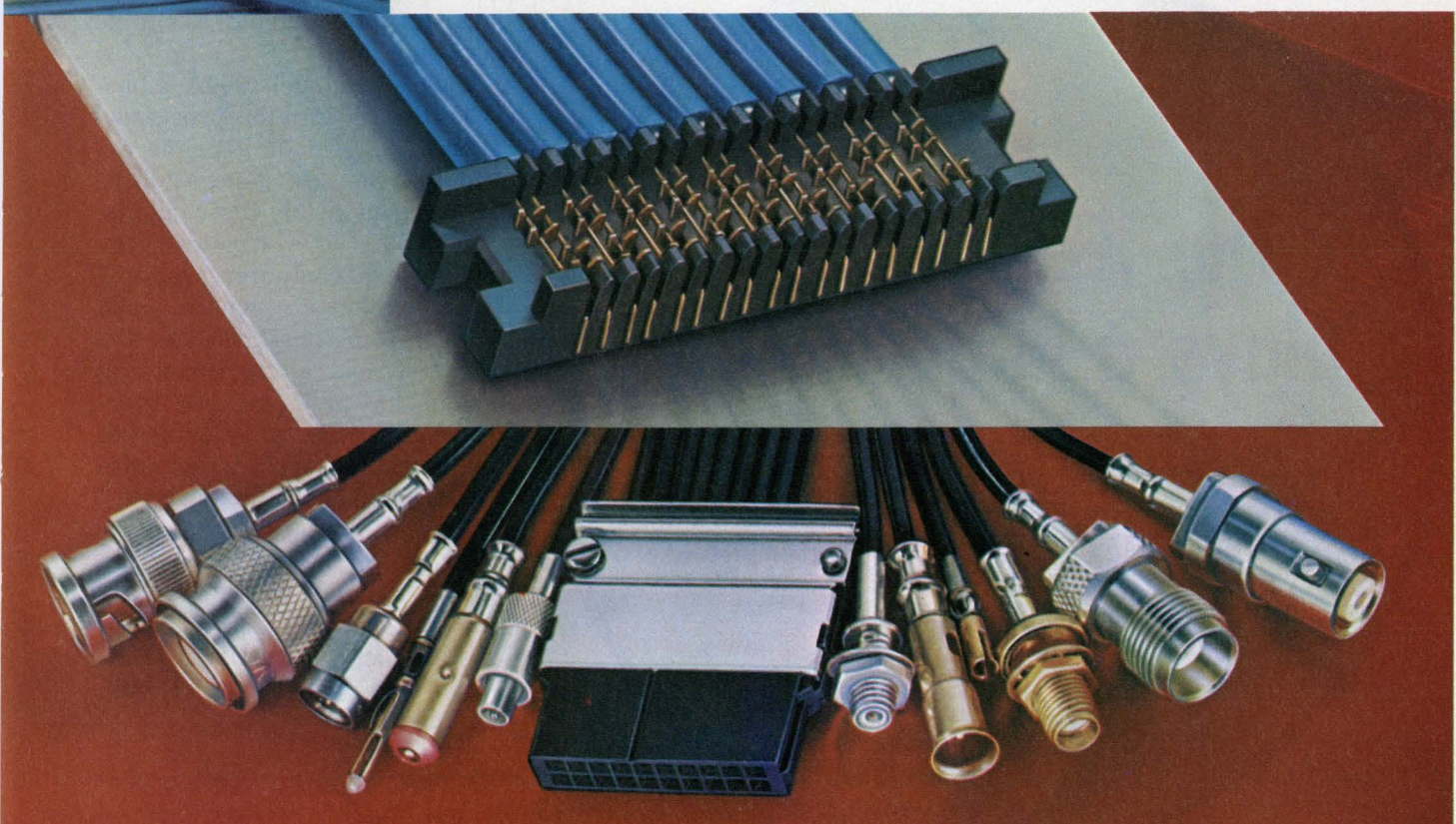
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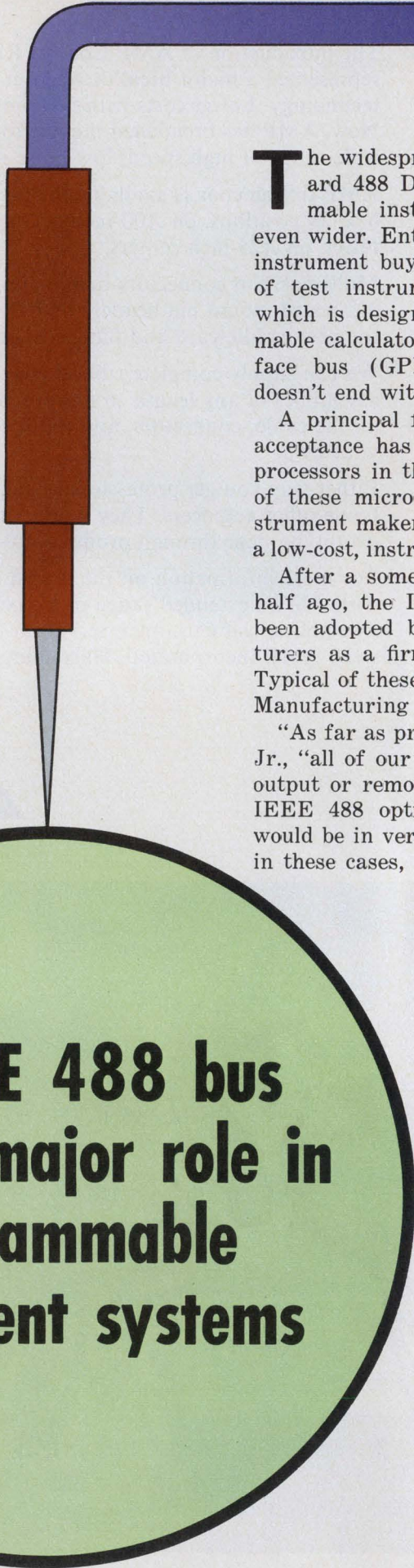
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CIRCLE NUMBER 40



The widespread adoption of the IEEE Standard 488 Digital Interface Bus by programmable instrument manufacturers is getting even wider. Enthusiastic acceptance of the bus by instrument buyers is creating a new generation of test instrumentation, the vast majority of which is designed to be controlled by programmable calculators via this general purpose interface bus (GPIB). Moreover, use of the bus doesn't end with programmable instruments.

A principal factor in the rising tide of GPIB acceptance has been the proliferation of microprocessors in the last year or so. Increasing use of these microprocessors has permitted the instrument makers to provide, among other things, a low-cost, instrument-to-bus interface.

After a somewhat hesitant start a year and a half ago, the IEEE Standard 488 bus has now been adopted by some 50 instrument manufacturers as a firm option for their product lines. Typical of these manufacturers is the John Fluke Manufacturing Co., Mountlake Terrace, WA.

"As far as product planning," says John Fluke, Jr., "all of our new products that have a digital output or remote control capability will have an IEEE 488 option. The only possible exception would be in very low-cost portable products. And in these cases, they would have a crude form of data output to drive a simple bus converter."

The Fluke Model 8500A, a bus-structured, 8080-microprocessor-controlled DVM, is a prime example of the new generation of 488-bus-compatible instruments. "We built the voltmeter very much like a computer system," Fluke explains, "where each function to be performed by the voltmeter has a corresponding module that plugs into an internal bus. The digital interface to the outside world plugs into slots provided for that purpose."

Three interface cards are available for the instrument: an RS-232-C serial module, a duplex-parallel interface designed for interfacing directly to minicomputers, and the IEEE 488 interface.

**The IEEE 488 bus
plays a major role in
programmable
instrument systems**

Jim McDermott
Eastern Editor

Microprocessors and the 488 busses are being combined in instrumentation to provide a total system capability far beyond that originally envisioned for the bus, according to Pete Silvernail, group engineer at Wavetek, San Diego. Distributed processing or networking makes use of the intelligence scattered throughout the system in each instrument interconnected by the bus, Silvernail explains.

The original intention for the 488 bus developed by Hewlett-Packard was that it enable the user to assemble a group of bench-top measuring instruments and signal sources into systems that could be easily assembled or reconfigured.

But now the bus is finding a home in military radar systems, process-control systems, interfacing with the IEEE Standard 583 Standard Modular Instrumentation and Digital Interface System, usually called Camac (Computer-automated measurement and control), as well as in large-scale automatic test equipment systems.

Bus gives distributed processing capability

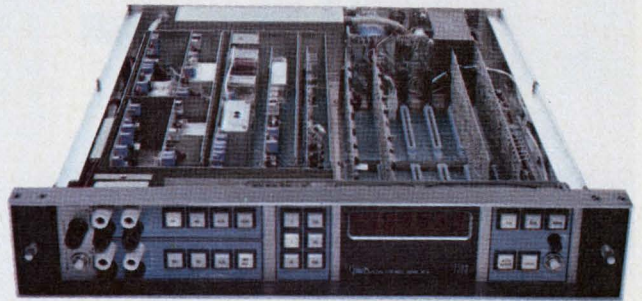
The distributed processing capability of a system configured around the 488 bus provides a powerful tool for the instrumentation-system user, which means, according to Silvernail, that processing is shared by the calculator and the various microprocessors throughout the system. Thus, processing done at the relatively slow 1-Mb/s maximum speed of the 488 bus is substantially higher.

So Silvernail doesn't see any significant need for superspeed on the GPIB bus. But what he does see is a great need for the ability to tell instruments exactly what to do and for the instruments to respond by telling what they're doing.

These "command structures" have been incorporated into the Wavetek Model 172 Programmable Signal Source, according to Silvernail. The 172 is a combination oscillator, waveform generator, pulse generator and synthesizer, all of which are manually or remotely programmable. The instrument can generate sine, square, triangle, pulse, ramp, haversine, havertriangle and dc-level waveforms on command.

The 172 has the widest frequency range of any programmable function generator today, says Silvernail, and operates from 0.0001 Hz to 13 MHz, with the synthesizer portion operating from 10 Hz to 13 MHz.

In the 172's command structure, the instrument receives and stores a set of instructions



This 5-1/2-digit programmable multimeter provides 1000 conversions per second. The Model 7500, by Data Precision, is also a universal ratiometer accepting any input combination.



Up to 10 of these Wavetek Model 172 programmable function generators can be controlled at one time through a 488 interface with optical isolation.

from the calculator (or controller) during slack or initialization time. Only then is it necessary to use a hand-wave signal that essentially says: "Now do this or that." This type of distributed operation reduces traffic on the bus significantly.

The 172 talks back

The 172 is the first machine to have an alphanumeric display that states what is happening within the instrument in English, French or German. For example, upon entering either a front-panel or remote frequency, the display reads: "Frequency is XX kHz," in one of the three languages.

On the other hand, if the range is exceeded, the display states: "Frequency range exceeded," and the excess is not indicated by the usual blinking LED, as with other instruments.



This automatic test set for transceiver measurements, by Rohde & Schwarz, is controlled through the IEEE bus by a programmable calculator. Card readers can also be used for system control.

While the 488-bus interface has been implemented initially in measuring and signal-generating instruments, Silvernail foresees the bus being adopted by display and storage systems as well.

"Within five years, every printer and plotter will be interfaced with the GPIB," he predicts. "I also say that many magnetic tapes and floppy discs will have that interface."

The move is to larger systems

In addition to being incorporated into programmable instruments, the 488 interface is being incorporated into computer-operated systems, according to Don Loughry, a Hewlett-Packard corporate interface engineer. Several other manufacturers are now providing bus-port interfaces, he adds.

A computer-controlled test system in Fairchild's new Logic System VII that uses multi-processor techniques employs the 488 bus to simplify the addition of programmable instrumentation. And the latest disc-based Logic-Circuit Test System from GenRad, Concord, MA—the 1795—has an optional 488 instrumentation port.

The 488 bus's distributed-processing capability that links a group of microprocessors has been

adapted to an application for which it was not originally conceived—an aircraft search system under development at MIT's Lincoln Laboratory. The bus's ability to connect several components of the radar system has simplified the system by eliminating the central computer needed in previous systems.

"While we've already used the bus on a small airborne radar, we have five or six other radar projects that we're going to use it on," says C. Ed Muhe, leader of the radar-techniques group at the Lincoln Laboratory.

Bus is central system element

"With the usual digital system, the first thing you think about is the central computer," Muhe notes. "But with the bus, we do just the opposite, we think of the bus as the central element of the system. And all the functional modules tie onto the bus."

"The basic idea is to functionally divide the system into parts that require the minimum amount of communication between them. We put enough microprocessor intelligence into each part so that communication on the bus is fairly small."

"As an example, the digital display has to be refreshed about 30 times a second, and the refresh function is put into the display with a local microprocessor. The display is updated only when there are changes in it, and this update is easily handled by the bus using rates of about 0.5 Mbytes per second."

Slow or fast μ Ps are used, depending on the requirements, Muhe points out, and the 8080 and 2901 are Lincoln Laboratory's favorite choices.

The bus saves substantial design time—a major advantage, according to Muhe. Using the 488 with standard building blocks to construct the radar systems means, for example, that a display can be connected with its μ P into another radar. With the standard interface, it's necessary only to plug it into the bus.

"While I know the bus offers a tremendous advantage in designing several systems using the same functional units, I think that the bus means less design work even for one system," Muhe concludes.

Programming is still a problem

Eugene Fisher, design engineer at the University of California's Lawrence Livermore Laboratory, Livermore, CA, is enthusiastic about using the 488 for interfacing instruments to mini-computers at the laboratory. With the proper bus interface, Fisher points out, he can acquire an



A microprocessor-based digital plotter, the Tektronix 4662, is a leader in the trend to provide plotters with the IEEE 488 general purpose interface as standard.

instrument for a particular instrumentation set-up and simply plug it in.

"All I have to do then," he notes, "is learn how to program it," notes Fisher, adding: "This is a continuing problem with each new instrument because each instrument manufacturer is interpreting the bus specification slightly differently."

Programming individual instruments has been a problem for some time because it has not been spelled out in the original specs.

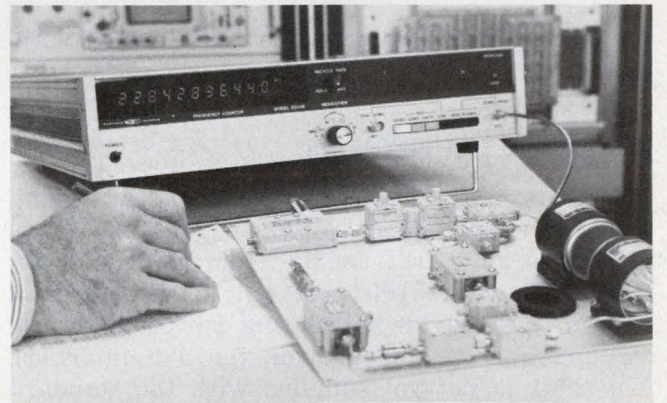
"Work is continuing in the standards area relative to software," says Don Loughry. "I prefer to call software 'codes and formats.' Draft documents are being generated and will be reviewed this month at the International Level in Europe in the parent committee of Technical Committee 66."

Historically, the interface of early programmable instruments has been the parallel, four-bit BCD bus, which is still available in standard form in the majority of today's instruments. But the demand for it is falling while the demand for the 488 interface rises.

As a result, instruments already on the market, but still reliable and highly useful, are now being retrofitted with IEEE 488 interface cards or modules. The Model 605-145 ASCII interface developed for Exact Electronics Models 605 and 606 Programmable Waveform Generators is a good



The status of the HP-IB bus as well as the range and the function to which the meter is set are provided automatically by this Hewlett-Packard 3455A DVM.



Fully automatic frequency measurements from 0.02 to 24 GHz can be made with this Systron-Donner 6054B Microwave Counter. The IEEE interface is optional.

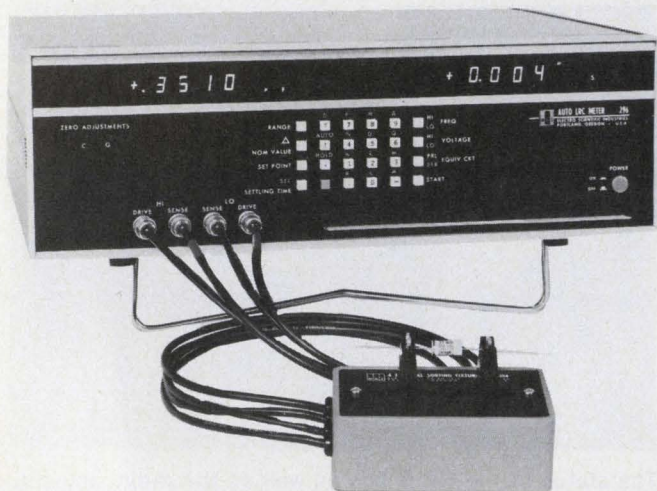
example. Only an inch and a half high, the new 488 interface module of the Hillsboro, OR, firm sits on top of the 3-1/2-in. rack package of the 605 and 606. The total package is only 5-1/4-in. high and fits into a 19-in. rack.

Keithley's new portable 4-1/2-digit, 30,000-count DMMs, Models 172 and 173, are being provided with a 6800 μ P-based IEEE 488 interface module (available in January, 1977).

Because these instruments are small, the interface module of the Cleveland manufacturer is a separate unit, not a plug-in card.

Three DVMs from Dana Laboratories—the 5000, 5900 and the 6900—are designed with integral BCD outputs. A piggyback package of the Irvine, CA, firm, the 55, designed with a microprocessor-controlled interface, is used for interfacing between the BCD outputs and the IEEE 488 bus.

For the Dana 9000 Counter-Timer, which uses



A complete automatic measuring system for production or incoming inspection is provided by this Electro Scientific Industries LCR bridge. It has a 6800 μ P.

an Intel 4004, the interface is incorporated within the box.

The number just gets bigger

Microprocessor interfaces are found in a number of other instruments. For example, the Model 296 wide-range LCR bridge from Electro Scientific Industries, Hillsboro, OR, incorporates a 6800 μ P to provide calculating power in the instrument as well as provide the 488 interface. The 2961 is not yet supplied with the standard BCD outputs.

"The instrument can be programmed remotely, including sequencing a mixture of tests," according to Jim Carrier, instrument product manager. "For example, a capacitor can be measured, followed by a resistor. Or it can be controlled to provide multiple-component, high-speed testing.

"A 10-limit sorting capability is available, using a plug-in option card," Carrier continues. "So, with one instrument you have a complete measuring system for production or incoming inspection."

A special feature incorporated in the digital bridge is the ability to do either percentage deviation or absolute deviation. Instruments have traditionally come with either deviation measurement.

The instrument program can be changed easily by simply substituting another program ROM in the μ P, notes Carrier.

The SMPU Test Assembly by Rohde & Schwarz, Fairfield, NJ, is a microprocessor-controlled, IEEE-bus compatible automatic test set for transceiver measurements. The system, whose



A calculator-controlled automatic test system for four-point probe applications, the Keithley System 53 contains a current source, DMM, 10-channel scanner and interface units.

deliveries have just begun, contains multiple instruments required to test both transmitters and receivers automatically.

Control comes from a card reader or through the Tektronix TEK 31 programmable calculator. Where more elaborate programming facilities are required, the Tektronix 4501 Graphic Computer system is used.

The SMPU is connected to the calculator through the IEEE bus.

The microprocessor is used for setting up and maintaining subroutines and for preventing erroneous and potentially destructive measurements. For example, if the transmitter test is selected by pushing the "transmitter" button, no type of receiver test can be called up, because the system will refuse it.

Not all microprocessors used in instruments function as a part of the bus interface. For example, the 4004 μ P in the Systron-Donner 7115 DMM provides intelligence for internal data calculations, self-calibration and troubleshooting.

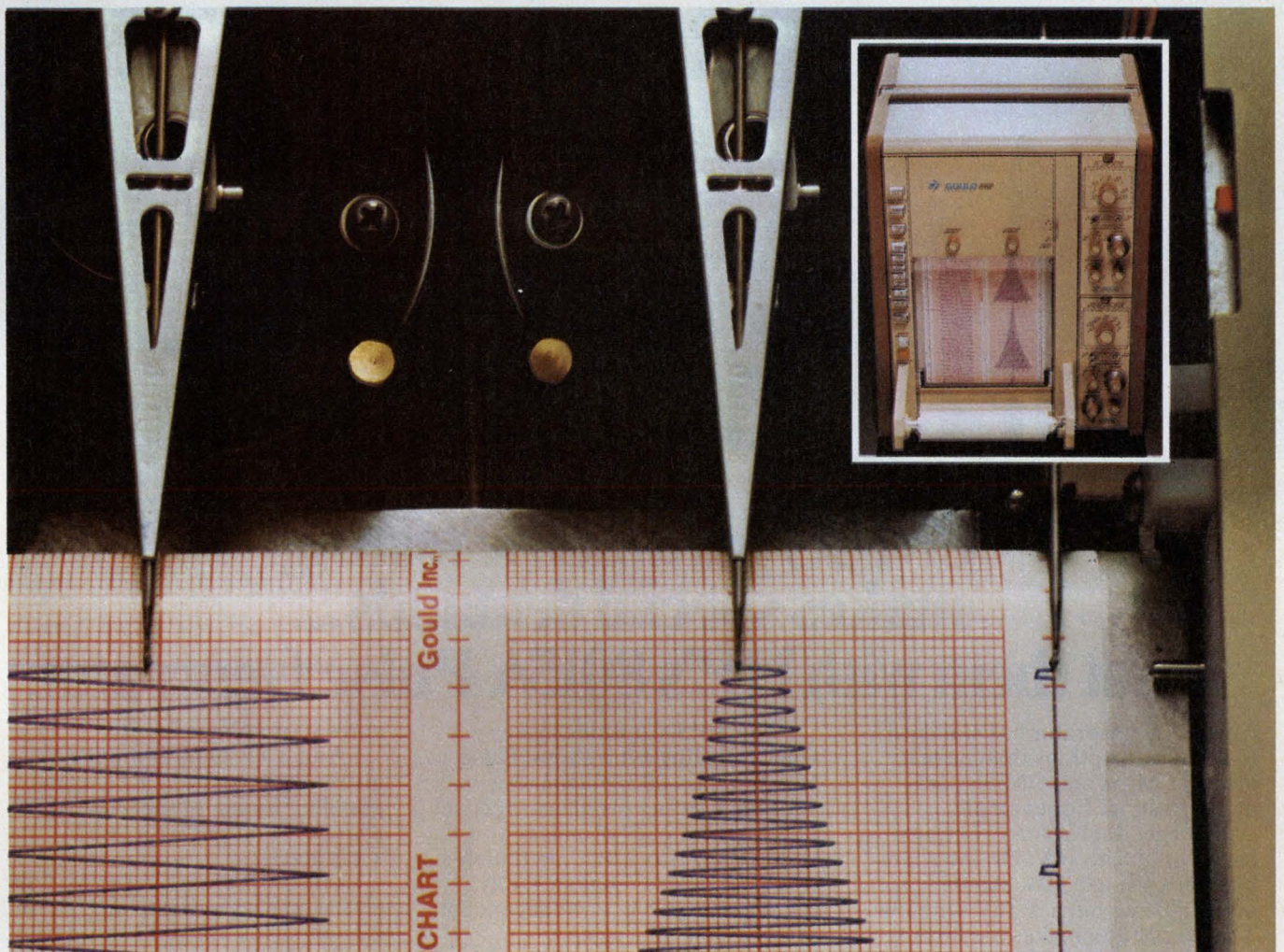
In the 7115—and in three other of the Concord, CA, manufacturer's instruments that interface with the 488 bus—the DPS 50 Power Supply, the 1600-series Microwave Synthesizers and the 6054B Microwave Counter are normally supplied with the BCD and the 488 interfaces as plug-in card options.

Camac systems take the 488 bus

The influence of the GPIB is spreading to the process-control field. Users of the Camac systems (IEEE 583) are providing the 488 bus with interfaces so that instruments that are physically incompatible with the Camac modular system of hardware—programmable attenuators, DVMs, and displays, among others—may be added.

Use of the Camac system is pretty much divided between nuclear instrumentation and process-control instrumentation. ■■

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Instrument as shown has pulse-burst option and optional handles.

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This pulse generator has standard features and options that make it ideal for MOS and CMOS parametric testing. For example:

You get dual-channel outputs, each variable to 16V. Or, they combine into a single 30V channel adjustable within a $\pm 16V$ window. That versatility makes the 8015A compatible with CMOS, and most MOS devices. You can delay channel B with respect to A for generating 2-phase nonoverlapping clocks. And combine the adjustable B delay with A + B to generate three-level signals.

Selectable source impedance on both channels lets you choose the best output termination configuration for your application. Of course you can vary the width (10ns to 1s), transition time (6ns to 0.5s), and rate (1Hz to 50 MHz). High-speed capability lets you work with advanced TTL and HTL logic as well as MOS. And low rep. rates or manual operation let you slowly step through logic states.

The 8015A options makes CMOS testing even easier. Pulse Burst (option 002) eliminates conventional gating problems. Just set the exact number of pulses you want (from 1 to 9,999) on thumb-wheel switches. That's exactly the number you get... independent of pulse-rate settings.

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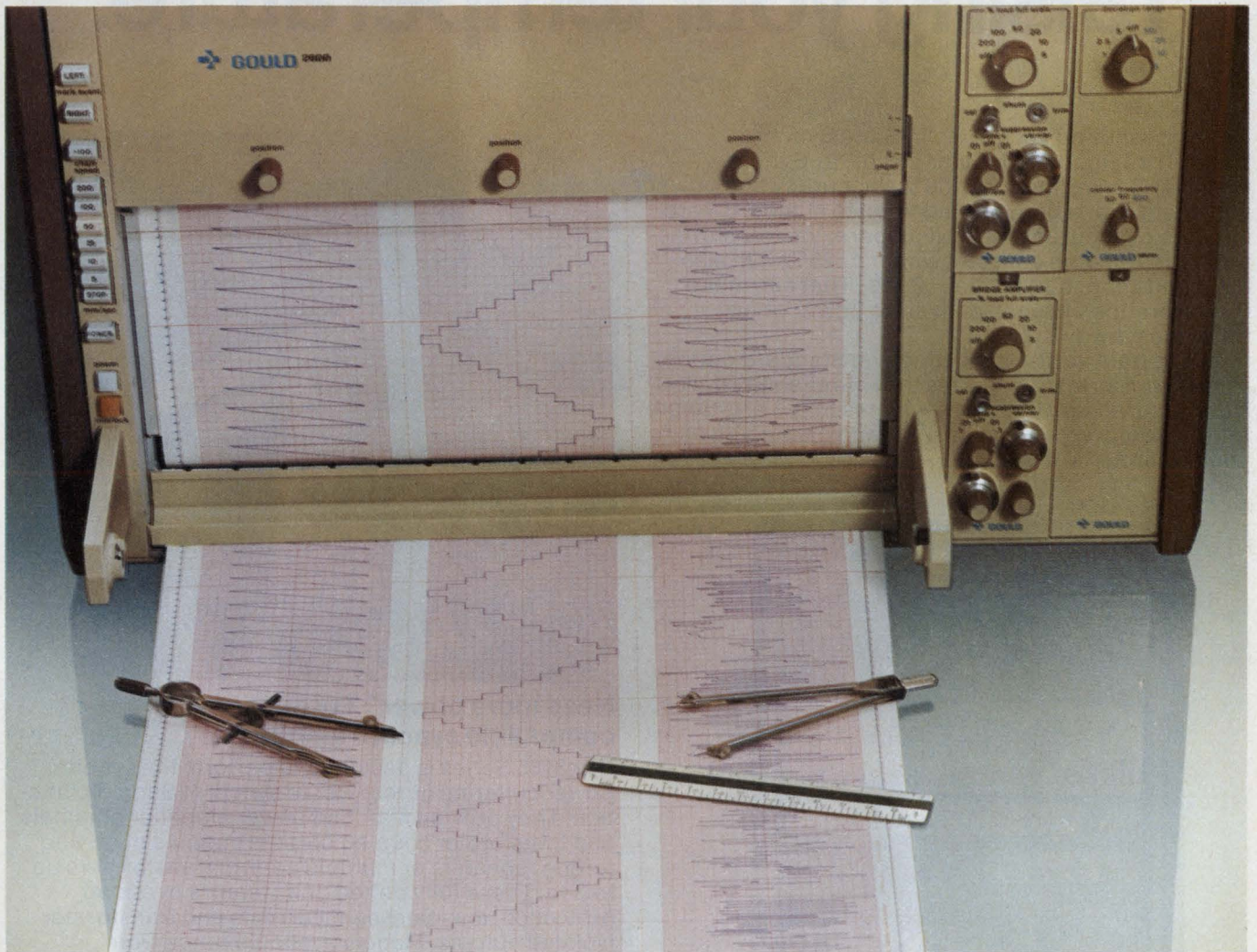
Contact your local HP field engineer for all the details. Or, write for the 8015A and 8011A data sheets and our Application Note 195 — "Pulse Generator Techniques in CMOS Applications."

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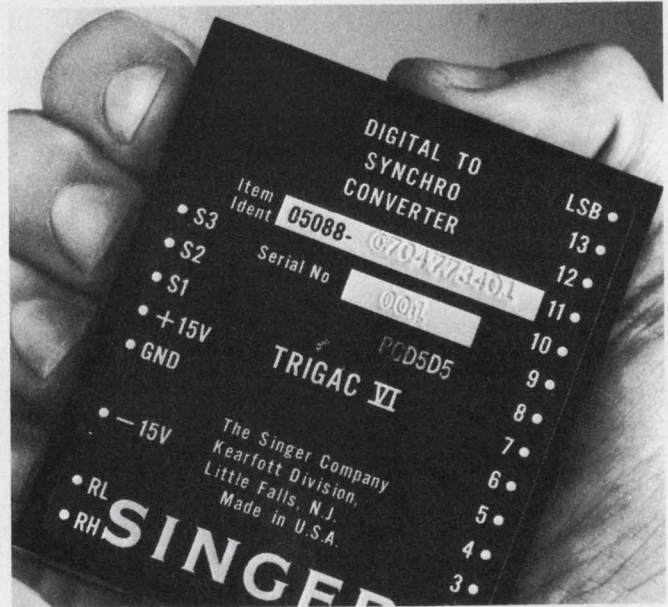
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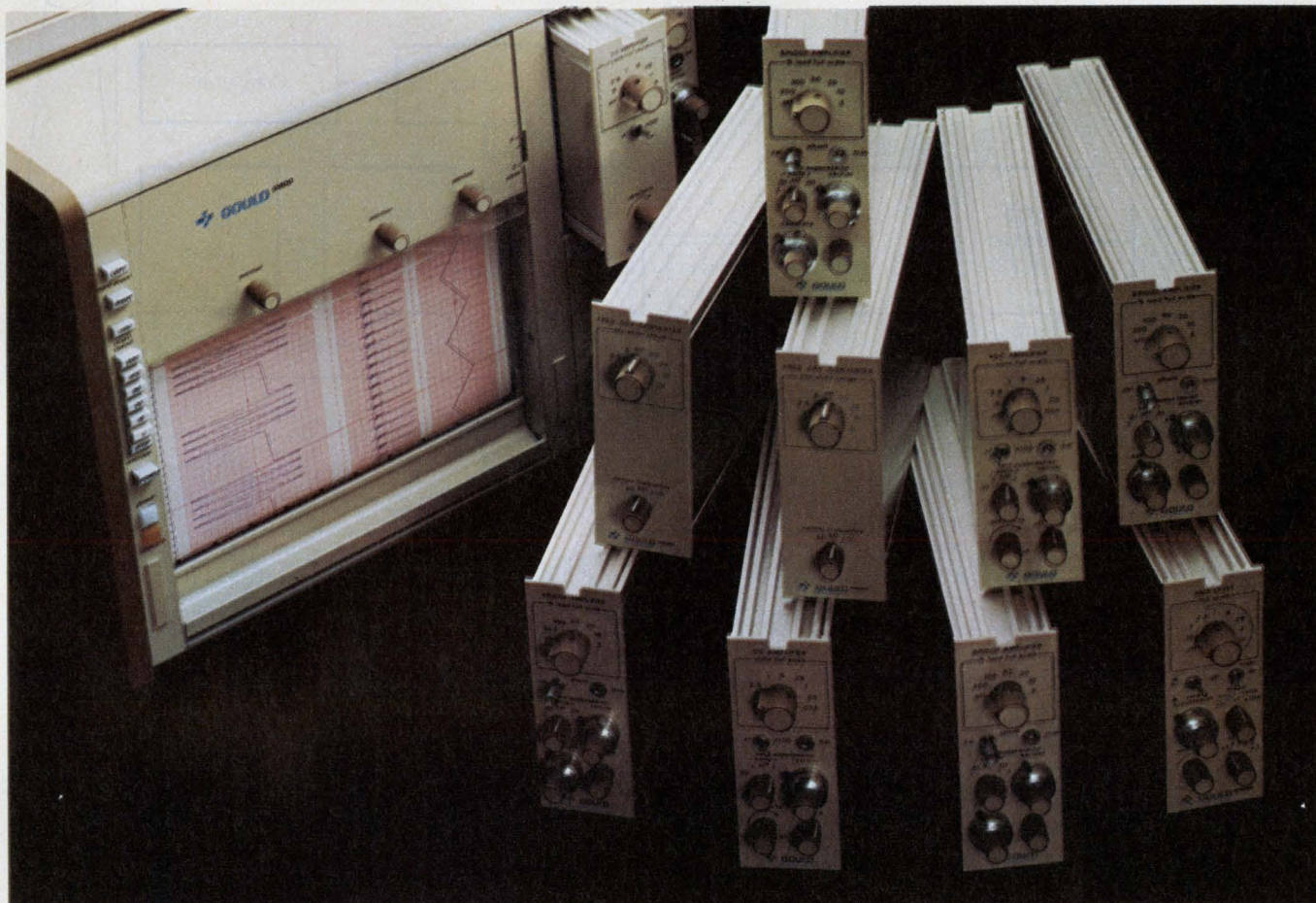
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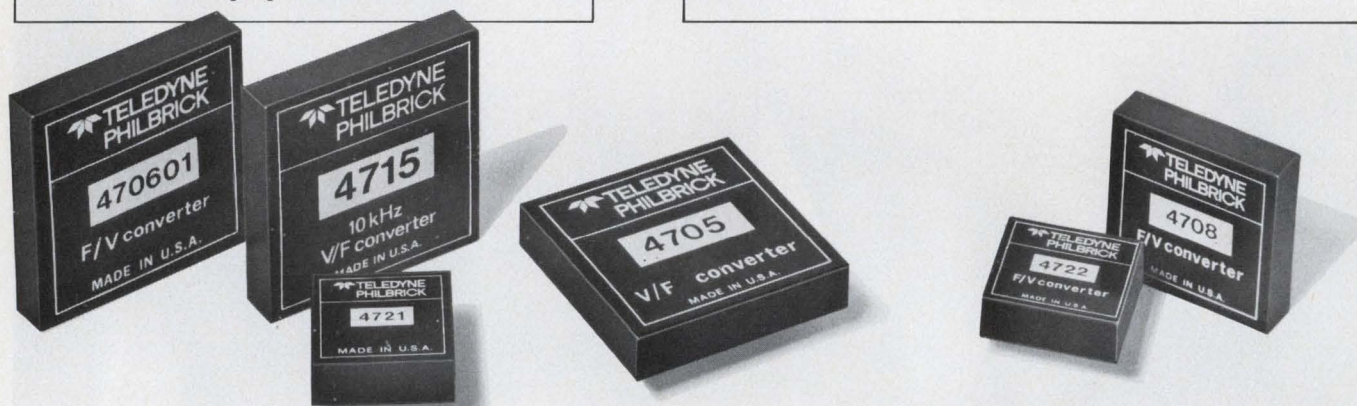
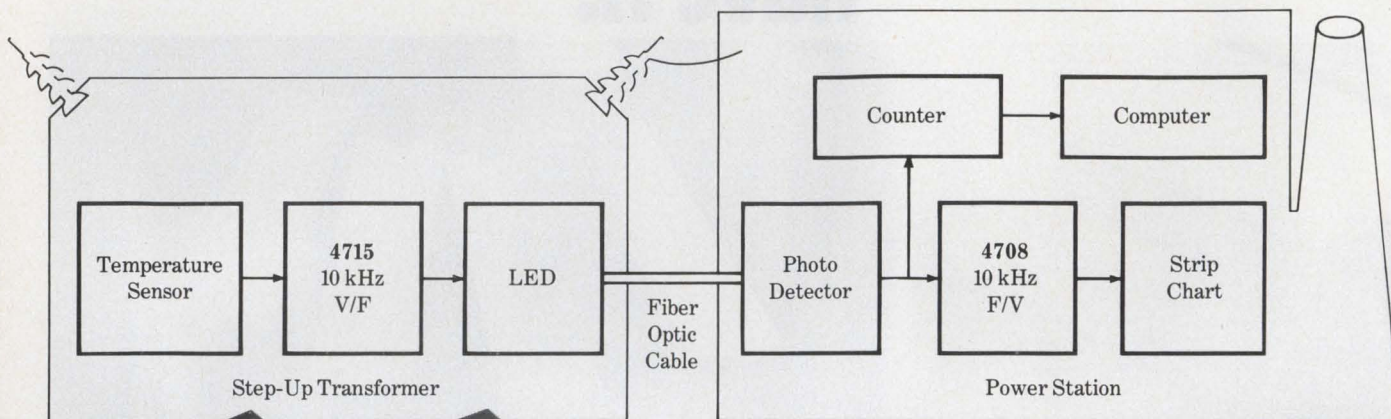
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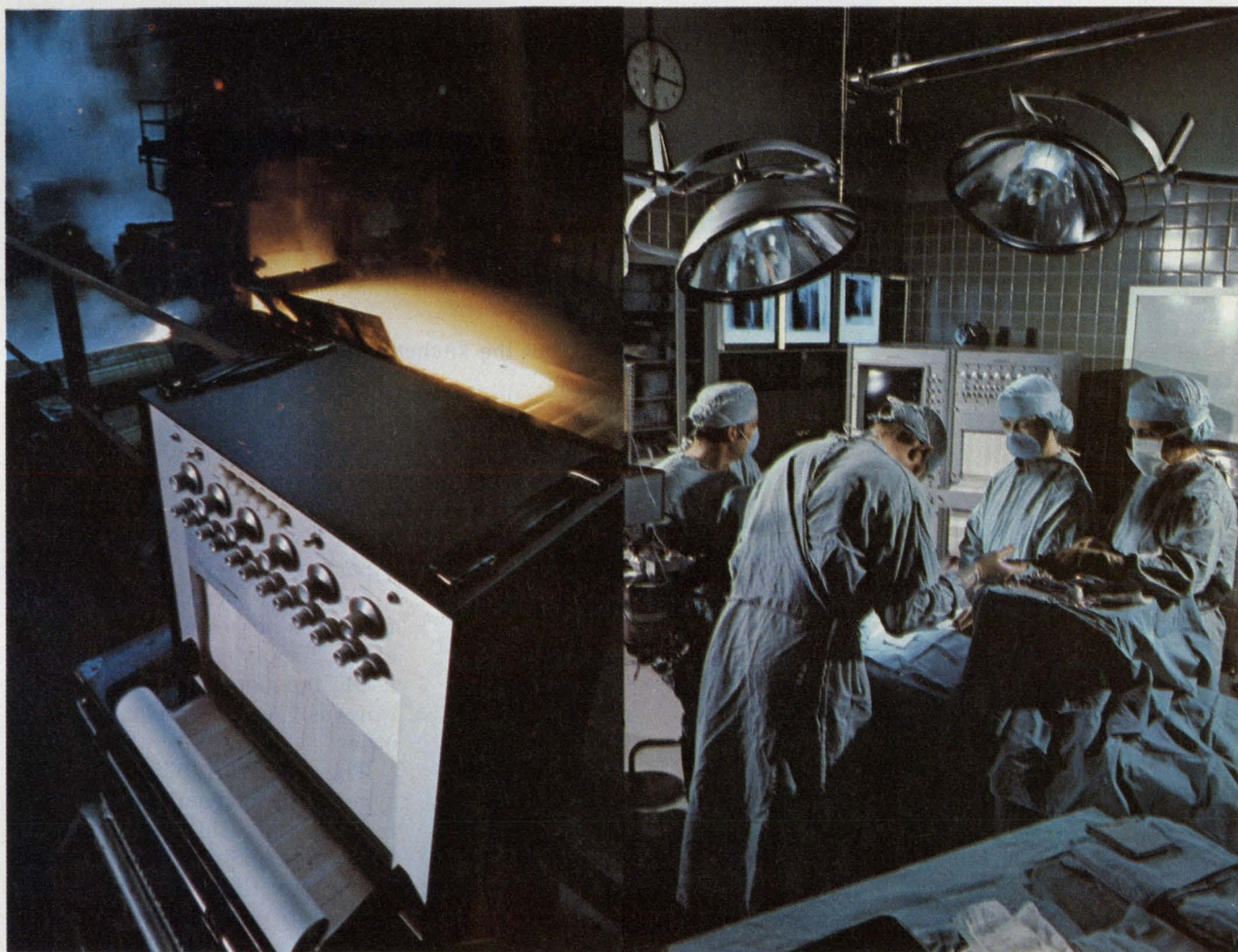
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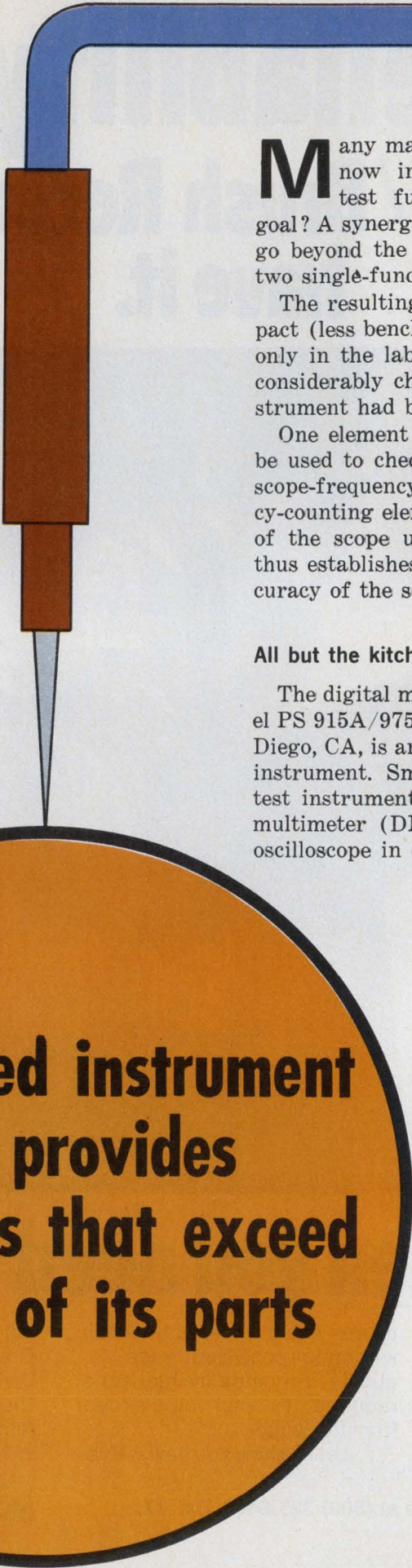
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CIRCLE NUMBER 47



Many major instrument manufacturers are now integrating a variety of different test functions into a single unit. The goal? A synergistic instrument with features that go beyond the result of simply putting together two single-function instruments.

The resulting instrument is usually more compact (less bench space needed), easier to use (not only in the lab but also in the field), and often considerably cheaper than if each component instrument had been purchased separately.

One element of the combined device can often be used to check another. In a combined oscilloscope-frequency meter, for example the frequency-counting element can provide a digital readout of the scope unit's sweep rate. This capability thus establishes a separate verification of the accuracy of the scope's sweep-speed dial setting.

All but the kitchen sink

The digital multimeter-counter-miniscope, Model PS 915A/975A (\$1295) by Vu-Data Corp., San Diego, CA, is an example of this new breed of test instrument. Small despite its lengthy title, this test instrument is the first to combine a digital multimeter (DMM), a frequency counter and an oscilloscope in one package.

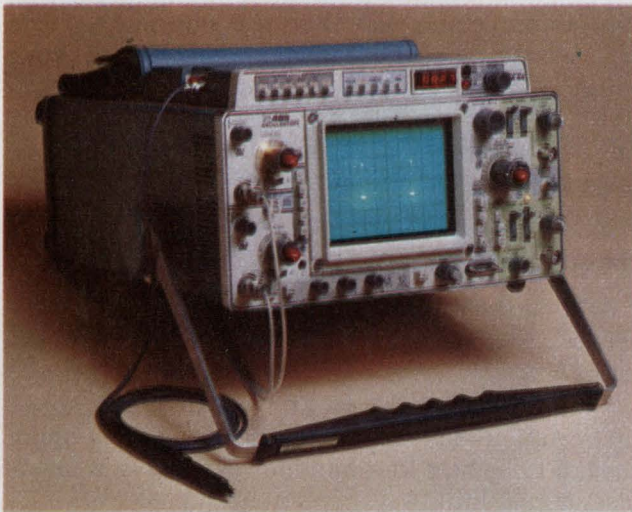
Each of these measurement functions possesses its own dedicated display, and each may be used independently or simultaneously, or to complement each other.

The PS 915A/975A provides synergistic convenience by connecting all three component units internally. Only a single probe (to the item tested) is needed to permit test measurements. This arrangement eliminates the often cumbersome external wiring interconnections required among the three instruments when used separately or even together.

Performing a conventional set of measurements on a power-supply circuit provides a good example of the convenience offered by such a combined instrument. The DMM portion can

**A combined instrument
often provides
capabilities that exceed
the sum of its parts**

Samuel Derman
Associate Editor



Measuring time intervals (to 1% accuracy), voltage, resistance, and even temperature (all digitally) is possible with the Tektronix DM 44 scope option.

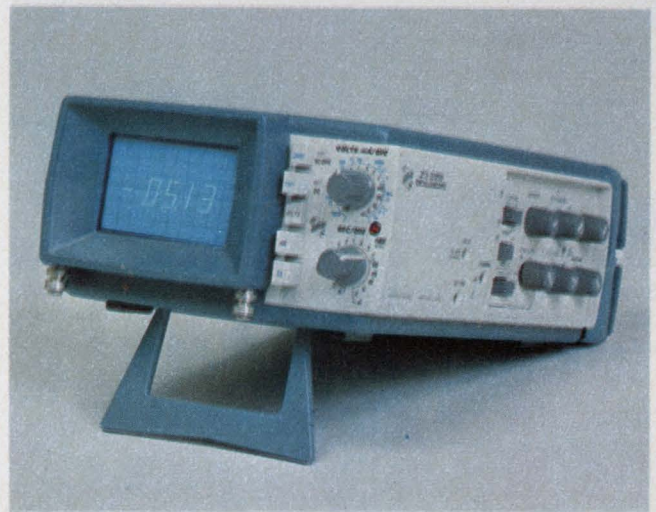
measure and display the dc level, while the ac ripple amplitude is displayed on the scope's CRT. At the same time, the ripple frequency is monitored and displayed digitally by the counter.

The Vu-Data PS 915A/975A is basically three instruments in one:

- An autoranging DMM, with its readings displayed on a 3-1/2-digit LED panel, measures ac and dc voltage as well as resistance.
- The scope, which carries its own model number, PS 915, provides vertical sensitivity of 10



A DMM, frequency counter and scope, all in one compact package, Vu-Data Corp.'s Model PS 915A/975A can be used on ac, dc, or battery.



Tektronix Model 213, a combined DMM oscilloscope, weighs 3.7 lb. The 3-1/2-digit display appears on the CRT of the dc-to-1-MHz scope.

mV per division at a 20-MHz bandwidth. Fastest sweep rate is 100 ns per division with the possibility of an increase to 20 ns per division by a five-times magnifier.

- The frequency counter, which is activated by the scope's trigger pulses, digitally presents the frequency of the signal displayed on the scope's CRT.

An "external-trigger" scope mode is also available, so that the frequency of the externally applied signal can be measured, whether this signal is displayed on the scope or not. A full four-digit LED display supplies the frequency readout.

In the "ac volts" mode, the device's DMM will give the RMS value of a sine wave appearing on the scope, so "eyeball" measurements of the peak-to-peak voltage amplitude, followed by the usual calculation to reduce this measurement to RMS value, are unnecessary.

Compact capability

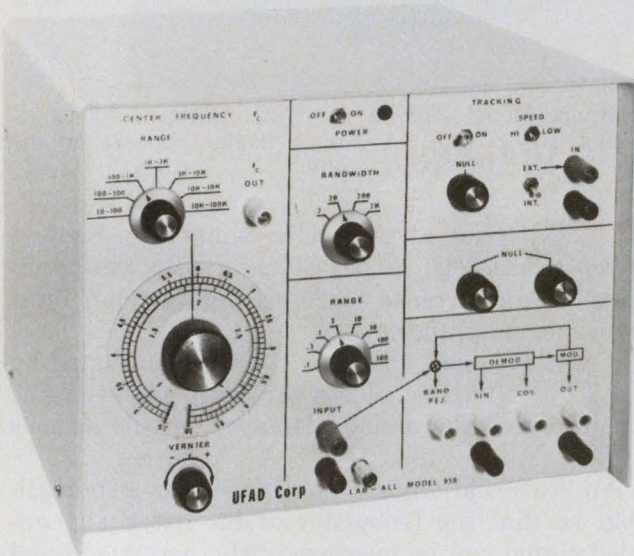
A serious competitor in the combined-instrument race is the Versatester by Systron-Donner Corp., Concord, CA. Designed not only for R&D work but also as a production and service test instrument, Versatester combines a multimeter, a signal generator and a frequency counter in a compact package. A single four-digit LED display with automatic decimal point supplies the readout for all component instruments.

Versatester offers a useful variety of devices and functions:

- 20-MHz frequency counter with autoranging.
- 20-MHz pulse generator.



Systron-Donner's Versatester generates pulse, square and sine waves from 20 Hz to 20 MHz. It also functions as a dc power supply and as a 4-digit multimeter.



Lab-All, manufactured by UFAD Corp., uses a precise filter to perform a wide variety of signal phase, spectrum and distortion analyses.

- 20-MHz square-wave generator.
- 20-MHz sine-wave generator.
- Dc-power supply (available voltages are +5 V, ± 15 V and ± 30 V).
- Multimeter (ac, dc and ohms) with a four-digit readout. In ac-voltage mode, voltages can be measured whose frequency is as high as 20 MHz.

Versatester's instruments all run continuously. For example, a sine-wave output is available simultaneously with pulse or square-wave output. Also, the multimeter modes can operate at the same time any one of the signal-generating modes is used.

The digital readout permits precise digital setting of sine-wave amplitude, upper and lower levels of the pulse and square-wave outputs, and power-supply output voltage to ± 10 V. Resolution in the dc-measurement mode is 0.1 mV and 0.1 mV RMS for ac.

The Versatester's synergism results in cost effectiveness, convenience, and portability. The cost is appreciably less than the sum of the costs of Versatester's individual components, says Norm Whitla, Systron-Donner's product manager. There are hidden savings too, Whitla adds. Fewer spare parts need be stocked, and only the one, basic instrument must be calibrated.

Pint-sized test package

Joining the race is a digital multimeter (DMM) and oscilloscope (\$1200) from Tektronix, Beaverton, OR.

Weighing in at 3.7 lb and occupying a space $3.0 \times 5.2 \times 8.9$ inches, the Model 213 is small enough to be held in a hand, or carried in a briefcase or tool kit.

Unlike the Systron-Donner Versatester and the Vu-Data PS 915A/975A, which use LEDs for the digital display, the 213's numeric figures are projected directly on the CRT face (in 3-1/2-digit format). Although this arrangement does not permit the operator to view the waveform and read the voltage simultaneously, a single pushbutton switch permits instant changeover from one type of display to the other.

The DMM can measure voltage (dc and RMS ac), ohms and current. Measurable dc voltages range from 0.1 V to 1000 V, and measurable current from 0.1 mA to 1 A full-scale. Resolution of the DMM is specified as 100 μ V for voltage measurements and 100 nA for current readings. Frequency range of the 213's scope is from dc to 1 MHz. The scope can also display current waveforms, unlike most field scopes of this type.

A second multifunction test device from Tektronix, the DM 44, is not a complete piece of test gear, but an attachable module for the Tektronix 464, 465, 466, 475 and 475A portable oscilloscopes. This optional feature provides:

- 3-1/2-digit LED readout.
- Direct numerical readout (with 1% accuracy) of the time interval between two signals presented on the scope's CRT.
- Delta-delayed sweep for very fast time measurements (i.e., pulse width, rise time).
- Dc-voltage measurements with 0.1% accuracy.
- Resistance measurements with 0.25% accuracy.
- Temperature measurement from -55 C to $+150$ C.

Linking the DM 44 module to an oscilloscope produces a highly versatile piece of test equipment—one that can make precise timing measurements (1% accuracy) and can perform gen-

eral circuit troubleshooting. The DM 44 option adds \$410 to the price of the selected oscilloscope. The temperature probe can be omitted if not required, however, and the price drops to \$335.

A DMM you can count on

For applications that require a frequency counter combined with the capabilities of a DMM, Valhalla Scientific Inc., San Diego, CA, has a 4-1/2-digit multimeter counter Model 4440.

For \$299 (plus an extra \$50 for the counter option), the purchaser gets several capabilities: dc and ac (RMS) voltage measurements from 200 mV to 1000 V, input impedance of 1000 megohms on the 200-mV and 2-V ranges and 10 megohms on all other ranges, current measurement (dc and ac) from 200 μ A to 2000 mA, resistance measurements from 200 Ω to 20 k Ω , and frequency counting from 2 kHz to 20 MHz, with accuracy of 0.01% \pm 0.005% of full scale.

The frequency counter is actually usable 7 MHz beyond its 20 MHz limit for measuring citizens band (CB) signals, says Harold Clark, Valhalla's president. Above 20 MHz, the counter indicates "overflow," and the first significant digit of the readout is missing. However, since CB frequencies all fall into the 26 and 27-MHz range, the value "2" for the first digit is understood.

A variety of available options extends the capability of the Model 4440.

For data-communications measurements, the user can determine the time duration of the tone burst signal—a low frequency sine wave burst sent over telephone lines to indicate that a remote operator wishes to communicate with a computer. The duration of such signals must be precisely controlled, and in cases where dozens, even hundreds of telephone lines link up to a central computer, checking out these time intervals can be exceptionally tedious. The 4440's data-communication option speeds up this testing process.

Temperatures can be measured via an optional probe that generates a dc voltage of 1 mV/ $^{\circ}$ C. When the user switches the digital multimeter to the 200-mV range, the meter becomes a direct reading thermometer up to a maximum of 150 C. Temperature resolution is specified as 0.01 C, but over-all temperature accuracy is limited to 2 C.

A pulse generator/power supply package, the Logiklab 151 (\$79.50) from Integral Electronics Corp., Commack, NY, is designed to be both a lab-testing device and a teaching tool.

The power supply is highly regulated, short-circuit proof and capable of delivering 1 A at 5 V dc. The signal source in the astable mode



A combined frequency counter and DMM with 4-1/2-digit readout, Valhalla Scientific's Model 4440 measures voltages to 1000 V and frequencies up to 20 MHz.

simultaneously provides true and complementary TTL-compatible square waves and pulses ranging from 10 Hz to 100 kHz.

In the monostable mode, single pulses whose widths vary continuously from 5 μ s to 50 ms are produced by either a manual or remote trigger.

Multimeter race is on

A tendency within the combined-instrument trend is to add temperature-measuring capability to the gamut of multimeter functions. Harold Clark, president of Valhalla Scientific, explains:

"Let's say a design engineer—one who typically uses a multimeter—has designed something that uses a power transistor. The power transistor gets hot, and the engineer needs to know just what the temperature rise is. That's a pretty universal need.

"Now he's not willing to go out and spend \$1000 on a temperature-measuring digital meter. So if you (the manufacturer) have a low-cost temperature-measuring option on your multimeter, the engineer will buy your product."

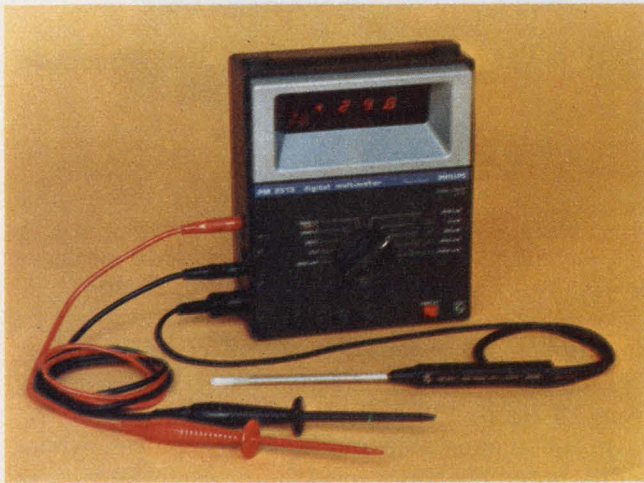
Philips Test and Measuring Instruments, Woodbury, NY, and Logical Technical Services (LTS) Corp., New York City are just two of a growing number of firms that currently offer a multimeter that can measure temperature.

Philips has two models available, the PM2513 and the PM2527. Using an LSI circuit, the 2513 multimeter functions with 26 ranges and a temperature-measuring option (-50 to 200 C)—all

within its 3-lb package. A 3-1/2-digit LED read-out provides the display.

Higher accuracy, autoranging, extended dc-voltage range, 4-1/2-digit display, and wide bandwidth on ac measurements (30 Hz to 100 kHz) come with Model 2527. This version not only can read surface temperatures between -60 and $+200$ C, but also can measure the surface temperature to 99% of final value within 10 seconds (See ED No. 11, May 24, 1976, p. 137).

A small hand-held DMM from LTS uses a semiconductor junction tip to provide tempera-



Philips Model PM 2513 DMM is also equipped to measure temperatures. Temperature range is -50 C to $+200$ C, with resolution to 0.1 C and accuracy of ± 1 degree.

ture-measuring capability. Autoranging and autopolarity also come with this Model 12T, which supplies readings via a 3-1/2-digit LED display. Accuracy for dc-voltage measurements is specified as 0.1%, and temperature-measurement range is -55 to $+153.5$ C.

Four AA-sized rechargeable NiCd batteries provide power for the 12T, which also has an ac adaptor/charger. (See "Portable Instruments: The Specs Are Fine, but Their Batteries Are Still Short-Lived," p. 60.)

A new phase in measurements

A single low-cost (\$2495) instrument from UFAD Corp., Grand Rapids, MI, simultaneously measures phase shift, voltage gain, and network distortion.

Known as Lab-All, the device uses a filter to select a precise band of frequencies. The exact bandwidth can be set to customer's specifications anywhere from 0.01 to 3000 Hz.

Determining the frequency components of a complex signal is just one of the many functions this filter can perform. Not only can the filter's

center frequency be positioned manually anywhere in the band from 30 Hz to 100 kHz with a front-panel control, but the filter can also be caused to sweep through a range of frequencies—in the manner of a spectrum analyzer—by injecting an external sawtooth voltage.

Lab-All comes with the following:

- Tracking bandpass filter (constant area filter). Shape of bandpass is such that at 60 dB down, bandwidth is only twenty times the 3 dB bandwidth.

- Quadrature outputs. At the selected frequency, dc voltages proportional to both the sine and cosine components of the signal are available as separate outputs.

- Tracking notch filter.

- Sweep filter.

- Wave analyzer.

- Spectrum analyzer.

- Distortion analyzer. (The rejected frequencies are available as a separate output.)

In addition to its wide variety of general applications, the Lab-All has been used in many special situations, according to Tony Heibel, UFAD's vice president:

- "Nondestructive testing" of humans to determine the degree of hardening of the arteries. A broadband noise signal was applied to a portion of a human limb in an experiment conducted at Michigan State University. After the signal had passed through the subject's body, Lab-All examined its frequency spectrum. The researchers discovered, interestingly enough, that the blood flowing through arteries coated with fatty deposits affected the transmitted signal so that its frequency spectrum differed measurably from a similar signal passing through subjects with lower arterial deposits.

Lab-All was used because its precise narrow-band capabilities could pick out the frequency differences.

- Balancing rotating machinery, such as crankshafts. Lab-All can accurately determine the amount of unbalance by measuring frequency variations.

- Tracking signals buried in noise or measuring signal phase with the aid of a scope. Lab-All is such a precise tracker, Heibel points out, that it can track a signal as low (relatively) as the 101st harmonic of a square wave.

- Other applications include measurements of noise and doppler frequency shifts and speaker and microphone testing.

- A scope CRT overlay, calibrated in both amplitude and phase is provided. By varying Lab-All's frequency, a Nyquist plot is generated on the scope screen. ■■

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CIRCLE NUMBER 295

MODEL SE6150



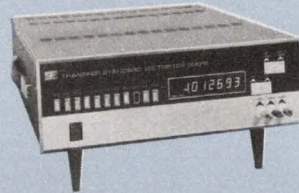
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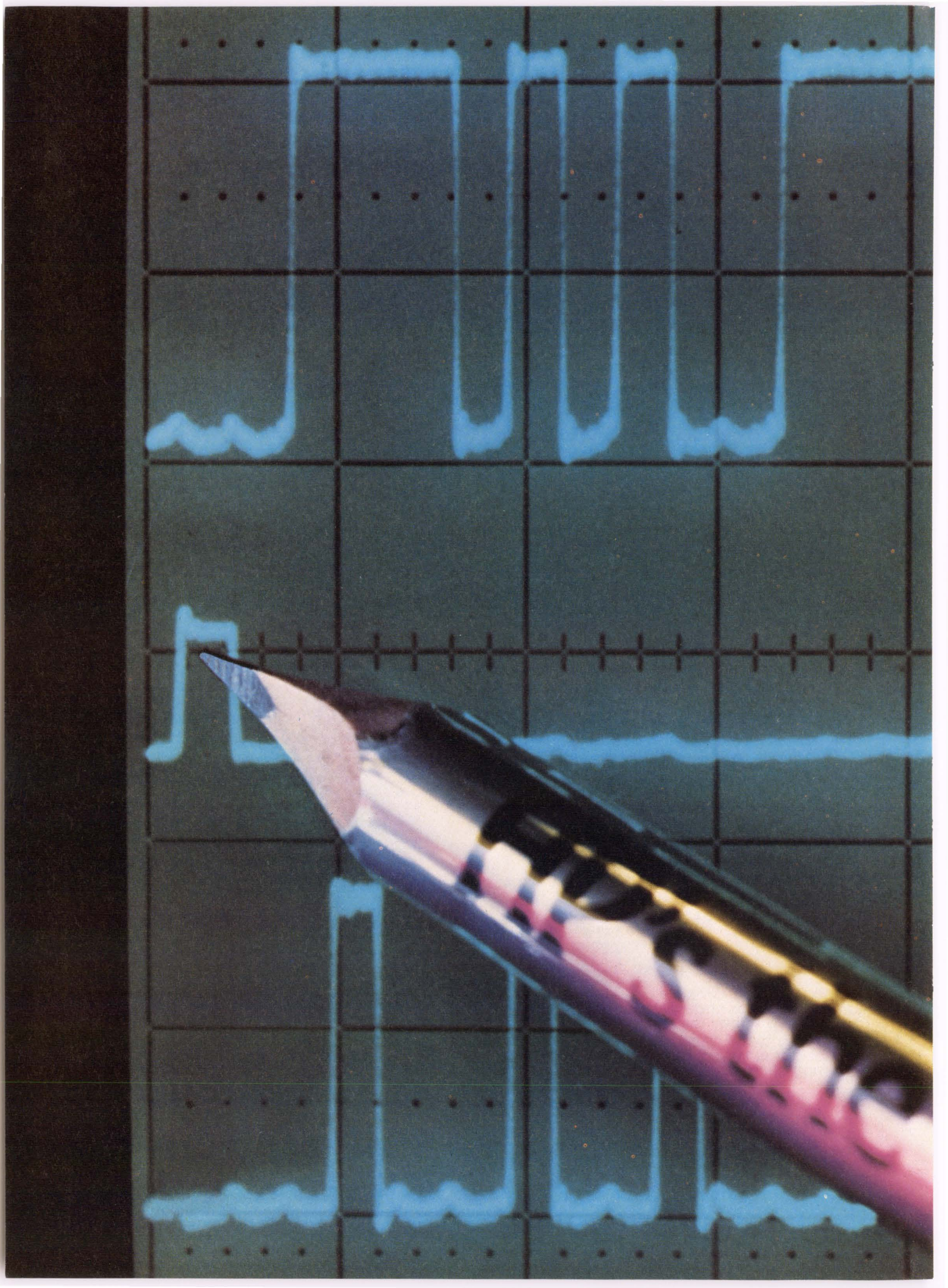
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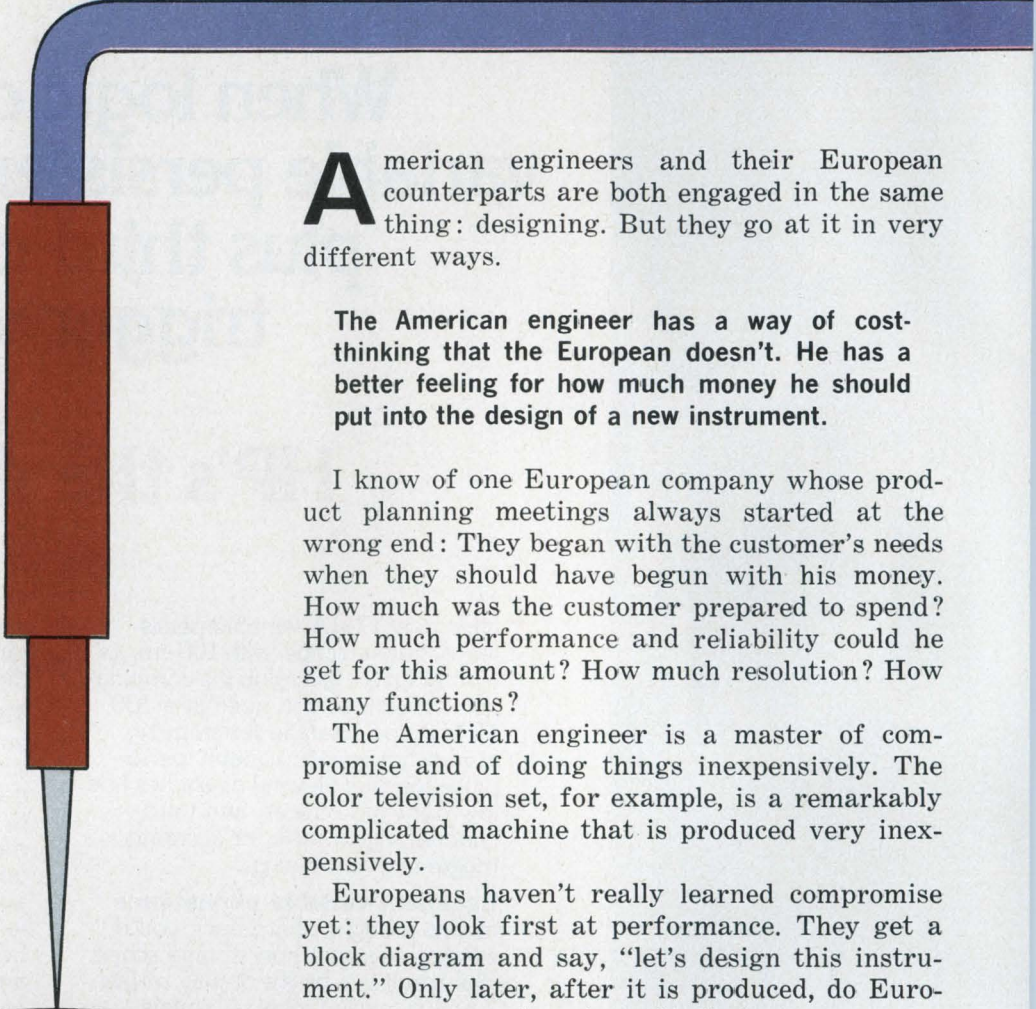
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086 11

CIRCLE NUMBER 49



American engineers and their European counterparts are both engaged in the same thing: designing. But they go at it in very different ways.

The American engineer has a way of cost-thinking that the European doesn't. He has a better feeling for how much money he should put into the design of a new instrument.

I know of one European company whose product planning meetings always started at the wrong end: They began with the customer's needs when they should have begun with his money. How much was the customer prepared to spend? How much performance and reliability could he get for this amount? How much resolution? How many functions?

The American engineer is a master of compromise and of doing things inexpensively. The color television set, for example, is a remarkably complicated machine that is produced very inexpensively.

Europeans haven't really learned compromise yet: they look first at performance. They get a block diagram and say, "let's design this instrument." Only later, after it is produced, do Europeans try to see how to make it cheaper.

The American engineer is much more adjusted to reality than the European. The European engineer wants to design the best in the world. The American engineer wants to design the most marketable.

European pride in design is overvalued and runs up the cost. Not only does this pride cause more performance to be designed into an instrument than the customer needs or wants to pay for, but it even stifles teamwork.

I recall once when two groups of engineers were designing synthesizers—each group was building "the best synthesizer in the world." Eventually, they became so competitive they wouldn't speak to each other. No one wanted to give any tips away to the opposing team. So

**Ulrich Rohde
of Rohde & Schwarz
Speaks on
European and American
Engineers**

John F. Mason
Associate Editor



Ulrich L. Rohde, whose father is co-founder of Rohde & Schwarz, Munich, not only markets company products in

the United States, but also designs instrumentation to be built in the United States.

they ended up with two excellent synthesizers—both so expensive no one would ever be able to afford them. So they had to be redesigned.

In America, the two groups would have talked with each other—possibly at lunch or while playing baseball—and they would have turned out one synthesizer in half the time and at a much lower cost.

European engineers—and the Japanese, apparently—are brought up to think that to earn money, they have to spend years and years designing something that's never been equalled before. But by the time it is finished, the product is no longer needed or new. European engineers should settle on some in-between point of view that's less theoretical and more practical.

Another reason Europeans design instruments with high performance specs is that most European governments require them.

This "excellence" works to the Europeans' disadvantage when they try to sell in America.

Americans say, "You have a fantastic machine, but it does too much; we don't want to pay for what we're not going to use." For example, Rohde & Schwarz has an excellent signal generator used for blocking tests as required in Germany, but such stringent tests and specifications are not required here. Hewlett-Packard has a similar machine that does only what the FCC now requires and costs less than Rohde & Schwarz's. So how do we convince an American to pay more for something he doesn't need?

European manufacturers will probably adopt American practicality in the next five years or so, anyway, because of the increasing availability of information. Not only are the American journals like *ELECTRONIC DESIGN* well read in Europe, because so many European engineers learn English in school, but now there's more personal contact with Americans. With the devaluation of the dollar, Europeans can now afford to travel to the United States to attend symposia and trade fairs,

and visit U.S. government agencies and industries. The dollar was devalued in 1968. So, actually Europeans have only had eight years of this personal exposure to American ideas.

One thing I don't understand is how American engineers can buy an instrument that not only barely does the job, but becomes obsolete in a couple of years.

Europeans like to have instruments that go far beyond their needs. But I suppose the American engineer can't be blamed completely; it's the management point of view that prevails.

The difference between the European and the American engineer begins in school. The American's education is more practical, the European's more theoretical.

I'm sure the German engineer, fresh out of school, typically knows more mathematics than the American. He goes more deeply into things. I'd also bet that the European engineer in general knows much more, mathematically, about the circuit he designs, and why he did it that way, than the American.

I have talked with people who admire me for some particular detail I happen to know. But, actually, the detail has very little meaning; I just learned it in school because I had to. Anyone can memorize a lot of formulas and equations—and later forget them or not even need them.

The Japanese have a similar in-depth background. Look at any copy of *Proceedings of the IEEE* and you'll find that most of those articles that contain those almost unreadable mathematical descriptions are authored by Japanese.

After the first two years in a German engineering school, every student must take on a special project—usually a mathematical problem—that he must finish successfully in order to get his diploma. Here in America, the special project would be to build a product, not solve a mathematical problem. The result is that the American is much better prepared for his job than the European; indeed, he's about two years ahead of a German engineer. If a German engineer is hired right out of school, it usually takes about a year before he can be used.

Another way the American engineer and the European differ is in their motivation. The American wants excitement and glamour. He likes to move from one job to the other. And he wants to work where he can play golf or swim or whatever it is he likes.

The American is more extroverted than the German. He dresses better, and—this is a metaphor for his whole point of view—his house and

car are more flamboyant. He's more caught up in status than the German.

The European in general is more interested in job security, fringe benefits and retirement plans. He also wants to excel at his work and be recognized for his engineering skills and achievements.

American engineers differ *radically* from their European counterparts in their willingness to exchange information.

Americans like to talk about what they're doing, while in Europe everything is a big secret.

I have seen things at Hewlett-Packard, for example, that I would never see at a German company as a visitor.

Maybe Americans are more open because of pride—they like to show people what they've



"I'm here to learn how to sell European products in America, what changes in design and philosophy are needed to be successful here."

achieved. More likely, however, Americans realize—whereas Europeans don't—that most proprietary secrets don't mean very much. If Rohde & Schwarz, for example, learned all of American Company X's techniques for making better oscilloscopes, Company X would still make better oscilloscopes. It would probably have its own IC department, make its own CRTs, and would have evolved its own manufacturing procedures. However, I'm sure that Company X wouldn't find it so easy to produce military communications to compete with Rohde & Schwarz in Europe.

Communication is important because people are like wolves. They occasionally like to be by themselves, but they do best when they're together. If someone is isolated, he's either sick or in

trouble. Once when I was a development manager, I instituted weekly meetings where engineers could tell their colleagues what they were doing.

Are Americans good salesmen?

I used to meet American salesmen who had come to Germany to sell semiconductors or instruments. And I admired them tremendously. They had the courage to come to a foreign country where they couldn't speak the language. They had to rely on finding enough German engineers who spoke English to be able to function.

If these men didn't make a sale, however, it was usually because their company didn't back them up. The company couldn't assure its salesman that the component he was trying to sell would still be in production by the time the European customer needed it in large quantities. It has also happened that by the time the European company has finished a design, the desired component was no longer being produced, and we had to start over again.

American salesmen are even good in America, considering the red tape everyone must go through to sell to an American firm.

In Germany, a department head often needs about five internal signatures to buy instrumentation for his company. Here in the United States, I've seen companies that require 10 or 12. Any salesman who can get through all this red tape has to be admired.

European engineers also differ from Americans in their approach to writing specs; the Europeans are more conservative than aggressive. European engineers promise the very minimum a product can achieve so the customer who gets the one product out of a hundred that falls to that level won't be disappointed.

Americans, on the other hand, pride themselves on their "specsmanship." A clever sales force can put an instrument's best spec forward, so to speak. Or specs can be written in a way that's hard to interpret for all cases. Europeans haven't done this yet.

How do Europeans sell to the American market? That's what I'm here to find out.

Back in 1967, before the dollar was devalued, American instruments were expensive in Europe and European products were cheap in America. Rohde & Schwarz sold easily in America, but Europeans found it difficult to buy American products. I remember the HP spectrum analyzer—it was practically the only one being made, and it was unbelievably expensive.

Then the dollar went down, and American products were in great demand in Europe. They hadn't suddenly become better, just cheaper.

European-made products are more expensive to

Who is Ulrich Rohde?

Ulrich L. Rohde is winding up his second year as president of Rohde & Schwarz Sales Co. (USA), which has offices in Fairfield, NJ, and a territory that covers the entire United States including Puerto Rico.

Besides marketing products manufactured by Rohde & Schwarz, Munich (Rohde's father, Dr. Lothar A. Rohde, is one of the company's founders), Rohde himself is also designing products for manufacture here in the United States.

Born in 1940, Rohde studied communications engineering at the technical universities of Munich and Darmstadt, and after working for other companies became head of the Research and Development Div. for Military Communications Equipment of AEG-Telefunken in Ulm, West Germany.

A Senior Member of the IEEE, Rohde has published more than 40 articles in the field of communication engineering. While still in school, he wrote a book on the behavior of transistors at very high and ultra-high frequencies.

"My father had always said that if you wanted to become an expert in a subject, write about it. I did and it was a great success; it sold 20,000 copies, which is a lot for a book published in German. But it didn't win me any friends at school. People thought I was presumptuous, I suppose, writing a technical book while still an undergraduate.

"How did I get from Munich to Fairfield, NJ? I'm here to learn how to sell European products in America, what changes in design and in philosophy you need to be successful here. Because once you are successful in America, you're successful worldwide."

produce than American-made products because, first of all, European labor is expensive—there are so many fringe benefits that Americans don't have. For one thing, it's almost impossible to fire a German engineer. Germany is probably the only country I know that has a strong engineer's union.

Also, some European products contain American-made high-technology components, which means the factory in Europe has had to wait to receive the shipment from the United States; it's no doubt had to hassle with customs, and it has had to deal with, and pay, distributors.

The solution is to produce a reliable product that's in demand and that's economically competitive, which rules out digital voltmeters and counters right away. I'd like to know how many people got burned making these devices. The

number of them being offered is unbelievable.

Rohde & Schwarz's latest really successful instrument is not an inexpensive, bread-and-butter product; it is the SMPU, a fully automatic, radio-telephone test set assembly.

Rohde & Schwarz is selling the SMPU for less than HP's comparable Bigfoot. Our SMPU is about \$45,000. We've sold to RCA and General Electric, which use them in the production of their communication equipment.

How did we do it? It was very simple. We used a lot of things we already had available, and we put them all into one box, using only as much of a device as we needed and no more.

We took the most significant assemblies of a digital voltmeter, an audio-distortion analyzer, a power meter—only those portions that we needed—and automatically, the SMPU became cheaper. Basically, we ended up with a computer-controlled magazine full of PC boards and one μ P. The main cost was for the software.

Learning to produce more for less is the only way to compete. And we're learning. We have several more instruments in the works that we also feel will be successful.

Why did I go with the competition? I didn't go with my father's company for several good reasons.

I wanted to be on my own. I didn't want people to think that I was qualified by heritage alone. I knew I was a good design engineer, and I wanted to prove it. At Rohde & Schwarz, I knew I'd be handicapped in my day-to-day work by being the president's son. If you were my boss, for example, you'd feel a little funny knowing that my father was president. Also, I knew if you and I should reach a roadblock on a technical issue, and we went to my father, he'd side with you.

I thought it was better to gain experience by working in a company other than Rohde & Schwarz, Munich, which my father and Dr. Schwarz started in 1933.

My first contact with an outside company, however, would never have turned out well if I hadn't been able to deliver the goods—if I hadn't been a good designer at 19, when I was still in school.

One day, one of Telefunken's top engineers, Prof. Werner Nestel, came to our house for lunch and, noting my studied silence, asked me afterwards what was wrong. So I told him. After school, I had built an amateur radio receiver in the cellar of the house, and it had worked like a charm. But when my father came down to see it, he unfortunately grasped an uninsulated wire.

To teach me a lesson for my negligence, he locked the cellar door when we left, and I couldn't get back in.

Don't worry, the professor told me. He would do something. What? Get the key? No, he couldn't do that. But a few days later, I received a handful of transistors—the very first vhf/uhf transistors ever built in Germany. And with them I built an FM radio, probably one of the first in Germany. I sent it, and my thanks, to the professor, who in turn sent me his thanks and a check for the design. Telefunken then produced the radio.

After finishing my education and working for several small companies I was hired by Prof. Nestel at Telefunken as a design engineer and division manager.

Here in New Jersey, I'm a salesman. But I spend quite a few week-ends here in the office building synthesizers. One was for a microwave project. I have already sold the first piece.

Now I couldn't have done this at Rohde & Schwarz in Munich or at Telefunken. They're both too big. I'd have ended up with difficulties. And that's normal. There must be rules. Everyone can't go around doing whatever he likes. But I'm the boss here in this sales office and I can do what I like—on week-ends.

Do you know what I always wanted to do? I had good experience in Europe with big companies and I would really have liked to see how a big American company works from the inside. I'd like to have worked as vice-president of engineering for something like Hughes Aircraft, or another big company, where I could work with radio communications designers.

But now I enjoy promoting Rohde & Schwarz and other companies in the United States and have even organized some manufacturing here.

America spoils me. If I had the choice of going back or staying here, I think I'd be in trouble. I like it here, my wife does. We have a 15-month old daughter who has an American passport. I have a house here I couldn't have near Munich—there's not that much space near Munich. No one there has a one-acre lot.

I am able to keep in touch with my friends in Germany. I get up every morning at six and talk to them by my short-wave radio at home. It's their lunch time then. And would you believe that just outside of Fairfield, here in the woods of New Jersey, there's a very good little German restaurant? Good German beer, wurst, sauerbraten—whatever you like. Let's go! And when we come back, I'll give you some Leberkäse to take home; there's a good German butcher not far from here. ■■



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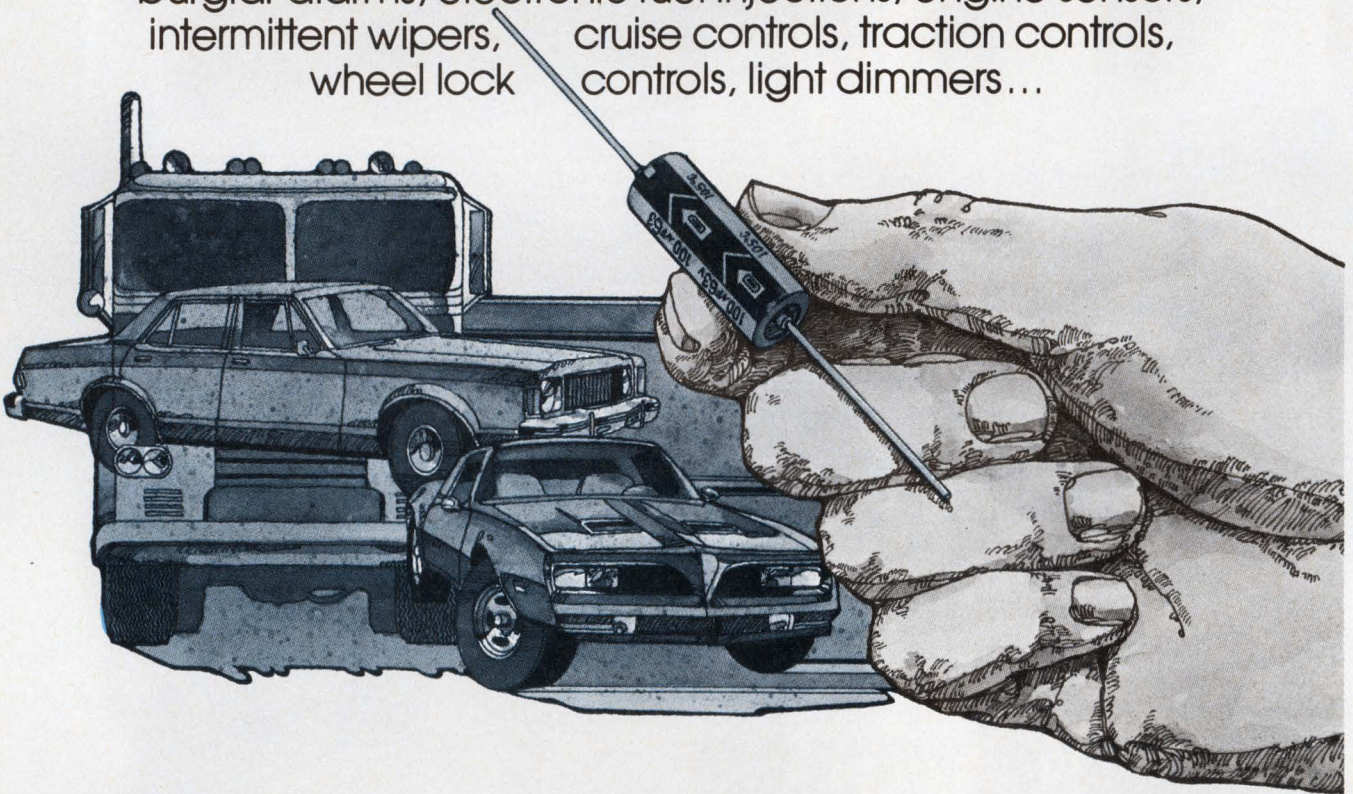
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CIRCLE NUMBER 51

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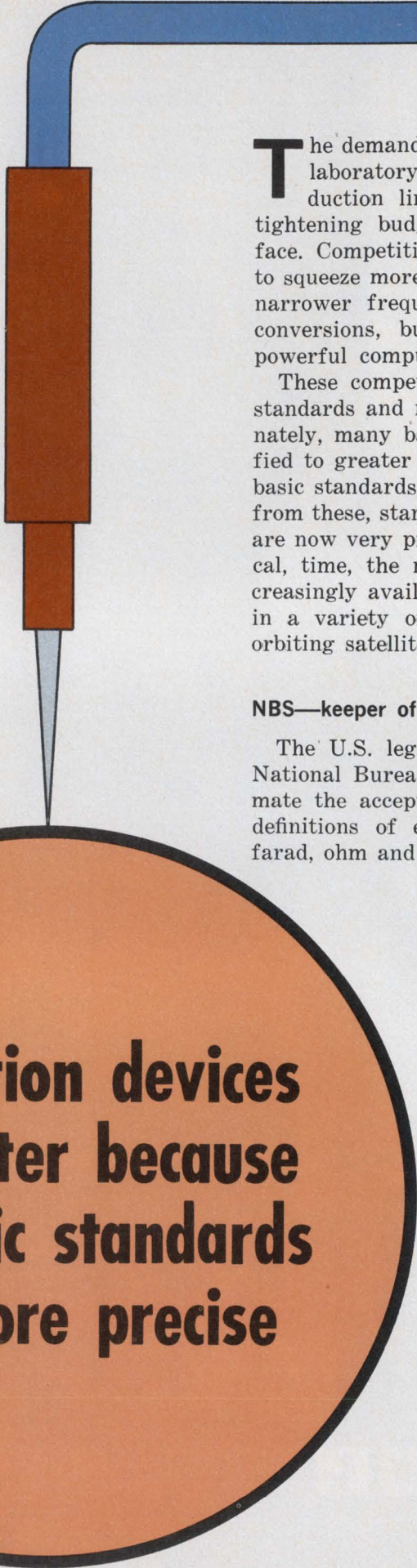
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The demand for ever greater precision in the laboratory, on the bench and on the production line continues in the face of the tightening budgets that design engineers must face. Competition is forcing engineers not only to squeeze more information capability onto ever narrower frequency bands and more bits into conversions, but also to interface with more powerful computers.

These competitive advances require improved standards and measuring equipment, and, fortunately, many basic standards can now be specified to greater accuracies than ever before. The basic standards for voltage and capacitance, and from these, standards for resistance and current, are now very precise. Frequency and its reciprocal, time, the most precise parameters, are increasingly available in standalone hardware and in a variety of existing broadcast or planned orbiting satellite distribution systems.

NBS—keeper of the keys

The U.S. legal standards, maintained by the National Bureau of Standards (NBS), approximate the accepted international (MKS system) definitions of electrical measuring units. Volt, farad, ohm and ampere standards are set by the Electricity Division of NBS in Gaithersburg, MD; the nation's master clock is the responsibility of the Time and Frequency Division in Boulder, CO. The standards are stringent: for electricity, NBS measures accuracy down to parts per million; for the master clock, accuracy is a matter of picoseconds.

NBS makes every effort to disseminate these extremely accurate values to industry; conversely, secondary (industrial) standards sent to NBS by its industrial customers are calibrated against its primary standards. Measurement Assurance Programs (MAPs) ensure that industrial total measurement processes are reliable. Time and frequency are distributed via VLF radio transmission and satellites.

**Calibration devices
are better because
the basic standards
are more precise**

Sid Adlerstein
Associate Editor



Repeatable color performance from monitors is obtained with Tektronix' J16 photometer. Any number of monitors corrected to a color temperature of 6500 K can be matched for color even at separate locations.

But how accurate are the values of the basic standards themselves? The entire measurement process depends on the precision of the NBS standard. Fortunately, some of the basic standards have recently been made extremely precise.

The volt is now more precise

Increased precision for the standard volt has been achieved by using the ac Josephson effect to calibrate the average value of the voltage standard itself, a bank of Weston cells. The ac Josephson junction is the most accurate voltage source ever, and its voltage, a series of steps, is known to a few parts in 10^8 .

The Josephson junction is a frequency-to-voltage converter in which, the tunnel junction of two superconductors—separated by a thin insulator, properly biased with dc current and irradiated with microwaves—produces a series of voltage steps proportional to the microwave frequency. Its proportionality constant depends on the values of the electron's charge and Planck's constant, and is known to better than one part in 10^8 .

As a standard, the Josephson reference has three advantages:



Calibration skills are maintained in the cassette library of Julie Research's Locost test system. Programs question the operator who responds via the keyboard.

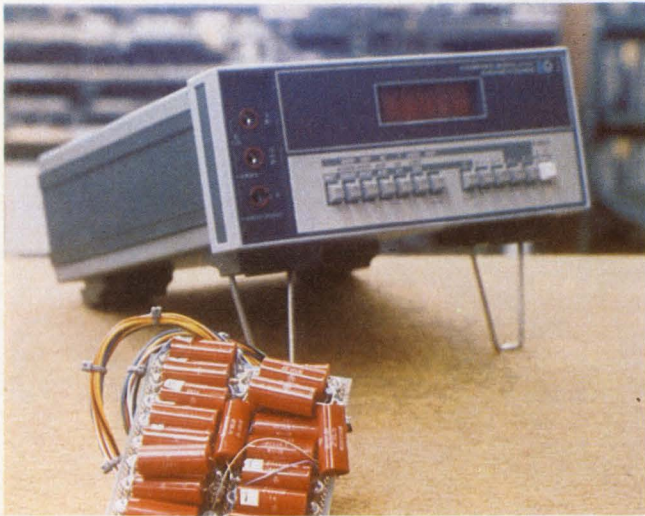
- The junction itself is readily reproduced.
- The thin films are permanent structures that require no mechanical adjustments before calibration.
- The junction requires no cleaning or reconditioning.

There are drawbacks, however. The superconducting junction requires nearly absolute zero temperature; output voltage is only 5 mV per junction; and the process is time-consuming. NBS uses two junctions in series for 10-mV output, but the circuitry needed to scale the output up to the 1-V level at cryogenic temperatures is a source of error. Because calibration with the Josephson effect takes so long, even the NBS doesn't calibrate its standard cell bank more than once a month.

Capacitance is the most precise electrical unit

Currently, the most attainable electrical standard is the unit of capacitance, the farad. With the Thompson-Lampard capacitor as the basis for calibration, the U.S. legal farad standard is calibrated to 0.02 parts per million of the international definition.

The Thompson-Lampard is a variable-cross-type capacitor, with a grounded conductor rod passing through its center. Moving the rod between its extremes results in a $1/2$ -pF change in capacitance. This value is precisely calculable to less uncertainty than two parts in 10^8 , in terms of only one variable—the distance the rod is



moved. This distance is measured on a stabilized laser interferometer built into the device.

The U.S. legal farad standard consists of a bank of five fused-silica dielectric capacitors, each with a value of 10 pF.

Resistance is calibrated to the capacitance standard. The equipment used to perform this calibration is so accurate that the U.S. legal ohm is less than 0.06 parts per million from the internationally defined ohm—despite the numerous calibration steps involved.

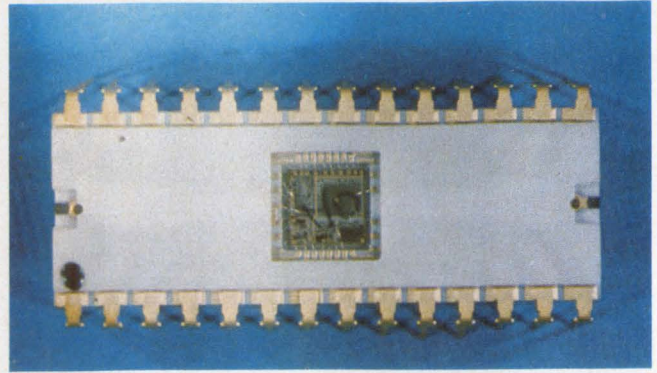
The precision to which the ohm and volt standards are known have limited the fluctuation in yet another standard—the ampere. An absolute determination of the ampere is carried out at NBS only once every ten years or so because the procedure is so cumbersome and inexact. A balance measures the force produced by current flowing in two conductors. But this method has as much as 15 parts-per-million error. The volt and ohm standards can be used to produce the ampere to an accuracy of 0.07 parts per million.

Frequency is the most precise standard

The most accurate standard available, frequency, is derived from the hydrogen maser. The hydrogen maser is capable of stabilities of 1 part in 10^{14} for 100-s averaging and 2 parts in 10^{15} for 1000-s averaging.

While they are ultra-precise, hydrogen masers are also expensive, large, heavy and sensitive to shock and vibration. But precision hydrogen masers have been made that have a diameter of only 19 in., a height of 30 in. and a weight of 80 lb. These have been applied in airborne-relativity experiments.

Since, for most applications, the maser's ulti-



Tantalum nitride fine-line resistors (right) provide long-term accuracy and temperature stability for HP's 3465A five-function bench or field DMM (left). Fine-line resistors and MOS ICs in its a/d converter give the unit a one-microvolt sensitivity for dc voltage.

rate precision is superfluous anyway, the less precise atomic-frequency standards, cesium and rubidium, are widely used in industry. Also, quartz-crystal standards are now available that offer surprising stability and spectral purity. The frequency stability is usually of the order 10^{11} for rubidium standards and either 10^{12} or 10^{13} for cesium standards. On the other hand, quartz-crystal oscillations boast stabilities of 10^{10} and even better.

In addition to atomic and crystal standards, precise frequency is available through WWVB, a VLF standard broadcast station run by NBS.

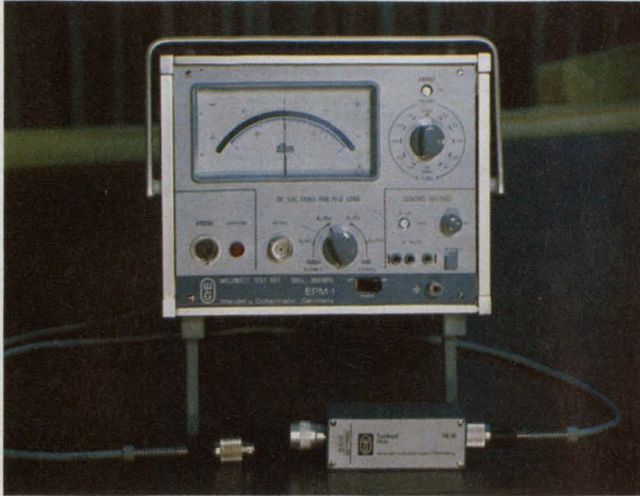
An alternative to WWVB for obtaining precise frequency is the use of a TV color sync-burst comparison. All four major TV networks (ABC, NBC, CBS and PBS) have extremely stable carrier frequencies. The frequency in their color bursts (3.58 MHz) is synchronized with atomic clocks.

The TV-color-sync-burst technique is accurate to 1 part in 10^{11} . TV network time is offset from the rest of the world's agreed time (UTC time) by 3000 parts in 10^{11} . Normal TV-network-broadcast signals are the NBS signal minus 3000 parts in 10^{11} .

Two NBS stationary Geophysical Orbiting Earth Satellites (GOES) now broadcast to the earth and cover the North American continent.

Industrial low-frequency standards

Today, low-frequency electrical instrumentation offers the variety of a flea market. Streamlined and softly colored five-and-six-digit meters stand alongside the walnut and black of the older, more staid analog devices, while stable components, using new materials and processes re-



Accurate rms measurements at zero dBm and zero dB levels are provided by W & G's EPM-1 milliwatt test set. Probe circuitry prevents thermocouple burn-out.



Removable reference assembly simplifies calibration of dc functions and ohms in Hewlett-Packard's 3455A, a guarded integrating 5-1/2 or 6-1/2-digit multimeter.

place prosaic wire wound resistors. In the precision-instrument bazaar, a new generation of automatic equipment vies with the older, manual hardware. Nearly ultimate accuracy and lower, but cheaper, precision come in almost every instrument.

A reference that can maintain a unit of voltage with a 1-ppm precision at the one-volt level is now available from Superconducting Technology, Mountain View, CA. It consists of a Josephson junction with low-temperature Dewar, microwave and dc-bias junction sources, and a potentiometer.

In addition to its line of impedance standards and precision bridges, GenRad of Concord, MA, has introduced an inexpensive capacitance standard with 0.25% accuracy over seven range selections, from 1 μ F to 1 F. The GR 1417 costs \$775 and can be used as a standard for dissipation factor (D).

A fine-line process at Hewlett-Packard, Palo Alto, laser trims resistors on a sapphire substrate to ratios of 0.01%. The fine-line process was first used in HP's 3465 multimeter. Now, every DVM on the HP drawing boards uses the stable fine-line processed resistors whose values range from 5 Ω to 10 M Ω .

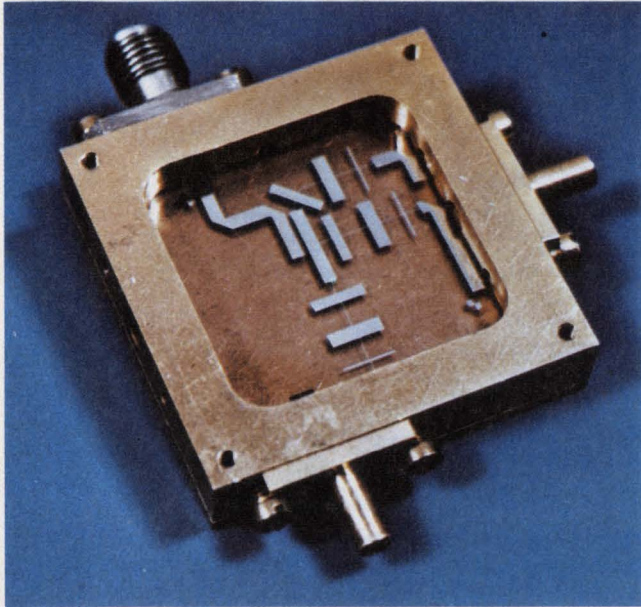
Automated standards are the trend at Ballantine Laboratories, Boonton, NJ. Ballantine's Model 1500A auto-balance ac-to-dc transfer standard, for measuring true rms-ac voltage, brings the precision of the standards lab to the calibration and manufacturing areas. Featuring 0.005% precision and calibration from 2 Hz to 30 MHz, this remotely programmable instrument reportedly can be used even beyond 100 MHz.



Seven ranges of capacitance from 1 μ F to 1 F can be selected with the GR 1417. The four-terminal standard also acts as a standard for dissipation factor.

The feeling at Electro Scientific Instruments, Portland OR, about measuring dc resistance in the ppm range is that the measuring instrument's long term stability is degraded when its size is reduced and its speed increased. Consequently, the calibration cycle must be shortened.

Architected systems for test and calibration are a major involvement at Julie Research Labs in New York. Its Locost line of automated precision test and calibration systems are controlled by master programs on cassettes. The software asks the operator a series of questions to which he replies via keyboard entries.



The world's most accurate voltage standard, the Josephson junction (left) is mounted in a microstrip enclosure for microwave irradiation while held at -77 K or less. Capacitance is a distance function in the Thompson-Lampard variable cross capacitor (right).

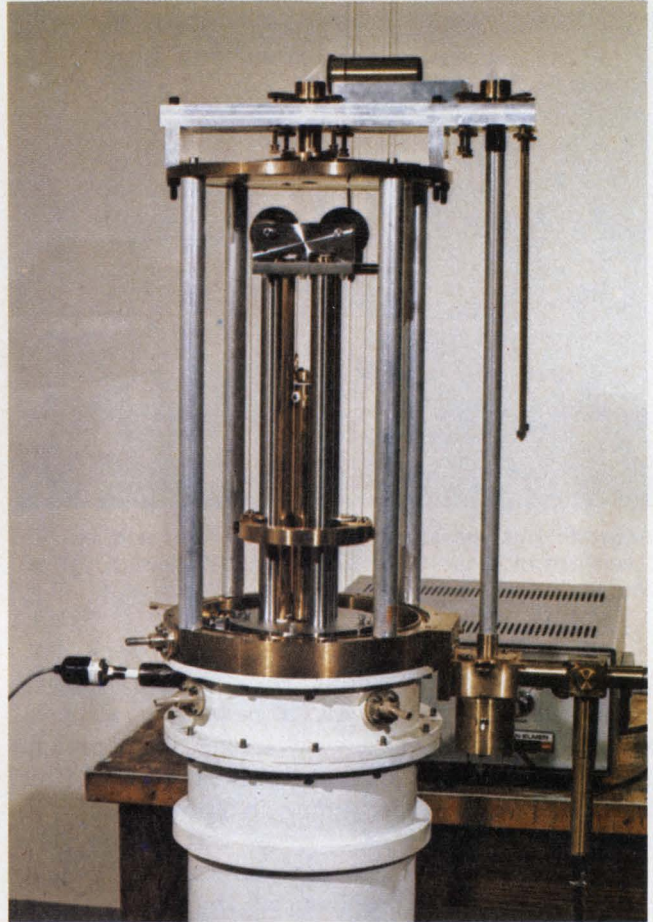
Time bases for counters and local oscillators (LOs) for communication systems require precise frequency. Frequency counter time bases require frequency stability, while modulated-carrier communications devices are concerned primarily with having a phase noise (spectral purity) of low spectral density, especially near the carrier. This is especially true of digital systems where channels are spaced only 10 to 15 kHz apart; obviously, phase noise near the carrier is a crucial consideration when information is phase-modulated onto a carrier. And in the upcoming area of gigahertz timing, both phase noise and stability are important.

Frequency hardware is available

Fortunately, industrial frequency sources abound. New component quartz-crystal oscillators from Austron of Austin, TX claim a phase noise of -110 dB at 1-Hz deviation -155 dB at 10 Hz and -180 dB at and beyond 1 kHz.

For Austron's 2010B Disciplined Frequency Standard, stability of a few parts in 10^{13} per day is maintained for several months by the instrument's third-order servo loop. The unit's quartz oscillator is corrected from an input, say a cesium-beam standard or a Loran-C signal. The device then "learns" its frequency offset and aging rate and constantly corrects itself.

Hewlett-Packard's quartz oscillators emphasize long-term stability rather than spectral purity.

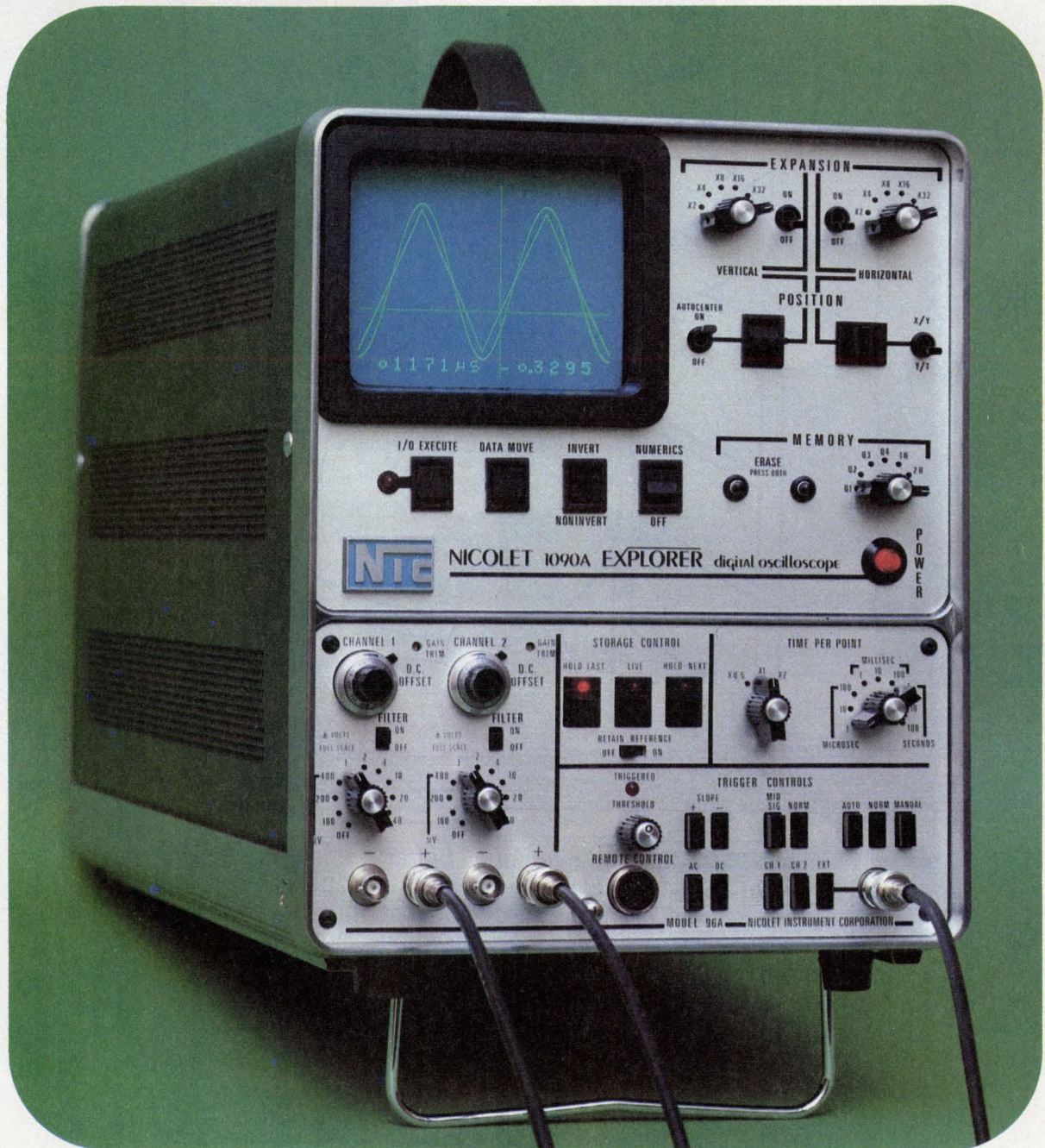


HP's 10544A instrument is intended for use in communications systems as a counter's time base rather than a LO. The unit has a long term stability of 5 parts in 10^{10} per day. However, the 10544A has pretty respectable phase noise characteristics— -83 dB at 1 Hz to -145 dB at 1 kHz.

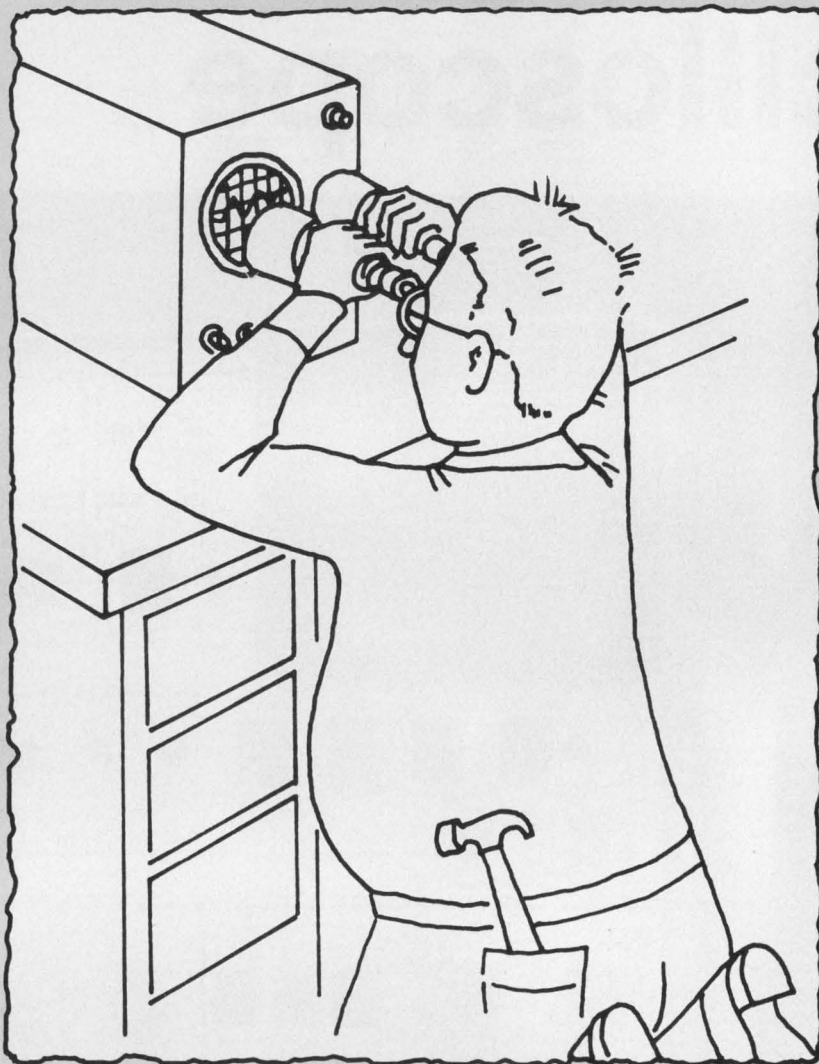
The -145 dB noise floor is partly the fault of the unit's switching regulator. At the beginning of 1977, HP's 10544B quartz oscillator will be available. This new instrument will have its internal dc generated by a linear regulator, and the noise floor for the unit will be lowered to -150 dB at and beyond 1 kHz from the carrier.

Arbiter Systems of Goleta CA, markets a Model 1011B frequency comparator for under \$3000, which compares a unit under test to the standard TV broadcast color burst. The comparator requires eight cycles of the 3.58-MHz color burst to phase-lock. No warm-ups or adjustments are needed, and like any phase locked system, the uncertainty (error) is reduced by increasing the sampling time (averaging). However, averaging times with this system are in seconds rather than days, as with VLF systems. For example: a frequency may be tested to an accuracy ($\pm 1/2$ LSB) of 10^8 in 1 s or up to 10^{11} in 1000 s. ■■

a new generation oscilloscope



HAVE YOU EVER NEEDED STORAGE 'SCOPE RESOLUTION THAT JUST WASN'T THERE?



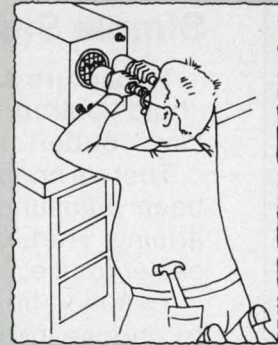
In a storage 'scope you need better, not lower resolution, because what you capture will be all you'll ever see if the signal occurs just once.

Nicolet's general purpose storage oscilloscope provides 20 times better resolution than the next best storage 'scope. And you don't need binoculars or a microscope. You can electronically zoom in on any detail of interest. Quickly and easily, whether the signal is stored or live.

Hide a Waveform???

Some storage oscilloscopes can hold a trace, without fading, for so long a time that the instrument specifications merely say "holds until erased".

This is true of Nicolet's storage oscilloscope, **EXPLORER**. And a fine additional feature is that you can cause the stored information to be hidden away, out of sight, until you want to see it again. This means that you can use the **EXPLORER** for normal operations in the meantime. It isn't tied up by the holding process. You can tuck away several waveforms, out of sight. And can recall any of these, or all of them at once superimposed, for examination and comparisons. A minute, an hour, days, or weeks later.



Write-through Storage!

If you want to see the effects of small changes while they are occurring in a circuit system, it's great to be able to store the original waveform and continue to see live, ongoing signal waveforms superimposed on the original waveform.

Especially in the case of the **EXPLORER**, which allows up to 64X expansion of corresponding regions of both the stored and live waveforms. Changes of as little as 0.02% can be clearly seen and there's no limit to the length of time this can be continued. The stored signal doesn't degrade in the least.

What's Automatic Persistence?

Variable persistence storage oscilloscopes are useful for observing signals that don't occur often. The persistence time can be adjusted so that the trace fades by the time the next signal is expected.

Automatic persistence is better. The trace remains, without fading, right up to the time the next signal occurs. It doesn't matter how long or short the interval between signals, and no adjustments are needed. Nicolet's **EXPLORER** oscilloscope has automatic persistence.

NI COLE
INSTRUMENT
CORPORATION

Simple Signal Capture!

To capture a signal with the **EXPLORER** just press a "hold" button. To return to live action, press the "live" button.

There's no mode switching, no enhancement, no beam adjustment, no erase step and no sweep arming. The **EXPLORER** is much quicker and much easier to use.

To speed up reaction time, use a remote sensor to choose the interesting signal. It can decide before, during or after. That's important because sometimes neither you nor the sensor know that the signal should be held until the signal has started or ended.



Store a Week-Long Signal!

Storage oscilloscopes are handy for observing very slow signals. Sweep times as long as a minute, in a non-storage scope, result in a display that's not much more than a slowly moving dot. But a storage scope generates a clear trace representing the signal waveform, which is much better.

For longer sweep times you'd better borrow a pen recorder. Or use Nicolet's storage oscilloscope which has sweep times that range from microseconds to days.

Even if very slow signals are not your immediate interest, it's handy (fun, in fact) to record overnight or over-weekend changes in such variables as temperature or line voltage. With high accuracy and better resolution than a high precision pen recorder.

These are half a dozen significant new capabilities of the **EXPLORER**. There are half a dozen more, and a few more of less importance.

Hundreds of pleased **EXPLORER** users find them easy and natural to operate. In the words of one, "Anyone who has ever actually used an **EXPLORER** in his work will never want to go back (to the older 'scopes) again." Evaluated by one of the nation's largest laboratories, "An excellent oscilloscope — providing significant advantages."

EXPLORER is a low frequency, general purpose oscilloscope. Bandwidth, 1, 2 or 5 MHz depending on plug-in.

The **EXPLORER** is pictured here with the Model 96A plug-in for two-input, 1 MHz applications.

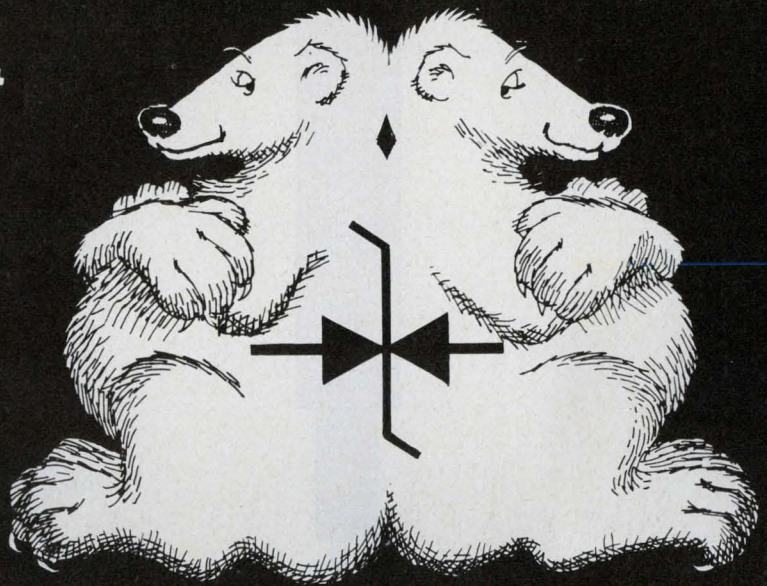
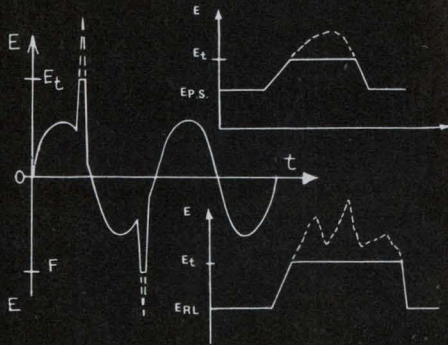
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CIRCLE NUMBER 56

New! Bi-polarity Silicon Transient Suppressors!



LOWEST DYNAMIC IMPEDANCE!

**Can be supplied as JAN, JANTX or JANTXV
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This new series of silicon bi-polarity transient suppressors is unique in that a single device will provide voltage transient protection symmetrically (i.e., provide protection for A.C. signals in addition to D.C.). This new series of devices has peak pulse power ratings of 500 to 1500 watts for 1 millisecond and its response time is effectively instantaneous (less than 1×10^{-12} sec.). Therefore, these versatile devices have many protection applications where large voltage transients can permanently damage voltage-sensitive components. The devices are encased in Semtech's Metoxilite, fused directly to the high temperature metallurgically bonded assembly. For use in commercial, industrial, military and space programs.

500 Watt

Peak Pulse Power

Types: IN6102 through IN6137

Break down Voltage V(BR):

From 6.8 to 200Vdc $\pm 10\%$

Peak Surge Voltage (Vsm): 11.0 to 286.0V

Peak Surge Current (Ism): 45.4 to 1.7A

Temperature Coefficient of V(BR): .05 to .11%/°C

Case Size (Max.): .140" D x .165" L

1500 Watt

Peak Pulse Power

Types: 1N6138 through 1N6173

Breakdown Voltage V(BR):

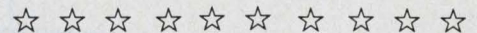
From 6.8 to 200Vdc $\pm 10\%$

Peak Surge Voltage (Vsm): 11.0 to 286.0V

Peak Surge Current (Ism): 136.4 to 5.2A

Temperature Coefficient of V(BR): .05 to .11%/°C

Case Size (Max.): .180" D x .165" L



4-LAYER DIODE IN METOXILITE!

Reduce circuit costs and increase reliability!

Semtech's 4 Layer Diode (PNPN) is a silicon switch that is controlled by the amount of voltage applied. The application of this diode to a circuit often reduces the number of associated components which in turn, leads to cost reduction and increased reliability. Now available in Semtech's proven Metoxilite construction as two terminal, fast-switching devices specifically designed for low voltage applications such as logic circuits, pulse generators, memory and relay drivers, relay replacements, alarm circuits, multivibrators, ring counters, and telephone switching circuits.

Types: 1N5779 thru 93, 1N5158 thru 60

Switching Voltage: 10 to 15V

Switching Speeds: t(on) = 75ns, t(off) = 250ns.

Junction Capacitance: 150pF

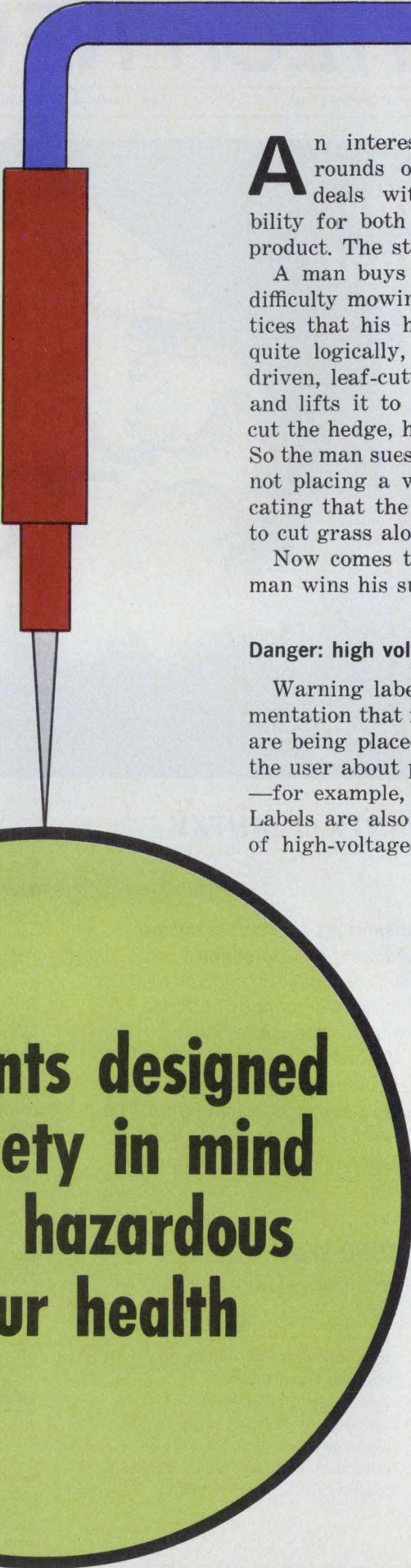
Case Size (Max.): .070" D x .165" L

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An interesting horror story making the rounds of the instrument manufacturers deals with the manufacturer's responsibility for both safe use and safe misuse of his product. The story goes something like this:

A man buys a power lawnmower and has no difficulty mowing his lawn. After a while, he notices that his hedge needs trimming, so feeling, quite logically, that he already owns a power-driven, leaf-cutting tool, he starts up the mower and lifts it to do the hedge. But before he can cut the hedge, he cuts off a couple of his fingers. So the man sues the lawnmower manufacturer for not placing a warning label on the mower indicating that the grass-cutting blade is to be used to cut grass alone and is hazardous to fingers.

Now comes the horror part of the story: The man wins his suit.

Danger: high voltage

Warning labels are a step toward safe instrumentation that most companies are taking. Labels are being placed on high-voltage probes to warn the user about putting his hands in certain areas—for example, too close to the tip of the probe. Labels are also being attached on outside covers of high-voltage instruments, and internal cages that cordon off the specific high-voltage sections.

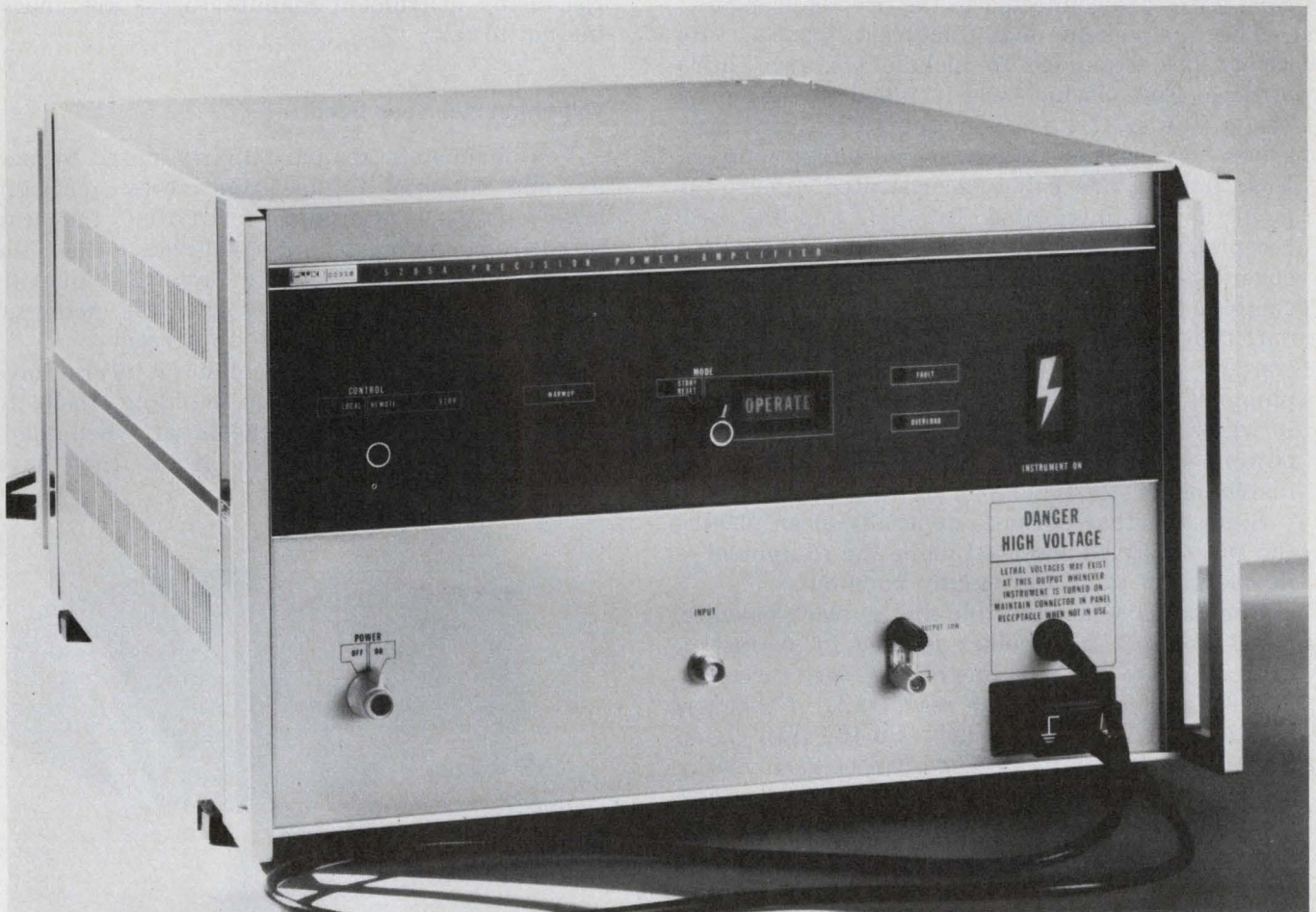
A red lightning-bolt design is becoming standard on front panels of instruments with high-voltage connectors. Some companies are even using the lightning bolt where lethal voltages may appear—for example, on voltmeter-input connectors. Here, the instrument doesn't generate high voltage on its input, but the input terminals become "hot" when high voltages are measured.

Liberal warnings can now be found within the text of specific measurement or calibration procedures outlined in instruction manuals. To make their point, these warnings are often printed or outlined in red and set off from the rest of the text.

Some companies have even

**Instruments designed
with safety in mind
may be hazardous
to your health**

Jim Gold
Western Editor



A lighted warning label that tells the user to be careful of high voltages is a new safety feature that is starting

to appear on instruments such as this precision power amplifier from Fluke.

gone to the extreme of putting lighted warning labels on their equipment. For example, an automated test system developed by John Fluke, Mountlake Terrace, WA, is capable of performing preprogrammed tests on many pieces of equipment. A good number of these tests have potentially lethal voltages crossing between the automatic tester and the tested device. The interface between them is a transition panel with a lightning-bolt label that lights up when the programmed test involves dangerous voltages.

Illuminated warning labels are especially useful when an instrument is meant to be used by someone unfamiliar with high voltage and its effects. But what about those who are supposedly familiar with high voltage—the engineers and technicians who deal with it every working day? Has anyone not been zapped by a “familiar” piece of equipment at one time or another?

Familiar with the moral of the story of the man and his lawnmower, most instrument manufacturers provide safety interlocks on their equip-

ment that are designed to protect the user. Many even go to the extent of incorporating double interlocking switches in situations where lethal high voltage exists.

Double interlocks maintain integrity

Double interlocks are used to guard against the failure of any single interlock switch to maintain the integrity of the protective interlock system.

Clear plexiglas shields are commonly employed with the interlocks over internal portions of the instrument where high voltages may be present. Besides permitting the area to be inspected and the curiosity of the purchasing engineer to be satisfied, the shield prevents access to the high-voltage area.

The exacting requirements of the medical electronics industry have led to the production of clear plastic, ac-line-cord plugs. The visibility of all connections from the insulated line cord to the

metal prongs of the plug helps ensure that the cord wires are connected to the proper prongs.

The instrument manufacturer's concern for safety has expanded to include his own safety devices. Fuses, which are included in equipment design for safety, are now being analyzed themselves by cautious instrument manufacturers. Fuse holders are being incorporated into equipment as an integrated fuse-hold-and-line-cord-receptacle combination that sometimes includes a cover-interlock switch for the instrument. This combined fuse holder and line-cord receptacle is outfitted with its own fuse cover, which prevents contact with the fuses while the equipment is plugged in. The cover slides over the receptacle in which the fuse is located. This ensures that the power is physically disconnected from the instrument.

Since the fuse cover is generally clear plastic, the fuses may be observed while the equipment is in operation to check for any burn-outs.

Similarly, when an old-style, black-bakelite, panel-mounted fuse holder is used in an instrument, the power (hot) line of the fused circuit is generally connected to the rear (tail) of the fuse rather than the front (head). So the fuse clamped into the holder by its head can be removed by unscrewing the front of the fuse holder and avoiding any directly exposed line voltage. The hot line is deep inside a hole in the fuseholder and can only be reached by touching the bottom of this hole with a probe whose diameter is limited to a quarter of an inch.

Proper grounding a must

Properly grounding all exposed metal parts on the outside of an instrument is essential to the safety of operating personnel. Standard practice requires that a solid connection be established between all exposed metal parts and the ground wire in a three-wire ac line cord. In fact, one proposed international specification requires that all exposed metal parts on an instrument measure not more than one ohm to the ground pin on the ac line plug.

Instrument power-line switches are also being scrutinized by safety engineers. Double-pole-single-throw switches that break both the hot and neutral sides of the power line are replacing the old single-pole-single-throw ac line switches to assure complete isolation from the power line when the equipment is switched off. Only the ground connection is left intact. The neutral side of the power line is not at ground potential in many cases, and allowing "power-off" adjustment of switched-off equipment with a portion of the

instrument's circuitry at other than ground is a risk many instrument manufacturers are choosing not to take.

Volt-ohmmeter goes boom

Volt-ohmmeters are particularly suited to misuse and potential failure. Since they generally have multiple ranges and sensitivities, they can be easily connected to large voltages even while set improperly. This usually happens while attempting to measure voltages with the meter set to measure either resistance or current.

Traditionally, ohmmeter manufacturers have protected their products by building them to withstand up to 30 V on the input when inadvertently connected to a live circuit, then have

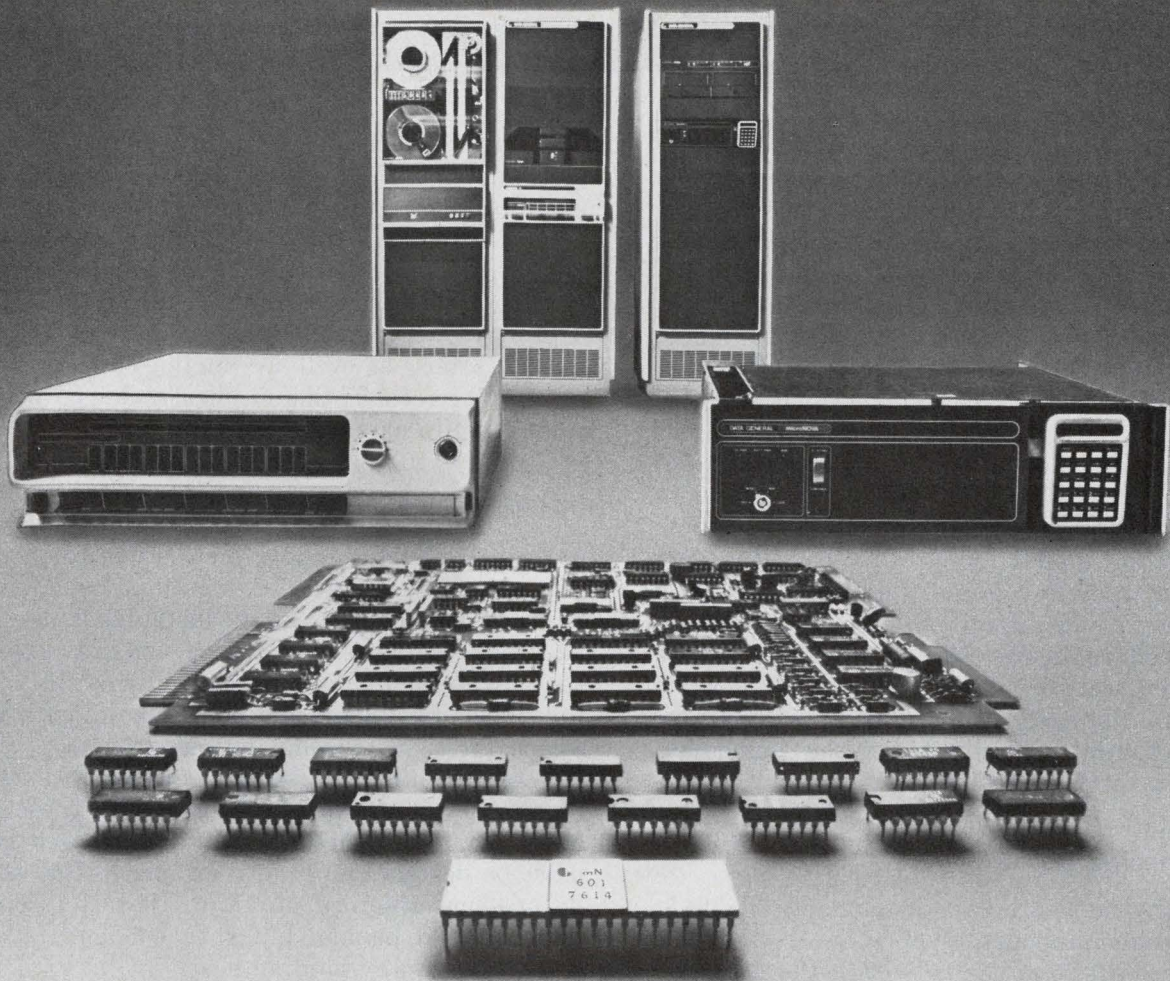


Double insulated cases make battery operated instruments safer. Used in instruments such as this dual trace scope from Philips, the double insulation permits the user to float the instrument so that signals riding on high voltages can be displayed.

relied on a fuse to save the meter above 30 V. Now ohmmeters are equipped with semiconductor protection circuits that enable them to withstand a guaranteed 250-V application, on the theory that the meters should not be harmed when connected to the ac power line accidentally.

However, as illustrated by the case of a man measuring voltages with a volt-ohmmeter held between his knees, meter manufacturers have more to worry about than protecting their own products. The man had the range switch set for current, and as he probed a power line, the volt-ohmmeter exploded. Fortunately, the man was not injured, and the volt-ohmmeter manufacturer learned the same lesson as the lawnmower manufacturer, but at a much cheaper cost.

But attempts to solve safety problems must be considered for their own safety value. The acci-



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dent just described caused one volt-ohmmeter manufacturer to install a 250-V rated protective fuse in one probe of his meter. But this in turn caused other problems. In one instance, a maintenance man was probing a 480-V busbar with his volt-ohmmeter accidentally set on current instead of voltage. The fused probe blew up in the man's hand, although the meter was apparently saved from damage.

Placing a guard chassis within the main cabinet of the instrument is a technique well suited to making measurements float with respect to ground. Typical proposed breakdown specifications for this application are 1000 V rms plus twice the maximum voltage expected between the guard chassis and ground. Since standard operating procedure in the United States is to use input-power transformers with 1.5-kV dielectric breakdown voltages, the guard's chassis-to-ground potential is limited for the immediate future to a ratable 250 V.

Floating exposes trouble

Currently, there are few instruments in the 3-to-5-kV, common-mode-input rating range, but many more will be available within the next two years, as safety standards become more common.

But now the standard laboratory technique for floating measuring instruments from ground, disconnecting the ground pin of the equipment's ac power-line cord, is coming under fire from the safety engineers. When this floating takes place, every exposed metal part of an oscilloscope, for example, rises to the common-mode voltage of the measured signal and presents a great opportunity for electrical shock. Because of this shock hazard, safety engineers are talking of redesigning the BNC connector to eliminate its exposed metal.

The alternative is to redesign the inputs to the oscilloscope and make all measurements differentially. This alternative, however, would raise the price of the oscilloscope from a few hundred to a few thousand dollars and reduce the bandwidth from a few hundred megahertz to a few megahertz.

To permit floating at virtually any potential, many companies are going to battery operation. But one specification is extremely important for the safe use of battery-powered instruments: leakage. If a battery-operated voltmeter, for example, is being used to measure voltage between the legs of a three-phase powerline, every part of the meter is above ground potential. If there is any leakage current flowing through the instrument's case, it may end up flowing through the person making the measurement.

Safety specifications for this type of test equipment are not easily generated. For example, capacitors must be tested to see if they withstand a certain voltage. And, if they are of the oil-filled variety, the dielectric may become polarized during the testing process. When discharged, these capacitors will present a safety hazard in themselves after—as well as during—the measurements. The reason: the oil-filled recharge without connection to external circuitry.

Binding posts are hazardous too

Even the lowly binding post is due for a redesign, because its exposed metal parts allow all too easy contact between an instrument user and hazardous voltages. Hazardous voltages are currently defined by safety engineers as 30-V rms for sinusoidal signals and 60 V for dc, with variations for nonsinusoidal waveforms.

Today's thinking is that ordinary five-way binding posts are unsafe for use with these voltages, and that something without exposed metal must be designed to take their place. But so far no one has designed anything that can connect to wires and banana plugs as efficiently as the standard five-way binding post.

Providing banana jacks recessed from the mounting panel so that only the mating banana plug can make contact with the jack has been reasonably successful. This method solves the problem at one end of the cable, but the other end of the cable needs to make contact, too. Thus either the other end of the cable has banana plugs with unsafe voltage on them, or some other connector is devised.

Binding posts are a safety problem whether they are located on sources of power or on the inputs to measuring instruments that never act as a source. Once the connection is made between the source and measuring circuit, all of the binding posts in the completed path are live.

Sinking sources save

Two notable ways to prevent instruments from damaging one another by misconnection are making sources capable of sinking current as well as sourcing it, and alternatively, disconnecting themselves from devices under test if required to sink current.

An ac calibrator from John Fluke has a transient detector that shuts down the calibrator and equipment under test before a destructive arc can occur. The calibrator does this by detecting the corona discharge that precedes an arc discharge. ■■

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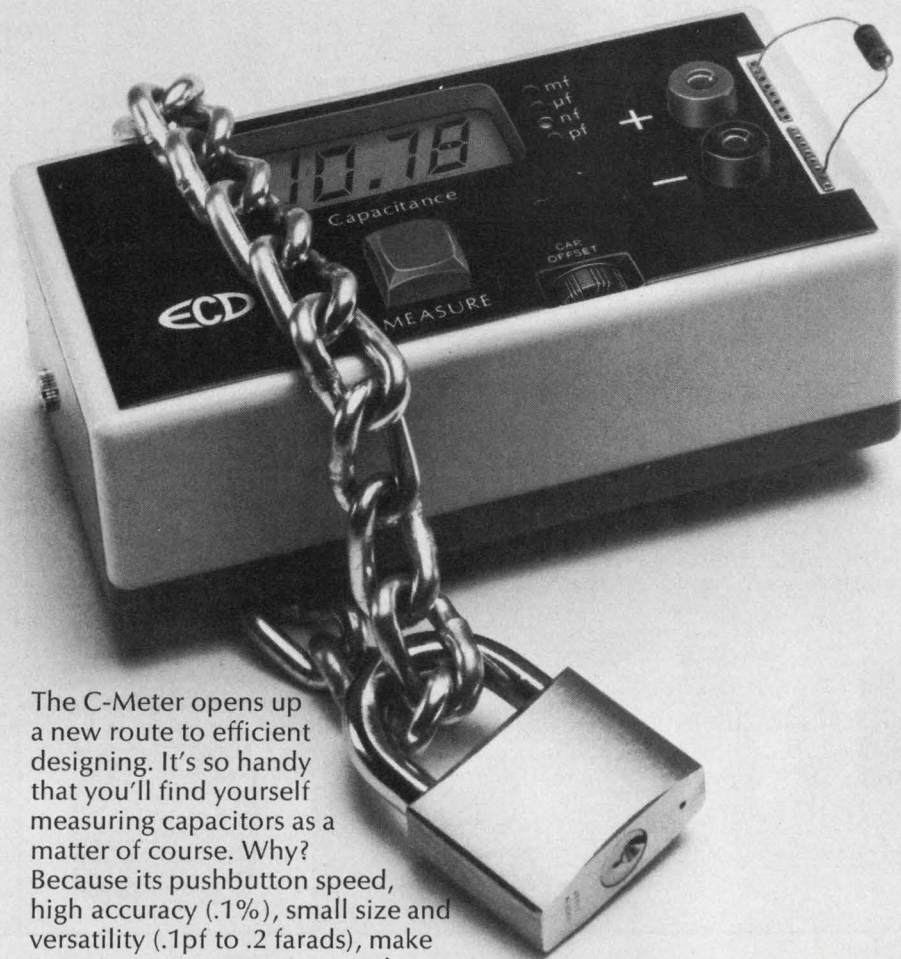


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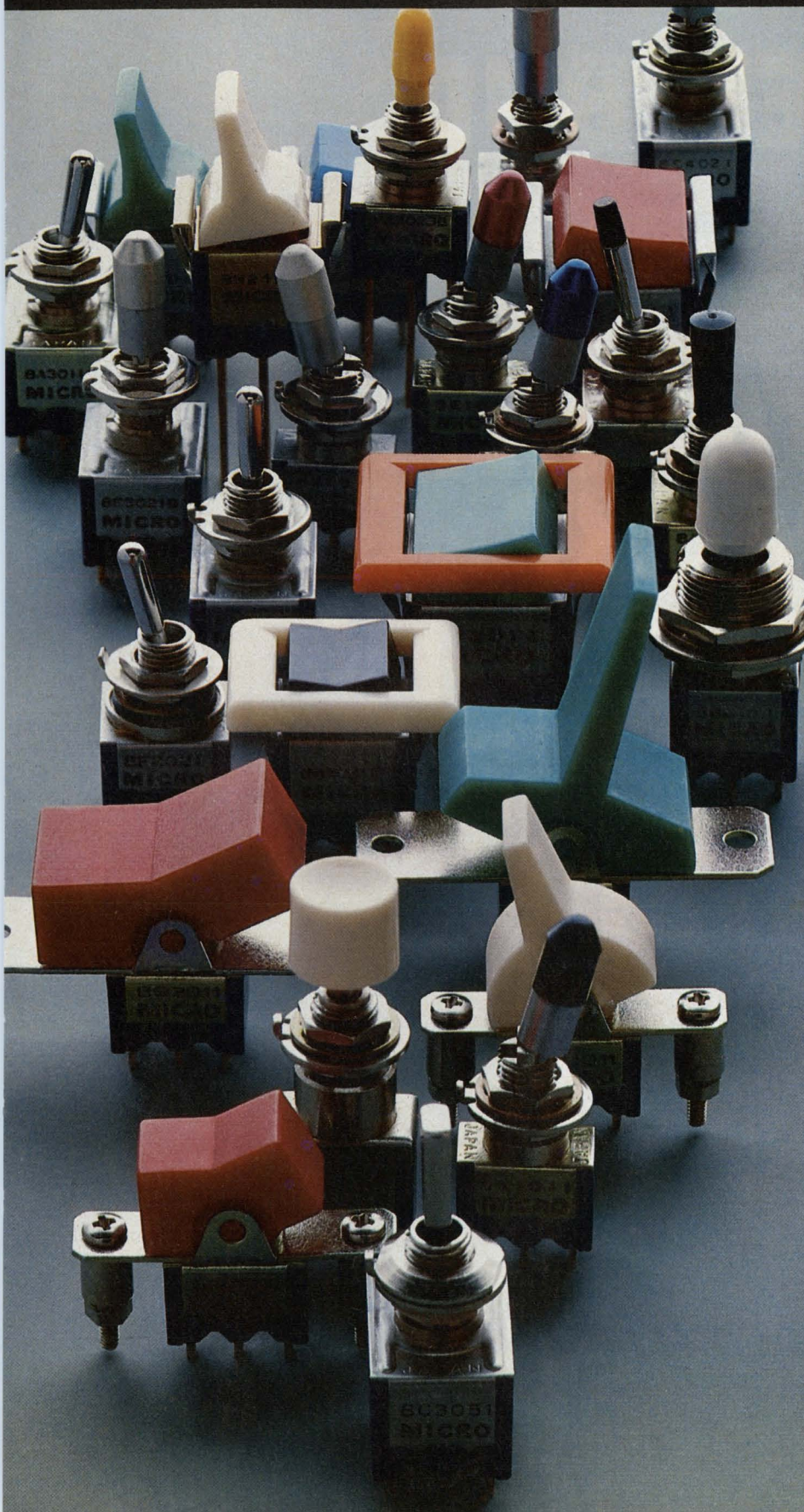
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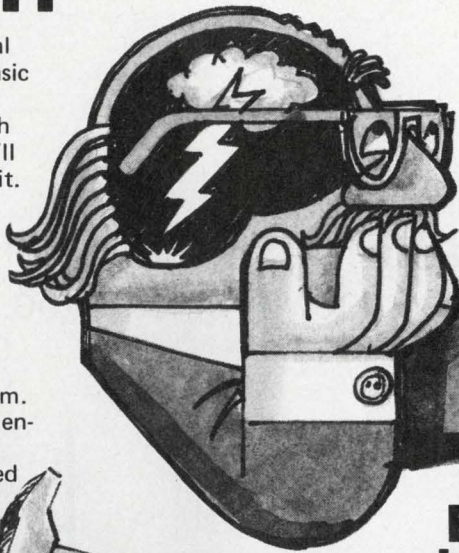
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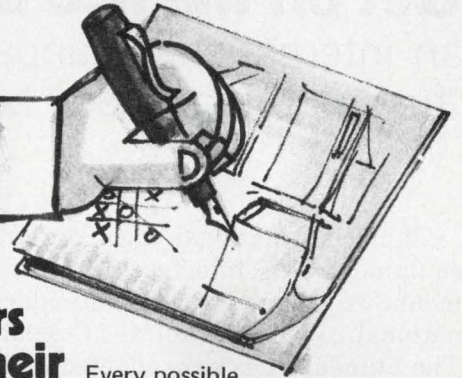
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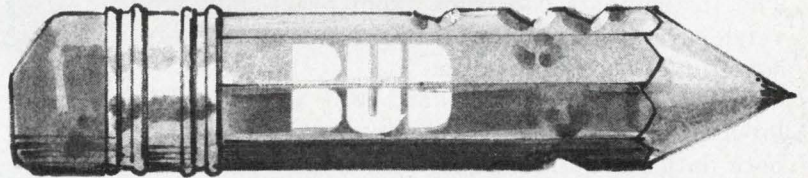
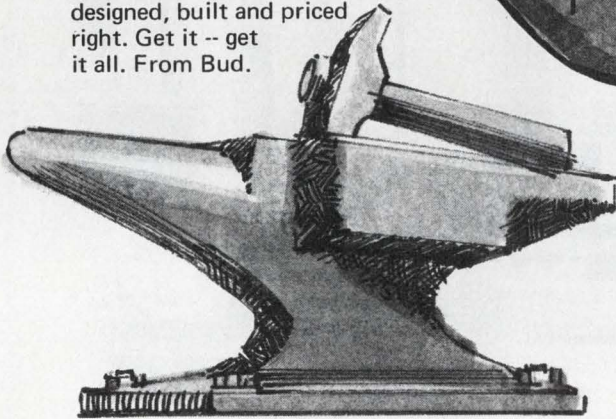
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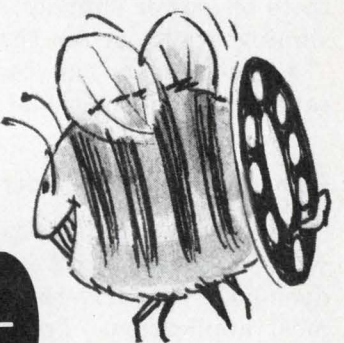
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Get on the IEC bus. Soon to be an international standard for interfacing instruments, the bus brings many benefits—and a few problems too.

Think international when you interconnect test equipment. An interface for measuring instruments will soon be a world standard of the International Electrotechnical Commission (IEC). The Standard has been adopted by the IEEE (Std. 488-1975), with a change in the connector proposed by the IEC.

Many benefits accrue from the standard. With it, you can connect up to 15 different instruments, spaced up to a total of 65 cable feet (20 meters). The instruments can come from practically any vendor—only minor software adjustments are sometimes necessary (Fig. 1).

The proposed IEC standard uses a byte-serial, bit-parallel format, with bidirectional lines for both data flow and addressing. Alterations to accommodate special needs can be made with simple and inexpensive reprogramming. And since the system is modular in concept, you can start small and work up as necessary.

Other advantages of an international standard include the following:

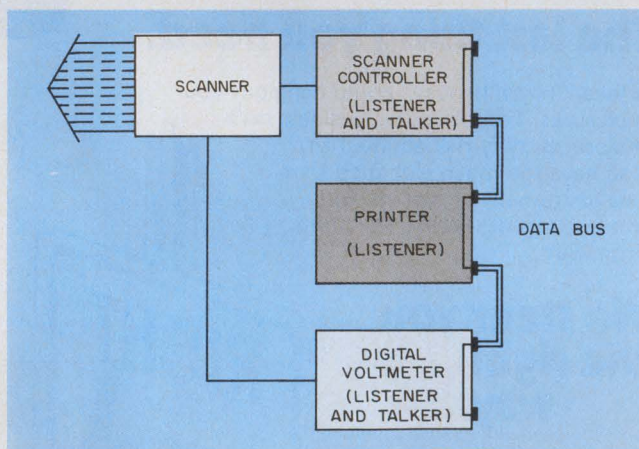
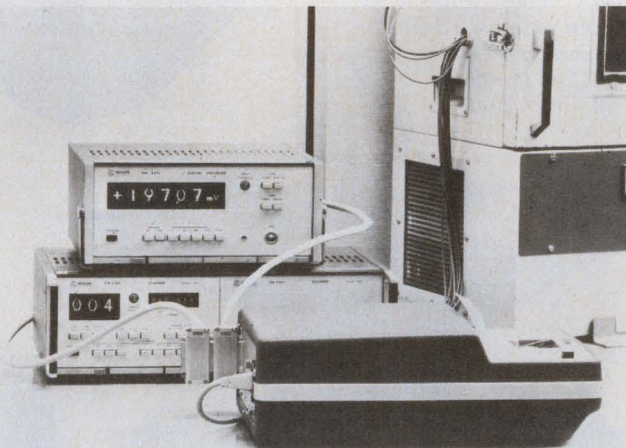
- No engineering costs are tied up in developing special interfaces.
- Instrument manufacturers can concentrate on producing instruments, not interface systems.
- Specialized modules can be easily produced; for example, power-supply makers can concentrate on power supplies and not worry about designing a system for the supplies to fit into.
- Instruments can be optimized internally to satisfy the international standard.

Details of the IEC standard

Maximum speed of the standard is 1 Mbyte/s with three-state drivers and 250 kbyte/s with open-collector drivers, speeds high enough for most applications. Transfer of one 8-digit word (8 characters) takes about 32 μ s.

The specified cable has both male and female

Manfred Richter, Interface Engineer, Philips Electronic Industries GmbH, Hamburg, Germany.



1. With the new IEC standard, "small" test systems are just as easy to interface as large ones (top). How the equipment interconnects is shown at the bottom.

connectors, so that plugs can be stacked piggy-back fashion, thus saving space on instrument back panels (Fig. 2). This makes expansion of the system very simple.

In general, any communications link requires three active devices: a listener, a talker and a controller. The controller decides the role each device plays at any time; any device not addressed remains inactive. Of course a device can perform more than one role at different times.

The proposed IEC bus system carries all mes-

Why an international interface standard?

The basis of the IEC standard is a set of objectives that define the bus but leave designers free to select the necessary interface capability. The objectives are:

- To provide cost-effective capability for simple bench systems.
- To be compatible with simple controllers. However, a system limited to just two devices must be able to use the link without controllers.
- To serve the needs of a wide variety of products—such as controllers, processors and instrumentation.

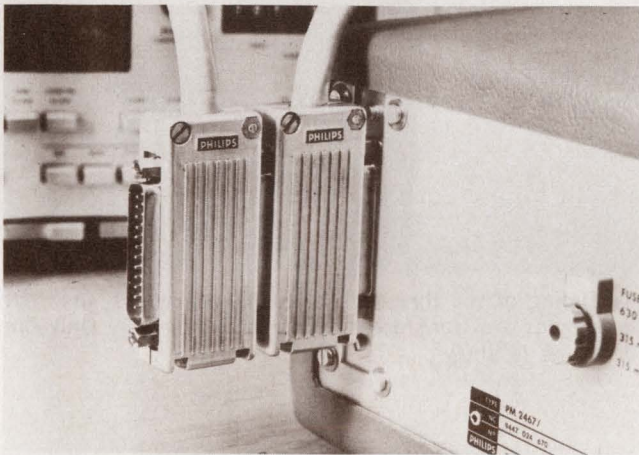
- To be compatible with the ISO, a 7-bit code for address and command data that's easy to generate, display and read.

- To provide for flexible data rates and communication paths with a minimum of timing restrictions.

- To provide capability to accommodate multiple listeners and direct communication paths—without buffering in the controllers.

- To permit a mode for transfer of basic data with unrestricted codes.

- To minimize the number of wires.

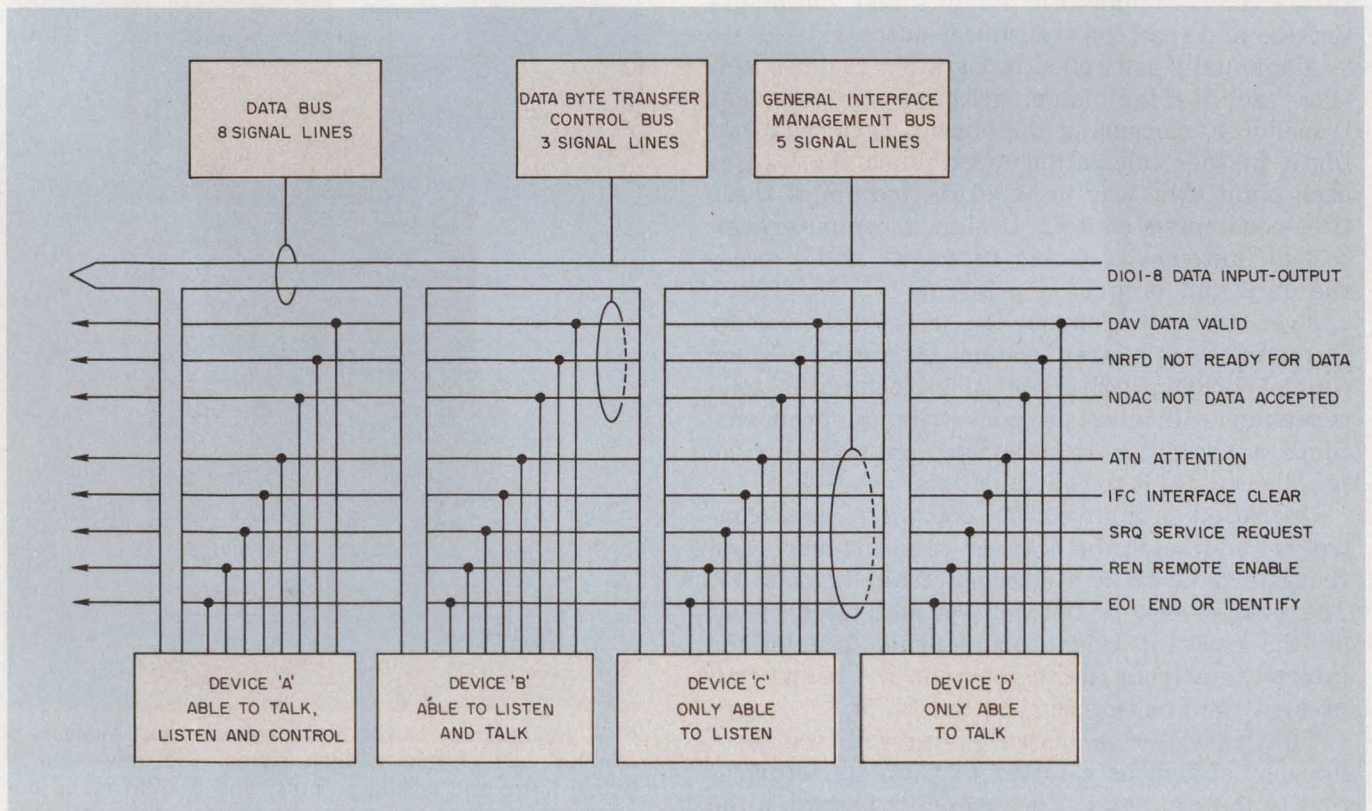


2. Space is saved and system expansion is easy with connectors that allow piggy-back stacking.

sages on a set of 16 lines: eight data-input/output lines, three data-transfer lines and five bus-management lines (Fig. 3).

The three data-transfer lines carry information from an addressed talker to an addressed listener or listeners. The Data-Valid (DAV) line indicates the availability and validity of data, the Not-Ready-For-Data (NRFD) line indicates the condition of readiness to receive data, and the Non-Data-Accepted (NDAC) line indicates acceptance completed. These three lines operate in what is called a three-wire interlocked handshake process to transfer each data byte across the interface (Fig. 4). The sequence of operations runs as follows:

1. Initial conditions are set up in talkers and



3. What the various bus wires do: 16 lines take care of data flow, data transfer and general housekeeping chores.

listeners—the DAV line is set to high (data not valid), the NRFD set to low (no listener ready for data) and NDAC to low (no listener has accepted data).

2. The talker checks the line conditions, then puts a data byte on the lines.

3. Listeners are ready to accept data, so the NRFD line goes high—this cannot happen before all listeners are ready.

4. When a talker senses that NRFD is high, it sets DAV low to indicate that the data are valid.

5. The first listener sets NRFD to low to indicate that it is no longer ready and starts to accept data. The other listeners follow at their own pace.

6. First listener to finish sets NDAC to high to indicate it has accepted the data.

7. When the final listener has indicated that it has accepted the data, NDAC goes high.

8. The talker senses NDAC high and sets DAV high to indicate that the data are no longer valid.

9. Talker removes the data from the line.

10. The listeners, sensing DAV is high, set NDAC low in preparation for the next cycle.

11. All three lines are now in the initial states.

A typical example of how the IEC data bus can be used is demonstrated by a system for the analysis of the stresses in prototype railway cars and passenger carriages. (Fig. 5).

A practical example of the bus

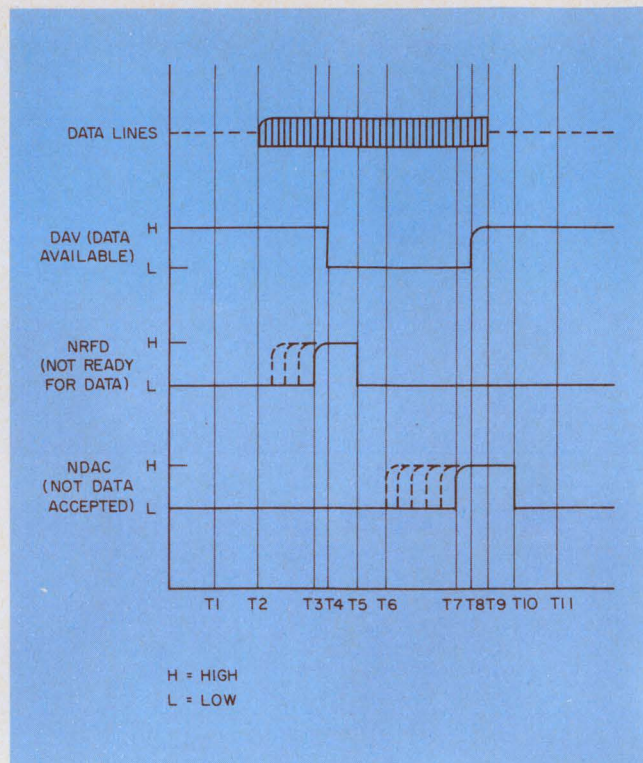
Upwards of 300 strain gauges are connected to the vehicle under test. Bridges and voltmeters process and read the transducer outputs.

A manually controlled test system requires setting each bridge value, selecting the relevant transducer, measuring the output, then performing a further calculation to establish the load at each point. One way to avoid the tedium of these time-consuming chores: Design a computer-controlled, automatic system to collect and process the data and produce a printout.

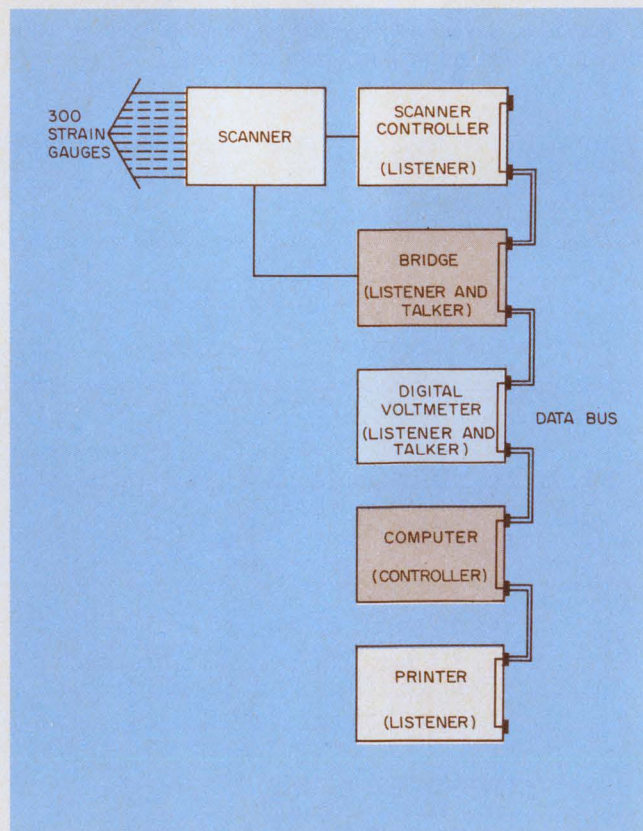
Even trying to connect the series of necessary instruments in a star system—scanner, scanner control, bridge, digital voltmeter, computer, teletypewriter—involves serious wiring problems. Since a computer is necessary anyway, it's no problem to use it to control a data bus.

Operation is simple. The computer, as a controller, addresses the scanner—the listener—and requests data from a selected-strain transducer. The bridge—also a listener—is addressed to set up the relevant bridge components to take the information from the scanner. So the bridge can present the analog signal to the DVM.

The voltmeter is instructed to act first as a listener, second as a talker to pass the information to the computer. The computer processes the information and commands the printer to listen



4. Timing of the three-line handshake process, in which data bytes are transferred across the interface. Only one data line is shown.



5. A practical use of the bus involves stress analysis of railroad cars. Strain gauges collect the raw data, a bridge forms the analog outputs, and a DVM reads and converts the signals. A computer controls the entire system automatically.

and do its job. Of course, if the information is wanted only for external processing, the printer can control the system and produce a series of output-voltage readings for later use.

The operation of the strain-gauge test system conforms to the following sequence:

1. The computer—as a controller—uses the IFC (Interface Clear Line) to start the system.
2. The controller sends a DCL (Device Clear) message to set all devices to an initial state.
3. The controller sends the listen address of the scanner control, followed by data, to select a particular strain gauge.
4. The controller sends an “unlisten” command, then the listen address of the bridge, followed by data for matching a selected strain gauge.
5. The controller again sends an “unlisten” command, then the listen address of the DVM, then data to read the output of the bridge on the analog line.
6. The controller sends an unlisten command, sets itself to listen, then sends the talk address of the DVM.

7. When the DVM has the measurement information, it sends the data to the computer.

8. When the computer has processed the information, it again clears the interface and sends the listen address of the printer, followed by the required output information.

9. When the printer has typed all information, the controller can restart the sequence.

Sometimes, output information is needed in several forms—say, in a tape memory as well as a printout. If so, bear in mind that a tape drive is obviously much faster than a printer and can supply a data-accepted signal as soon as it is finished. But a controller will not react until all devices receiving information have sent data-accepted signals, that is, the controller must wait until the NDAC line goes high.

Unresolved problems

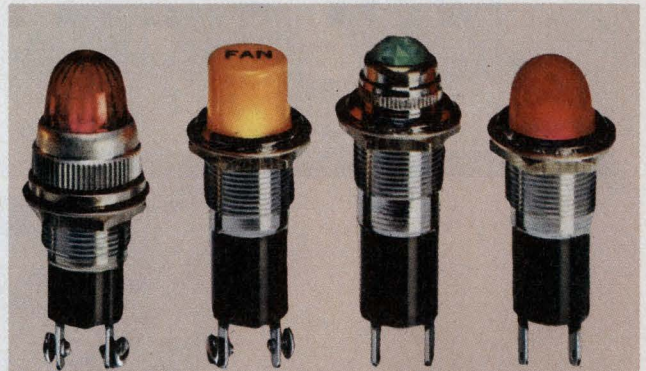
For distances longer than 20 m, the problem becomes more complicated. The present IEC system can be applied up to 330 ft (100 m) with some upgrading of hardware. For much longer distances, from 2000 up to 3000 m (2 to 3 km), it is necessary to go to full serialized busses with only one or two wires.

Much more work is necessary before all the interconnection problems are solved. But the IEC bus is the most practical step yet taken. Its success depends on people making an effort to understand and use the bus.

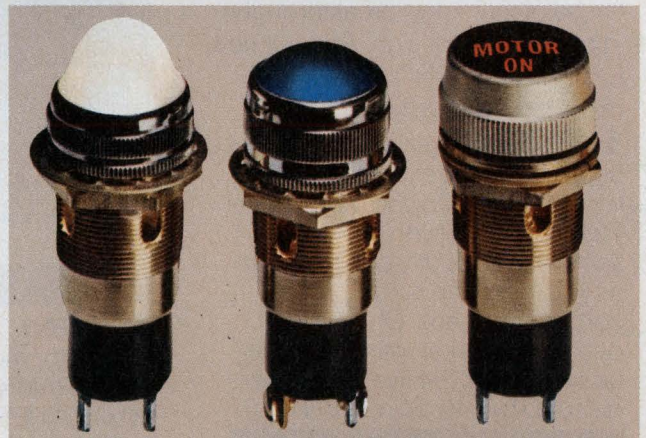
Further work is also underway in the field of “software,” for example, data formats. The problem here is to decide where to stop. If the description is taken too far, individual designers can be unnecessarily restricted. ■■

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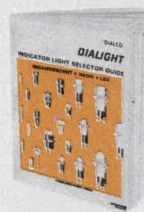
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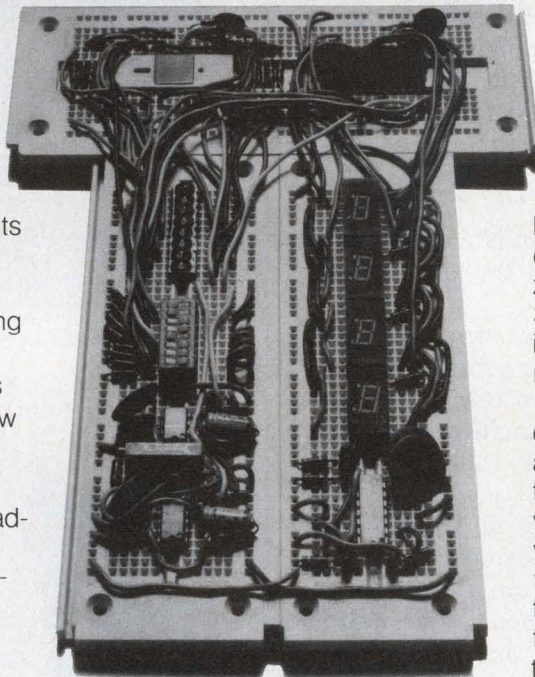
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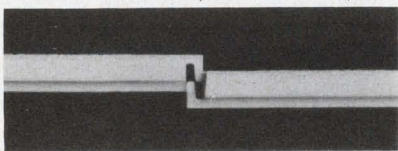
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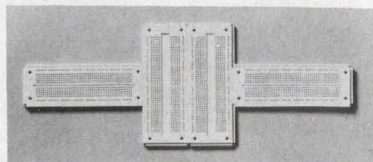


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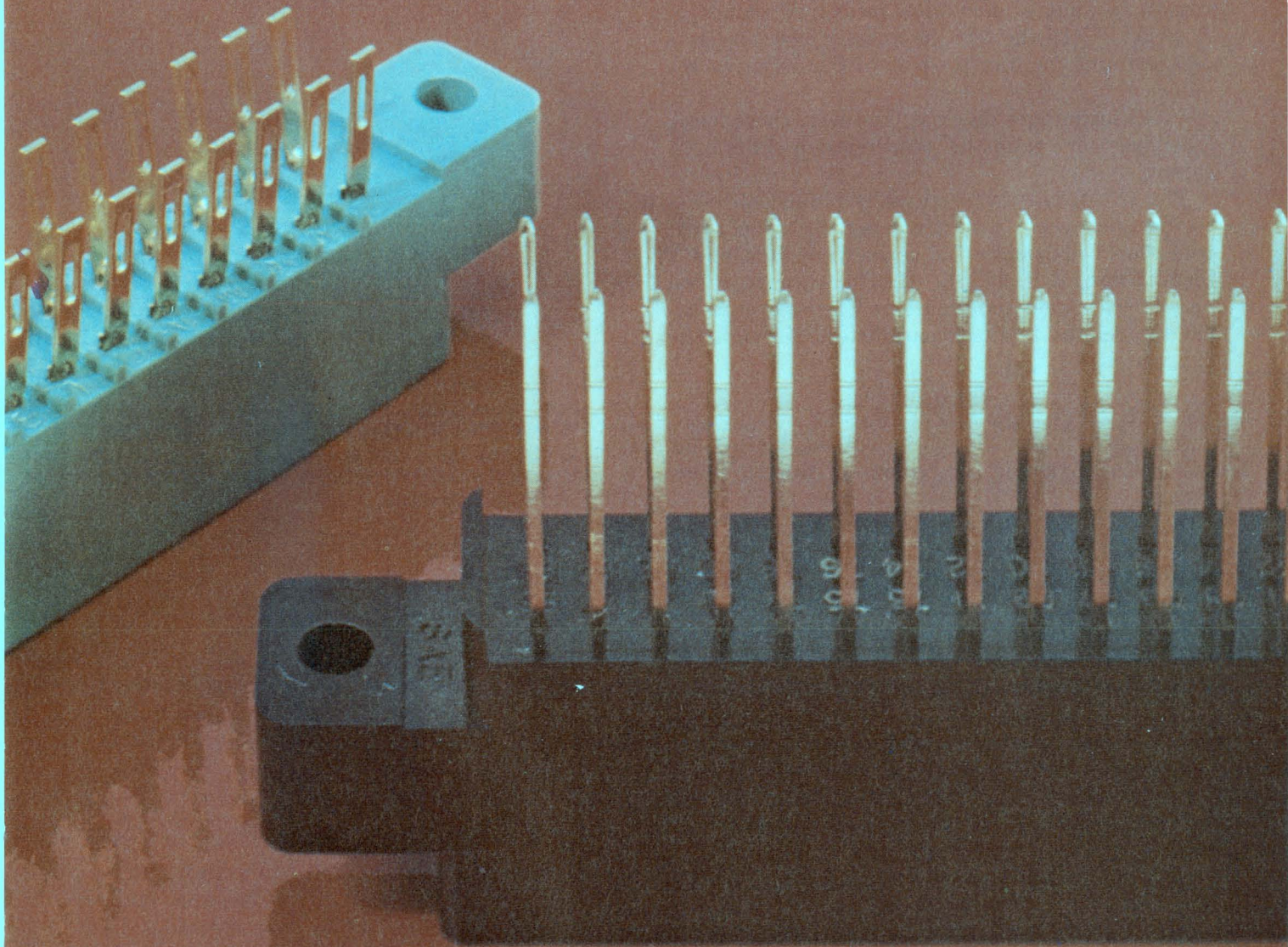
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CIRCLE NUMBER 66

Measuring capacitor loss: Are S-parameters any good? They're not, but other methods—like the use of Q-bridges or resonant coaxial lines—are acceptable.

In determining the losses of microwave capacitors, the Q values calculated from measured S parameters are worthless. Perhaps this is the reason that articles endorsing S parameters for capacitors emphasize the importance of low series resistance, but seldom give measured values of r_s or Q_c .^{1,2,3} In the few instances when such data can be found, no hint is given of the origin of the values.

Valid techniques do exist, however, those using Q-bridges or resonant transmission lines, for example.

The two S parameters usually published to describe microwave capacitors are S_{11} —the input reflection coefficient of a series capacitor and a termination, Z_o , and S_{21} —the forward insertion loss of the same combination. The Q of the capacitor relates to these parameters through the expression:

$$Q_c = \frac{2|S_{11}||S_{21}|}{1 - |S_{11}|^2 - |S_{21}|^2} \quad (1)$$

A recent treatment⁴ of the subject states that the Q of a capacitor can be found from S_{11} alone, giving:

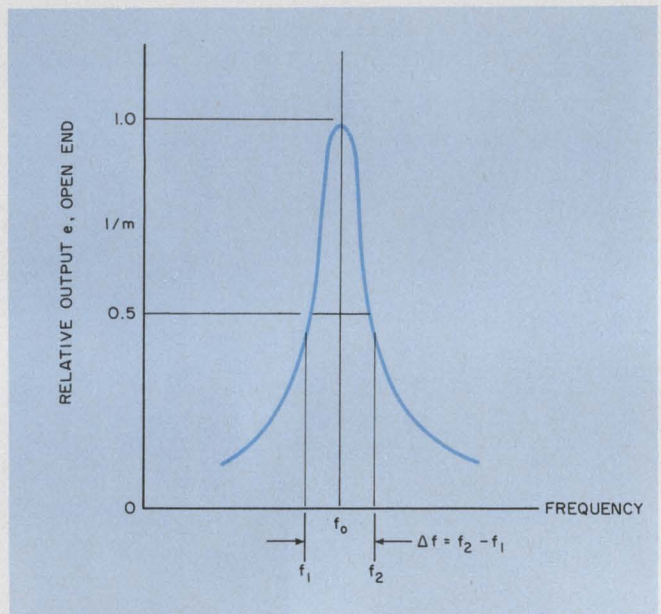
$$Q_c = \frac{\sin \theta}{\cos \theta - S_{11}} \quad (2)$$

where θ is the phase angle of S_{11} .

Although Q is acknowledged as a key parameter, no values are given. Instead, the "insertion loss" is tabulated for several capacitors over a wide range of frequencies. The loss is correctly defined as the sum of the reflective and dissipative losses, but the insertion loss is based on the expression for the reflection loss only.

For capacitors of high, or even modest Q values, it is true that the dissipated power is extremely small compared to the reflected power, but the correct relationship includes both and is given by:

$$\text{Insertion loss} = 10 \log_{10} \left(\frac{\text{reflected}}{1 - |S_{11}|^2} \right) + 10 \log_{10} \left(\frac{|S_{21}|^2}{1 - |S_{11}|^2} \right) \quad (3)$$



1. Using a transmission line to measure capacitor loss: An rf millivoltmeter reads the line output at resonance and also reads the output at two points on either side of resonance. The Q of the capacitor is then calculated from the frequency deviations.

or Insertion loss = $10 \log_{10} |S_{21}|^2$.

You may well wonder why insertion loss for capacitors is emphasized. For small values of capacitance, at frequencies in the order of a few hundred megahertz, the insertion loss is naturally high. The loss drops as either the capacitance or frequency increases, and it is almost entirely a function of the reactance.

Is insertion loss of any value?

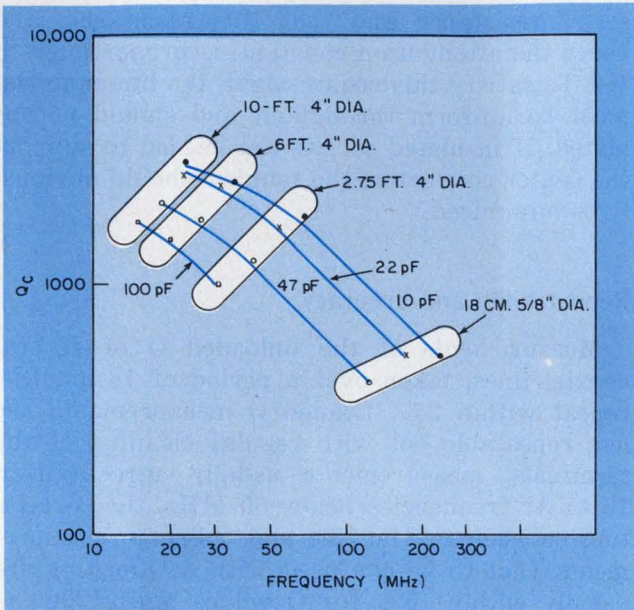
To attribute a low Q factor to a high insertion loss would be folly. The only redeeming value of insertion loss, other than characterizing reactance as a function of frequency, is to discover resonances in the capacitor or the test fixture.

The equations already given by Q_c are correct. Then where does the problem lie? The limitation is in the measuring system. Most equipment cannot resolve the small values of resistance and the resulting small differences of phase. Remember, the capacitor loss must be detected in the

R. E. Lafferty, Vice President and Engineering Manager, Boonton Electronics Corp., Route 287 at Smith Road, Parsippany, NJ 07054.

presence of a total resistance equal to twice the characteristic impedance of the system (100 Ω). What little effect the series resistance has on both S_{21} and S_{11} is lost in the uncertainty of S-parameter measurements.

Example: A 22-pF capacitor with a Q of 200 at 300 MHz has calculated values of 0.234160 for S_{11} and 0.971028 for S_{21} . If the series loss could be reduced to zero, calculated values would be 0.234424 and 0.972134, respectively, a change of only 0.11%, or approximately 0.01 dB. In a meas-



2. How the Q's of ceramic capacitors vary with frequency: At high frequencies, the slope of the plots vary approximately with the -1 power of frequency. At very high frequencies, when the skin depth becomes less than the plate thickness, Q will vary as $(f)^{-1.5}$.

uring system with two-digit resolution, there would be no detectable differences in the S values.

The failure of S parameters to provide significant values of Q is clearly illustrated in a table of calculated Q values for several capacitors. Measured values of S_{11} and S_{21} have been taken from published data, and the results of both equations (1) and (2) are listed. The absurd values of Q_c obtained with either equation are a convincing argument against using S parameters to measure capacitor loss.

Is there a better way?

How can the high-frequency loss of a capacitor be measured? A Q-bridge is a good means of directly measuring Qs up to 10,000 for capacitors from 20 to 1000 pF at frequencies of 0.1 to 50 MHz.

For frequencies above 50 MHz, the only suitable method known to the author requires a resonant coaxial transmission line. A quarter-wave

coaxial line is coupled loosely to a stable signal generator. The outer-to-center conductor spacing of the line should be compatible with the terminal spacing of the capacitor to be measured, provided the Q of the line can be held to a high value. The generator should have a digital display of the output frequency; if it doesn't, a counter must be used.

An rf millivoltmeter, lightly coupled to the open end of the line, detects the voltage at the resonant frequency, f_o , and on each side of resonance (Fig. 1).

The Q of the line at f_o may be calculated from:

$$Q_o = (f_o/\Delta f) \sqrt{m^2 - 1}, \quad (4)$$

where Q_o denotes the measured Q of the unloaded quarter-wave line, m equals the ratio of resonant to off-resonant voltage, and Δf equals the total bandwidth between the off-resonant voltage points. If the half-voltage points are used, Eq. 4 reduces to:

$$Q_o = \sqrt{3} (f_o/\Delta f) \quad (5)$$

Measuring Q_c

Connect the capacitor to be tested across the open end of the line. Resonance will now occur at a lower frequency, f_1 , where the reactance of the line equals the reactance of the capacitor. The generator frequency is again adjusted above and below resonance where the coupled voltage falls to half of its resonant value. Q_c can now be calculated using the following equation:

$$Q_c = \frac{\cos \beta_{1l}}{\sqrt{D_1 D_2 / 3 - (\pi/4Q_o) \sqrt{f_1/f_o} D_3}}, \quad (6)$$

$$\text{where } D_1 = \cos \beta_{3l} - \frac{\sin \beta_{3l} \left[\frac{f_3}{f_1} \right]}{\tan \beta_{1l}},$$

$$D_2 = \frac{\sin \beta_{2l} \left[\frac{f_2}{f_1} \right]}{\tan \beta_{1l}} - \cos \beta_{2l},$$

$$D_3 = \sin \beta_{1l} + \frac{\cos \beta_{1l}}{\tan \beta_{1l}},$$

and β_{1l} , β_{2l} , and β_{3l} are the electrical lengths of the line at frequencies f_1 , f_2 , and f_3 , respectively.

$$\beta_{1l} = (f_1/f_o) 90^\circ$$

$$\beta_{2l} = (f_2/f_o) 90^\circ$$

$$\beta_{3l} = (f_3/f_o) 90^\circ$$

Example: With a 6-ft copper line having an I.D. of 4 in. and an O.D. of 1.125 in., the natural resonant frequency is 41 MHz, and $Q_o = 2190$. When a 22-pF capacitor is connected across the open end, the resonant frequency drops to approximately 31.76 MHz. The measured frequencies at which the voltage falls to half of the resonant voltage are:

$$f_2 = 31.7766 \text{ MHz and } f_3 = 31.7448 \text{ MHz.}$$

Therefore $f_1 = (f_2 + f_3)/2$, which equals 31.7607 MHz.

With the aid of a calculator the following terms can be found:

$$\beta_{1l} = (31.7607/41) 90^\circ = 69.718610^\circ$$

$$\beta_{2l} = (31.7766/41) 90^\circ = 69.753512^\circ$$

$$\beta_3 l = (31.7448/41) 90^\circ = 69.683707^\circ$$

$$\text{and } \sin_1 = 0.938002$$

$$\cos_1 = 0.346631$$

$$\tan_1 = 2.706052$$

$$\sin_2 = 0.938213$$

$$\cos_2 = 0.346060$$

$$\sin_3 = 0.937790$$

$$\cos_3 = 0.347202$$

You can now solve for D_1 , D_2 , and D_3 , and then Q_c :

$$D_1 = 8.2292 \times 10^{-4}$$

$$D_2 = 8.2299 \times 10^{-4}$$

$$D_3 = 1.066097$$

$$Q_c = 2500.$$

An investment in a stable signal generator, a sensitive rf millivoltmeter and a programmable calculator will be well worth the cost if you intend to use this technique. Incidentally, if you use a generator with phase lock, be sure that the display of frequency follows the vernier control in the locked mode.

Because of the rigorous interrelationship of the measuring frequency, the capacitance and the length of the line, an unfortunate constraint is imposed with this method. For a given line, you may select capacitance or frequency, but not both. The parameters are related as follows:

$$C = \frac{1}{\omega_1 Z_0 \tan(1.91 \times 10^{-10} \omega_1 l_{\text{mm}})} \quad (7)$$

It is convenient to draw a graph of capacitance vs frequency for each line.

Sources of error

For the signal source, the major requirement is frequency stability. Accurate measurements can't be made with a generator that drifts. Residual AM or FM will not affect the measurement.

A small loop inserted at the shorted end of the line should be sufficient to excite the line and give a good reading on a loosely coupled rf millivoltmeter without introducing noticeable loss in the line. A terminating resistor in series with the loop will reduce the SWR on the connecting cable. Whether or not the induced voltage is a function of frequency is of little consequence because of the small deviation needed for the measurement.

There are a few requisites for the rf millivoltmeter: a high-impedance probe is important; it should be coupled loosely to the open, or test end of the line; and both the full-scale and half-scale readings on the ranges to be used (probably 1, 3, and 10 mV) should be calibrated.

For large-diameter lines, you can thread the probe directly through the outer wall. For smaller lines, a threaded bushing can be soldered to the outer wall, with some form of insulated feed-through connector to couple the probe tip to the center conductor of the line.

Probe loading with loose coupling does not in-

fluence the measured Q . This is proven by coupling the millivoltmeter at both the open end and as far down as a sixteenth of a wavelength. There is no measurable difference in the results. Calculations made with the measured capacitance between the probe and the line, and with the input resistance of the probe, also confirm a negligible contribution by the probe to line loading.

Errors of a few percent in the millivoltmeter calibration will cause similar errors in the measured Q and, with calibration, errors should remain less than 2%.

Eq. 6 assumes that the entire line loss is from series resistance and that this resistance, and hence the attenuation constant, is proportional to \sqrt{f} . To satisfy this requirement, the line material must be uniform throughout and should not be plated. If insulated screws are needed to support the center conductor, the number should obviously be minimized.

Repeatability and accuracy

Measurements of the unloaded Q of several coaxial lines, taken over a period of 18 months, repeat within 2%. Loaded Q measurements are less repeatable but with regular cleaning of the terminals, measurements usually agree within 10%. At frequencies below 50 MHz, the correlation between coaxial line and Q -bridge measurements (not to be confused with a Q -meter) are usually within 15% for Q values under 2000.

For Q values less than 2500, and assuming the Q of the line is greater than that of the test capacitor, the accuracy of this method may be within 15 to 30%. All factors considered, it is not now prudent to place a better figure of uncertainty on the outlined measuring technique. Regardless of the absolute accuracy, the measurement provides reasonable Q data— S -parameter measurements do not.

A plot of Q vs frequency for a few ceramic capacitors approximates the expected slope of $1/f$ at high frequencies for capacitors of low dielectric loss and with effective plate thickness less than the skin depth (constant r_s). Such a plot is given in Fig. 2.

Users of Q -meters who have experienced difficulty in measuring the loss of capacitors may be concerned that the transmission line measurement suffers from the same deficiencies. Two important differences between the two techniques yield a significant improvement in accuracy for the transmission line.

First, when you connect a capacitor to a line, the attendant lowering of the resonant frequency is accompanied by a predictable change in line loss (within a few percent). But when you connect a capacitor to the Q -meter, the internal variable capacitor is reduced to restore resonance.

Tabulated Q values calculated from published data for S_{11} and S_{21}

C (pF)	f (MHz)	S_{11} (Re)	S_{11} (Im)	S_{21} (Re)	S_{21} (Im)	Q_c (from S_{11} & S_{21})	Q_c (from S_{11})
10	100	0.54	-0.65	0.29	0.44	109	3.7
	110	0.47	-0.67	0.33	0.46	96	3.3
	120	0.41	-0.69	0.37	0.47	-480	2.9
	130	0.36	-0.70	0.41	0.49	-36	2.7
	140	0.30	-0.69	0.44	0.50	-103	2.6
	150	0.25	-0.68	0.47	0.50	237	2.5
	160	0.20	-0.67	0.50	0.49	47	2.3
	170	0.15	-0.66	0.53	0.49	47	2.1
	180	0.11	-0.65	0.55	0.49	43	2.0
	190	0.07	-0.64	0.58	0.48	52	1.9
200	0.04	-0.62	0.61	0.48	84	1.8	
22	100	0.17	-0.55	0.68	0.46	-175	3.4
	200	-0.09	-0.32	0.89	0.31	482	1.6
	300	-0.14	-0.18	0.94	0.22	28	0.94
	400	-0.15	-0.09	0.97	0.16	119	0.50
	500	-0.15	-0.03	0.98	0.13	-432	0.17
	700	-0.11	0.04	0.98	0.09	13	-0.32
	1000	-0.02	0.09	0.98	0.05	6.3	-3.2
	1500	0.07	0.03	0.99	0.03	11	0.47
	2000	0.03	-0.05	0.99	0.01	7.0	-1.9
	2500	-0.04	-0.03	0.99	-0.01	5.7	0.71
100	100	-0.02	-0.16	0.97	0.15	30	3.5
	110	-0.03	-0.14	0.98	0.14	-567	2.8
	120	-0.03	-0.13	0.98	0.13	54	2.7
	130	-0.03	-0.12	0.98	0.12	25	2.7
	140	-0.04	-0.11	0.98	0.11	17	2.1
	150	-0.04	-0.10	0.99	0.10	-126	1.9
1000	100	-0.01	-0.03	0.99	0.01	3.3	2.7
	200	-0.02	-0.03	1.00	0.00	-55	1.4
	300	-0.03	-0.03	0.99	-0.01	4.7	0.94
	400	-0.05	-0.02	1.00	-0.02	-33	0.38
	500	-0.05	-0.01	1.00	-0.02	-30	0.16
	600	-0.06	0.01	0.99	-0.03	7.9	-0.16

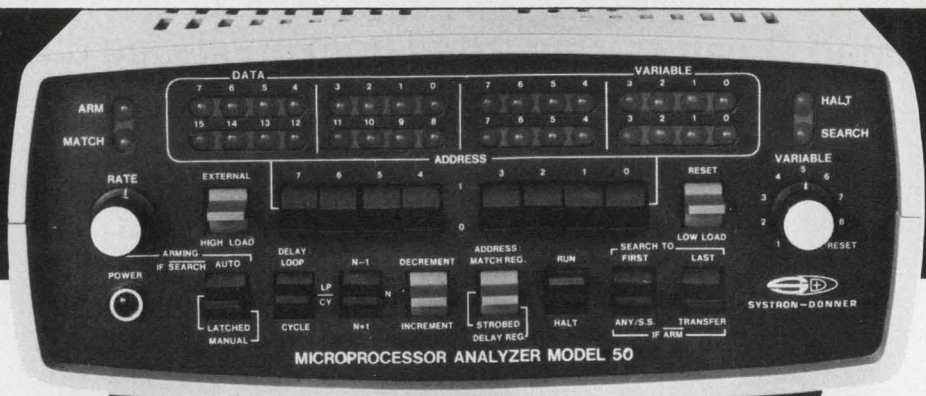
The change in the capacitance affects the loss of the internal capacitor, but the extent of the change is difficult to determine, and the repeatability is suspect. As a result, it is usually ignored, and the measured Q is generally higher than the correct value—and it may even be negative!

Second, the intrinsic Q values of transmission lines are substantially higher than those of the work coils used with a Q-meter. Consequently, capacitors of moderately high Q have a pronounced influence on the effective loss of a coaxial

line. The same capacitor on a Q-meter may barely change the reading. ■■

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4. *Vitramon News*, Vol. 11, No. 5, November/December, 1975.



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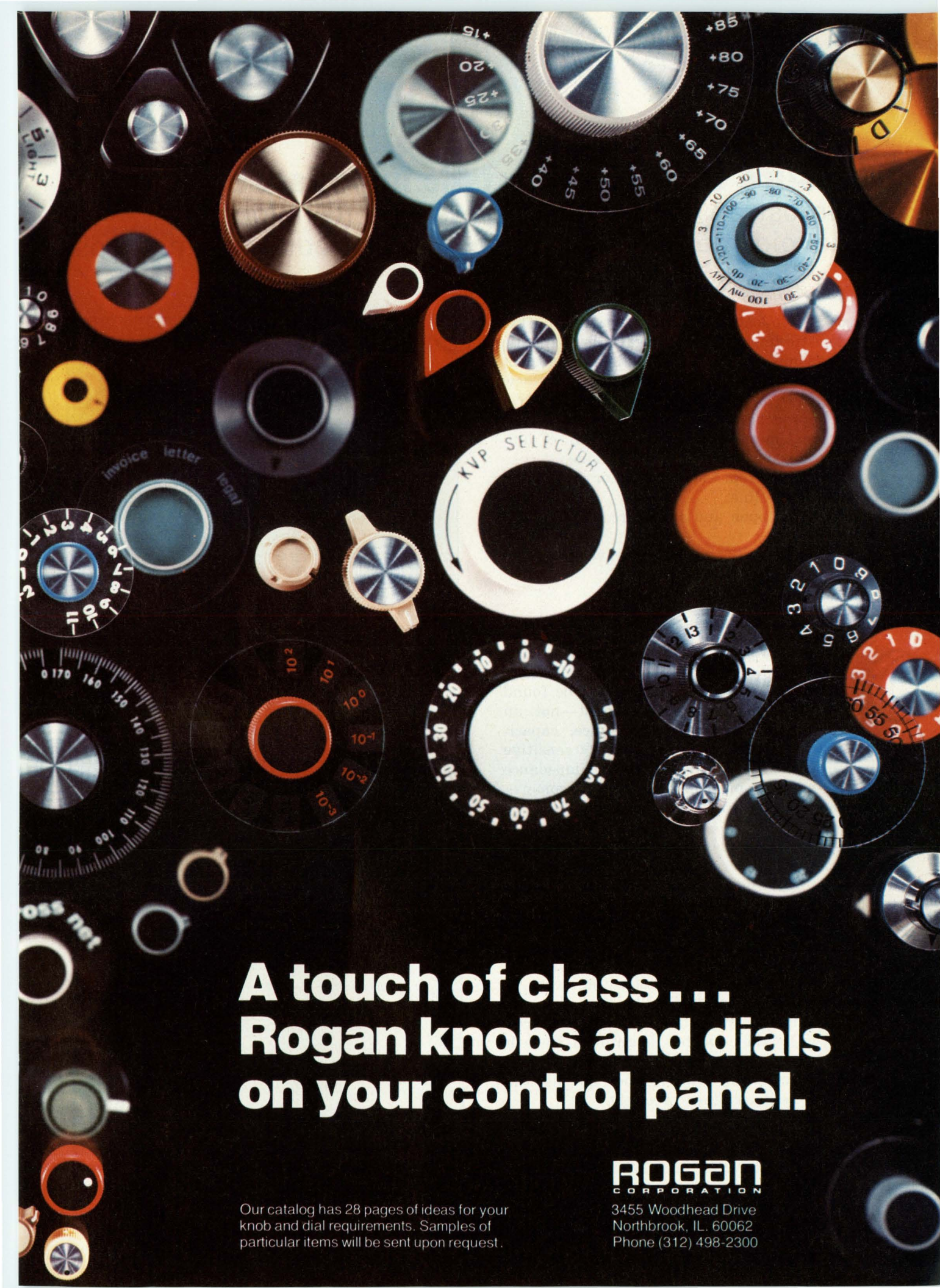
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Here's a two-load method for determining the characteristic impedance, Z_0 , of almost any audio or rf transmission line of any length without having to assume a no-loss condition. The new method avoids most of the disadvantages of traditional approaches.

Traditional methods of determining Z_0 of uniform transmission lines (Fig. 1) include:

- Calculating from the geometry or distributed constants of the line.
- Measuring open and short-circuited line impedances.
- Measuring a shorted eighth-wavelength line section.

Traditional methods have practical disadvantages

All three approaches have practical disadvantages that limit accuracy, convenience or both.^{1,2,3} In the first method, the constants must be found over the frequency range of interest—not an easy task, since distributed resistance, capacitance and inductance are all frequency sensitive to some degree. Also, calculating the impedance from line-material properties and cable geometry is tedious, unless simplifying assumptions are made.

The open and short-circuit method is the most widely used, but is accurate only for short lengths of low-loss sections. Furthermore, it's unusable for lengths near quarter-wave multiples, because the extreme impedance values obtained lead to poor accuracy. And when lengths are very near the critical quarter-wave multiples, the high impedance values are usually outside the measurement range of most commercial bridges.

Finally, only the magnitude of Z_0 is measured directly with the shorted eighth-wavelength method. And not only is the eighth-wavelength method limited to very low-loss lines, but also the length must be determined precisely.

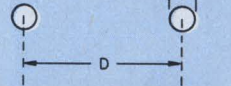
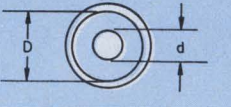


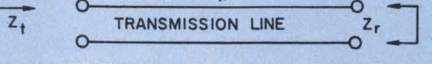
Except for the calculation method, these traditional methods assume low-loss lines. However, a

James E. McKay, Project Engineer, WSB Radio, 1601 W. Peachtree St. NE, Atlanta, GA 30309.

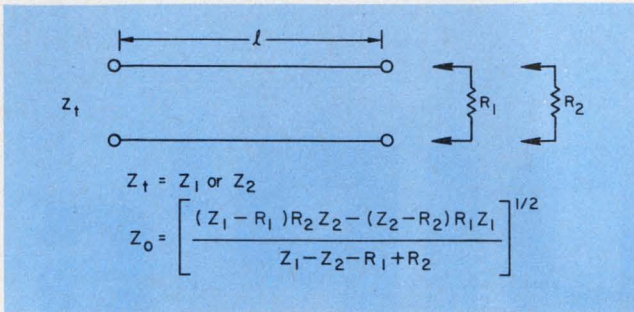
Traditional ways of determining Z_0

Calculations from line geometry

REPRESENTATIVE EXAMPLES

LINE GEOMETRY	CHARACTERISTIC IMPEDANCE
 <p>OPEN TWO-WIRE LINE IN AIR</p>	$Z_0 = 120 \cosh^{-1} \frac{D}{d}$ $\approx 276 \log_{10} \frac{2D}{d}$
 <p>SINGLE COAXIAL LINE</p>	$Z_0 = \frac{138}{\sqrt{\epsilon}} \log_{10} \frac{D}{d}$ <p>ϵ = dielectric constant = 1 in air</p>
 <p>BALANCED SHIELDED LINE</p>	<p>For $D \gg d, h \gg d$,</p> $Z_0 = \frac{276}{\sqrt{\epsilon}} \log_{10} \left[2v \frac{1 - \sigma^2}{1 + \sigma^2} \right]$ <p>$v = \frac{h}{d}$ $\sigma = \frac{h}{D}$</p>
 <p>ECCENTRIC LINE</p>	<p>For $d \ll D$,</p> $Z_0 = \frac{138}{\sqrt{\epsilon}} \log_{10} \left[\frac{D}{d} \left[1 - \left(\frac{2c}{D} \right)^2 \right] \right]$ <p>For $c/D \ll 1$ this is the Z_0 of coaxial diminished by approximately</p> $\frac{240}{\sqrt{\epsilon}} \left(\frac{c}{D} \right)^2 \text{ ohms}$
<p>OPEN AND SHORT-CIRCUIT METHOD</p>  <p>MAKE TWO MEASUREMENTS — $Z_i = Z_{oc}$ WHEN $Z_r = 0$ AND $Z_i = Z_{sc}$ WHEN $Z_r = \infty$</p> $Z_0 = \sqrt{Z_{sc} Z_{oc}}$ $Z_{oc} \text{ (open circuit)} = Z_0 \coth \gamma l$ $Z_{sc} \text{ (short circuit)} = Z_0 \tanh \gamma l$	
<p>SHORTED 1/8-WAVELENGTH LINE</p> $ Z_i = Z_0 $ $l = \lambda/8$	

1. Traditional methods of determining a line's characteristic impedance usually require assumptions not always true in practice, especially for long lossy lines operating at audio frequencies.



2. Using two known load impedances, R_1 and R_2 , to produce easily measured line input impedances, overcomes most of the shortcomings of the traditional methods for determining the Z_0 of a line.

low-loss condition can't be assumed for low frequencies as in many telephone voice and data lines.

Several special techniques are also used, including the use of slotted lines to compare Z_0 with a standard, time-domain reflectometry⁴ and the complicated Chipman method² of resonance-curve plotting. These methods are generally limited to microwave frequencies and require that line losses be negligible.

New method needs two measurements

Using two different known load impedances avoids many of the previously mentioned limitations (Fig. 2). The new method applies to both audio and rf lines of any length, and no assumption of negligible loss is required. The method uses the general-transmission line equation,

$$Z = Z_0 \frac{R + Z_0 \tanh \gamma \ell}{Z_0 + R \tanh \gamma \ell}, \quad (1)$$

where

- Z_0 = characteristic impedance
- R = load impedance
- γ = propagation constant
- ℓ = line length
- Z = impedance at a distance ℓ from the load

Solving Eq. 1 for $\tanh \gamma \ell$ yields

$$\tanh \gamma \ell = \frac{Z_0 (Z - R)}{Z^2_0 - RZ} \quad (2)$$

Two measurements are made at the frequency of interest. The first is a measurement of the line impedance, Z_1 , with a known terminating impedance, R_1 . The second measures an impedance, Z_2 , with another known load impedance, R_2 . Impedances or, preferably, resistances R_1 and R_2 are chosen to yield readily measurable values of Z_1 and Z_2 ; otherwise, they are arbitrary.

Note that γ depends entirely on the line constants, and ℓ is a fixed length, hence $\tanh \gamma \ell$ is the same for both measurements. Writing Eq. 2 for each measurement and equating them results in

$$\tanh \gamma \ell = \frac{Z_0 (Z_1 - R_1)}{Z^2_0 - R_1 Z_1} = \frac{Z_0 (Z_2 - R_2)}{Z^2_0 - R_2 Z_2}. \quad (3)$$

Solving for Z_0 yields

$$Z_0 = \left[\frac{(Z_1 - R_1) R_2 Z_2 - (Z_2 - R_2) R_1 Z_1}{Z_1 - Z_2 - R_1 + R_2} \right]^{1/2}. \quad (4)$$

The R_1 and R_2 quantities on the right side of Eq. 4 are selected for easy measurement. Note that Z_0 is independent of line length or losses. The error sources in Eq. 4 involve the normal measurement tolerances, not theory or assumptions.

If terminating impedances R_1 and R_2 are chosen to be pure resistances, the measured impedances Z_1 and Z_2 are, in general, complex; therefore, Eq. 4 can yield complex values for Z_0 . This result is expected for some lossy lines, and all practical lines at low frequencies.

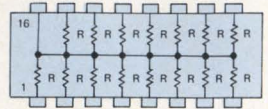
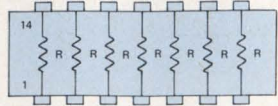
In the special cases of half-wave, low-loss lines or extremely short sections, be particularly careful when selecting the load impedances, R_1 and R_2 . They should be selected to best resolve the differences, $(Z_1 - R_1)$ and $(Z_2 - R_2)$, between the measured and load impedances. ■■

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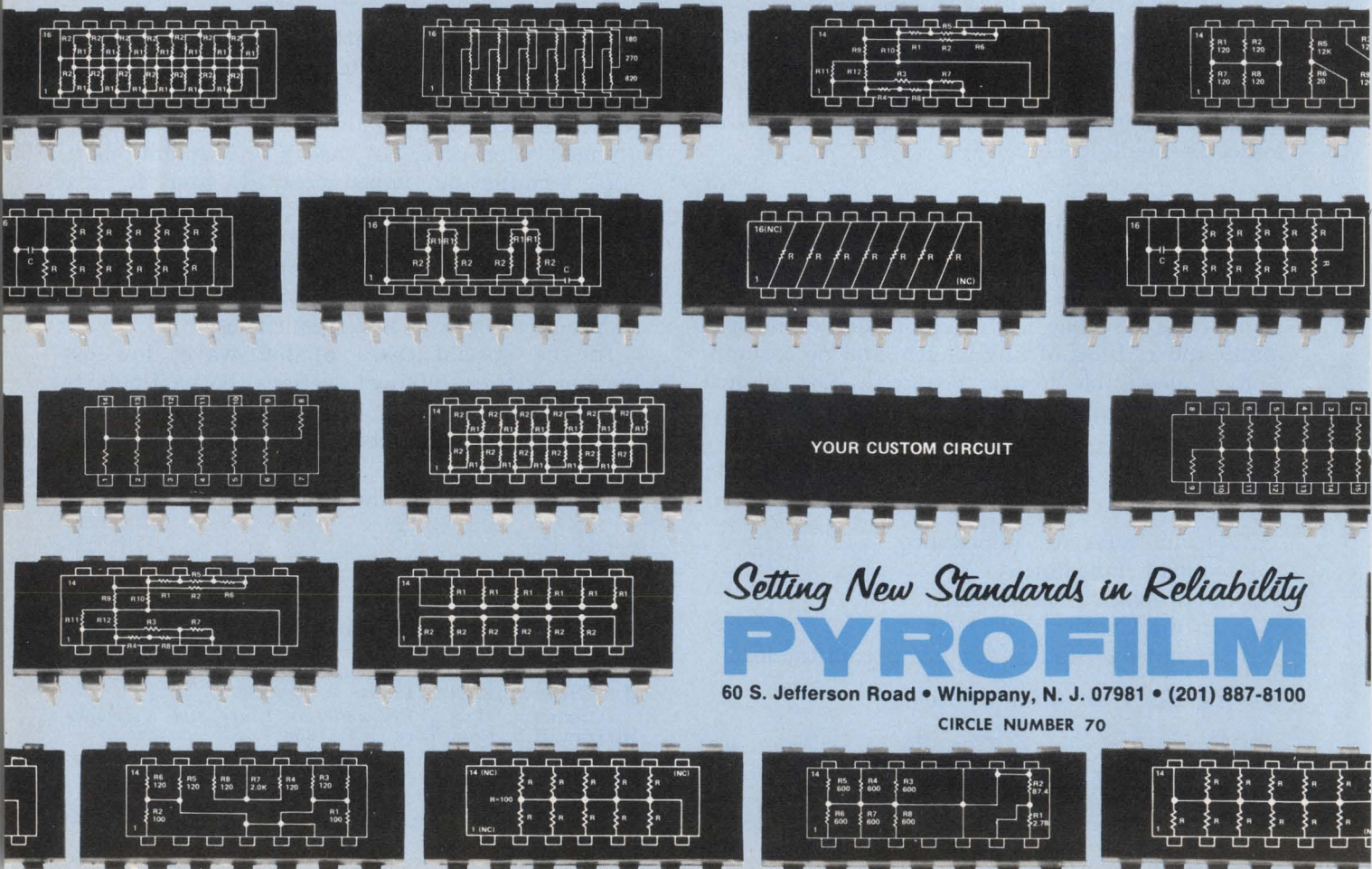


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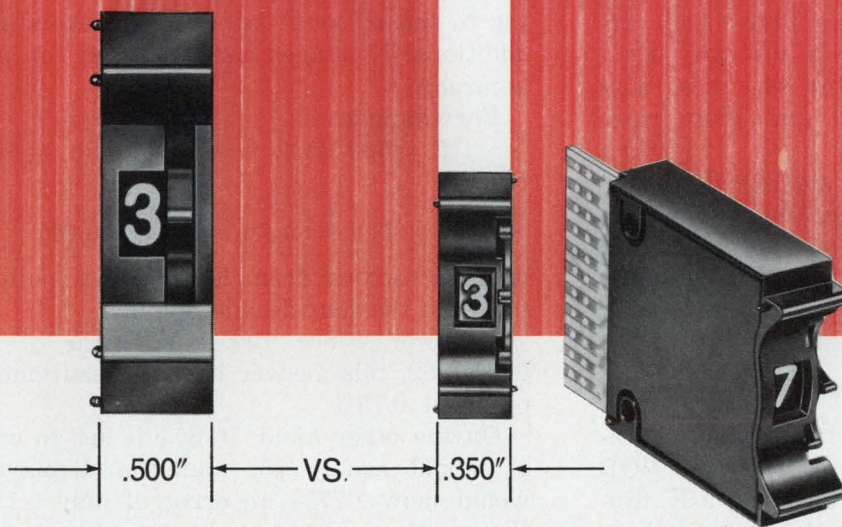
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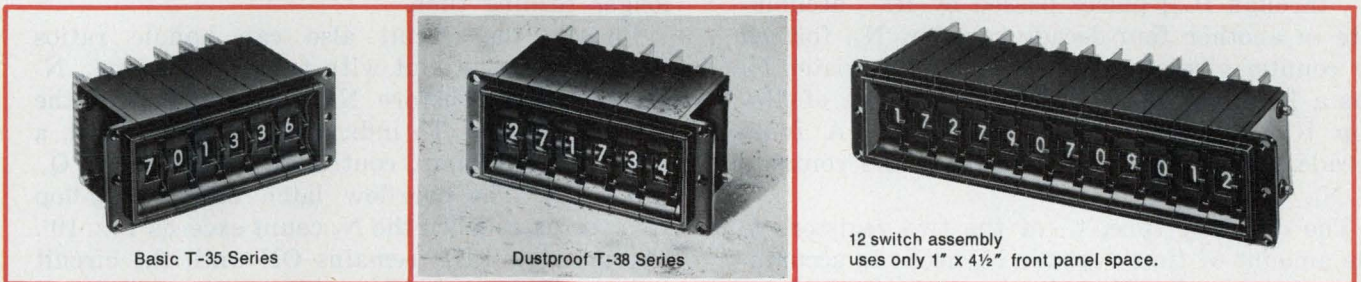
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Measure pulse-rate ratios automatically to four-place accuracy. Simple circuit handles steady or random signal rates with ratios greater or less than unity.

To determine the ratio of two signal pulse-rates, you don't need to separately record the individual rates and obtain the ratios with manual arithmetic. A simple counter-circuit arrangement (Fig. 1) provides a virtually real-time, 4-digit display of the ratio. The rates may be either regular or random, and their ratio greater or less than unity.

For random-pulse rates, the statistical accuracy—and for regular pulse rates, the absolute accuracy—depends on how long you are willing to wait for the result. The circuit works in the same way for random and regular signals.

Gated counters determine the ratio

In the simplified arrangement of Fig. 1, the input-pulse rates, f_1 and f_2 , enter the two NOR gates, IC_{1-1} and IC_{1-2} , respectively. A J-K flip-flop latch circuit, IC_{2-1} , controls the state of these gates.

Pulses passed by IC_{1-1} accumulate in a four-decade register, N_1 , formed by counter circuits IC_3 through IC_6 ; pulses passed by IC_{1-2} accumulate in another four-decade register, N_2 , formed by counter circuits IC_7 through IC_{10} . Register N_2 has a 1×10^4 overflow circuit consisting of flip-flop IC_{2-2} , transistor Q_1 and a LED. A four-decade, numerical readout displays the contents of N_2 .

The counting time, t_1 , of the two registers is the amount of time register N_1 needs to accumulate a count selected with switch S_{1-1} . When N_1 accumulates the selected count, latch IC_{2-1} operates and closes gates IC_{1-1} and IC_{1-2} . The circuit then holds and displays the contents of N_2 until the circuit is manually reset with S_2 .

Clearly the ratio of the pulse rates f_1 and f_2 are related to the counts, n_1 and n_2 , accumulated in the corresponding registers, N_1 and N_2 , by the following equation:

$$f_2/f_1 = n_2/n_1.$$

The n_1 counts are the powers of ten— 10 , 10^2 ,

10^3 or 10^4 —for easy interpretation of the displayed ratio. A switch section, S_{1-2} , automatically illuminates the proper decimal point corresponding to the n_1 count selected. As explained later, additional N_1 stages can be added for increased accuracy.

For example, if

$$f_1 = 580 \text{ Hz}, f_2 = 45 \text{ Hz}, \text{ and } n_1 = 10^3,$$

then

$$f_2/f_1 = n_2/n_1 = \frac{77}{10^3} = 0.077$$

with the second from left decimal point illuminated on the four-decade display.

However, since the true ratio of f_2/f_1 is 0.0775862, this answer has a measurement error of about 0.75%.

On the other hand, if S_{1-1} is set to count 10^4 , n_2 would equal 775, and the displayed ratio would show .0775—an error of only 0.11%. But the reading time for this greater accuracy is 17.24 s vs 1.724 s for the first example. If n_1 could be greater than 10^4 , then even greater accuracy could be attained, but, of course, at an even longer reading time.

Clearly, the circuit also can handle ratios greater than one. But with f_2 greater than f_1 , N_2 might overflow before N_1 has accumulated the selected number. To indicate such a condition, a LED overflow lamp, controlled by transistor Q_1 , turns ON. The overflow latch circuit, flip-flop IC_{2-2} , actuates when the N_2 count exceeds 1×10^4 . The overflow LED remains ON until the circuit is manually reset by S_2 .

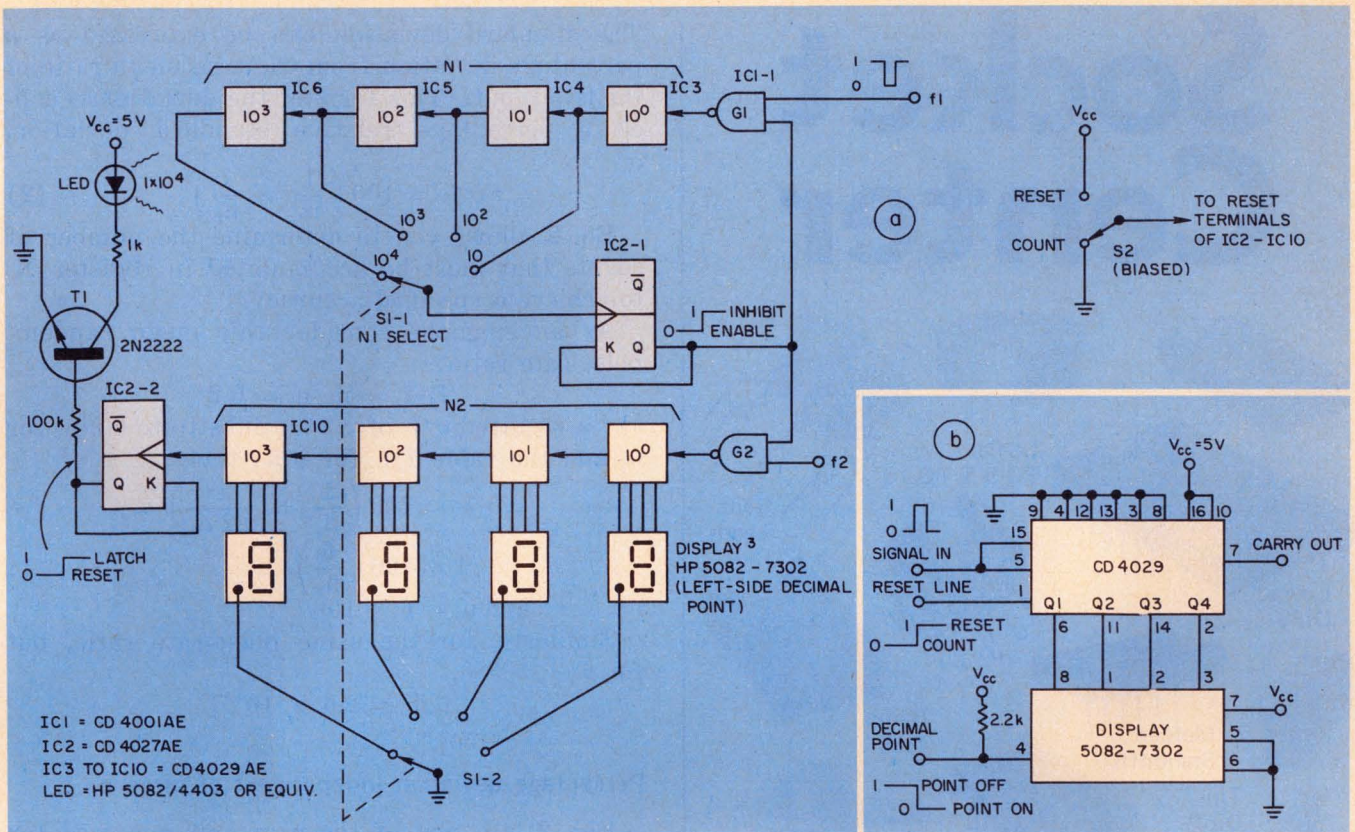
Determining errors of random-pulse ratios

When the input pulse rates are random and have a Gaussian distribution, the ratio-measuring procedure—whether f_1 is greater or less than f_2 —is the same as for the regularly spaced pulse inputs just described. However, now the accuracy of the measured ratios becomes a statistical quantity.¹

The standard deviation, σ , of the measured ratio of random inputs is given by the expression:²

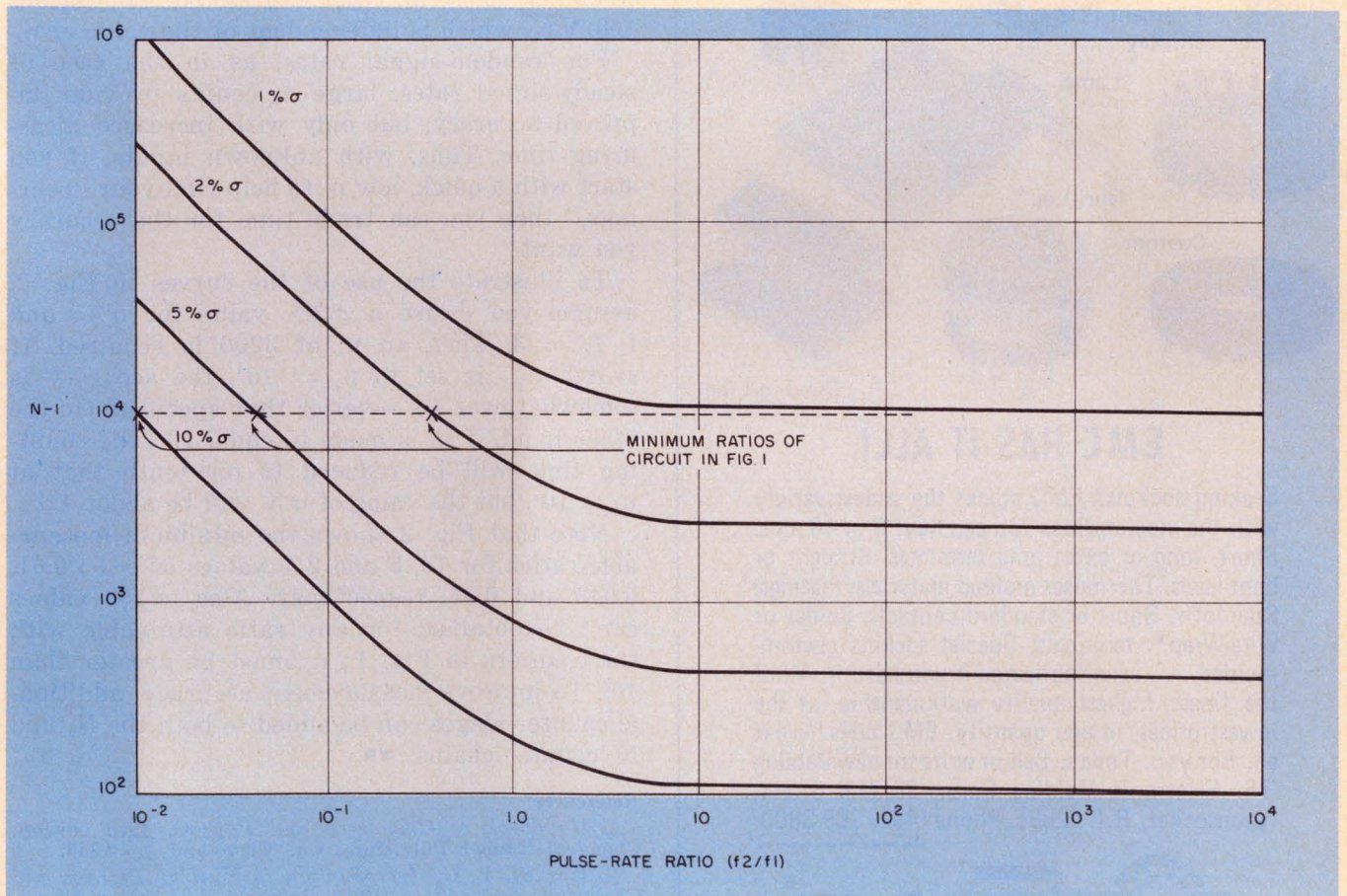
$$\pm \sigma = \frac{n_2}{n_1} \left(\frac{1}{n_1} + \frac{1}{n_2} \right)^{1/2} \quad (1)$$

H.A. Cole, Chartered Engineer, Atomic Energy Research Establishment, Harwell, Oxfordshire, England.



1. The decimal point of the four-place readout for the rate-ratio circuit (a) is automatically established by the

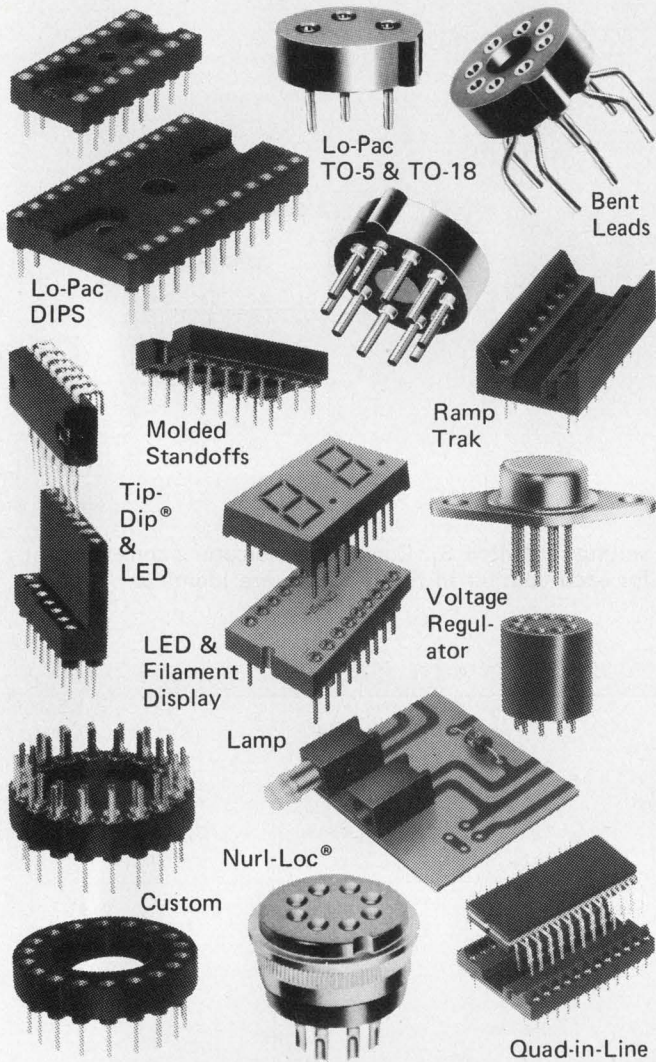
setting of switch S_1 . Counter-to-indicator connections (b) for each counter in the N_2 chain are identical.



2. For random pulse-rate signals, the count of chain N_1 , as set by switch S_1 , determines the expected pre-

cision of the ratio measured in terms of a percentage relative standard deviation, σ %.

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Interconnection Specialists

CIRCLE NUMBER 72

The standard deviation can be expressed as a percentage deviation from the true mean ratio of the two inputs. This form of the deviation is called a percentage relative standard deviation, $\sigma\%$:

$$\pm\sigma\% = 100 \left(\frac{1}{n_1} + \frac{1}{n_2} \right)^{1/2} \quad (2)$$

Eq. 2 allows you to determine the number of counts that must be accumulated in register N_1 to achieve a specified accuracy.

As an example, consider this mean random-pulse-rate ratio:

$$f_2/f_1 = n_2/n_1 = 0.2$$

and a required $\sigma\%$ of $\pm 1\%$. Substitute $0.2 n_1$ for n_2 and the value 1% for $\sigma\%$, then

$$\pm\sigma\% = 100 \left(\frac{1}{n_1} + \frac{1}{0.2 n_1} \right)^{1/2},$$

$$1 = 100 \left(\frac{6}{n_1} \right)^{1/2},$$

$$\text{and } n_1 = 6 \times 10^4.$$

Similarly, for the same pulse-rate ratio, but for $\sigma\% = 5\%$,

$$n_1 = 2.4 \times 10^3.$$

Percentage deviation independent of large n_2

Fig. 2 is a plot of the n_1 counts required for given percentage relative standard deviations, $\sigma\%$, over a range of random input ratios from 10^{-2} to 10^4 . It is interesting to note that in Eq. 2, when $n_2 \gg n_1$, the expression approaches $100/\sqrt{n_1}$, which is independent of the value of n_2 .

For random-signal rates, as in the case of steady-signal rates, large n_2 counts provide improved accuracy, but only with increased measuring time. Thus, with unknown inputs, if you start with a quick, low n_1 to help find your "bearings," then you can trade time for the accuracy you want.

To illustrate the use of the curves in Fig. 2, assume you desire a $\pm 2\%$ value for $\sigma\%$, and $f_2/f_1 = 3$. Then an n_1 of 3200 is required. If switch S_{1-1} is set to $n_1 = 10^4$, the accuracy is somewhat over 1% —better than specified. On the other hand, if n_1 is made to equal 10^3 , the counting time will be reduced to one-tenth that at $n_1 = 10^4$, but the value of $\sigma\%$ will be about 4% .

Note that Fig. 2 shows the minimum measurable ratios for 10, 5 and 2% values of $\sigma\%$: 0.01, 0.043 and 0.35, respectively. Also, $\pm 1\%$ values can't be obtained for any ratio attainable with the counters in Fig. 1; n_1 must be greater than 10^4 . To improve measurement accuracy, additional counter stages can be added to both the N_1 and N_2 counter chains. ■■

References

1. *Handbook of Chemistry and Physics*, 49th edition, Chemical Rubber Publishing Co., Cleveland, p. A253.
2. Harvey, B. G., *Introduction to Nuclear Physics and Chemistry*, 2nd edition, 1969, Prentice-Hall International, Englewood Cliffs, NJ, pp. 358-361.
3. *Hewlett-Packard Application Note 934* (5082-7300 series), Palo Alto, CA.

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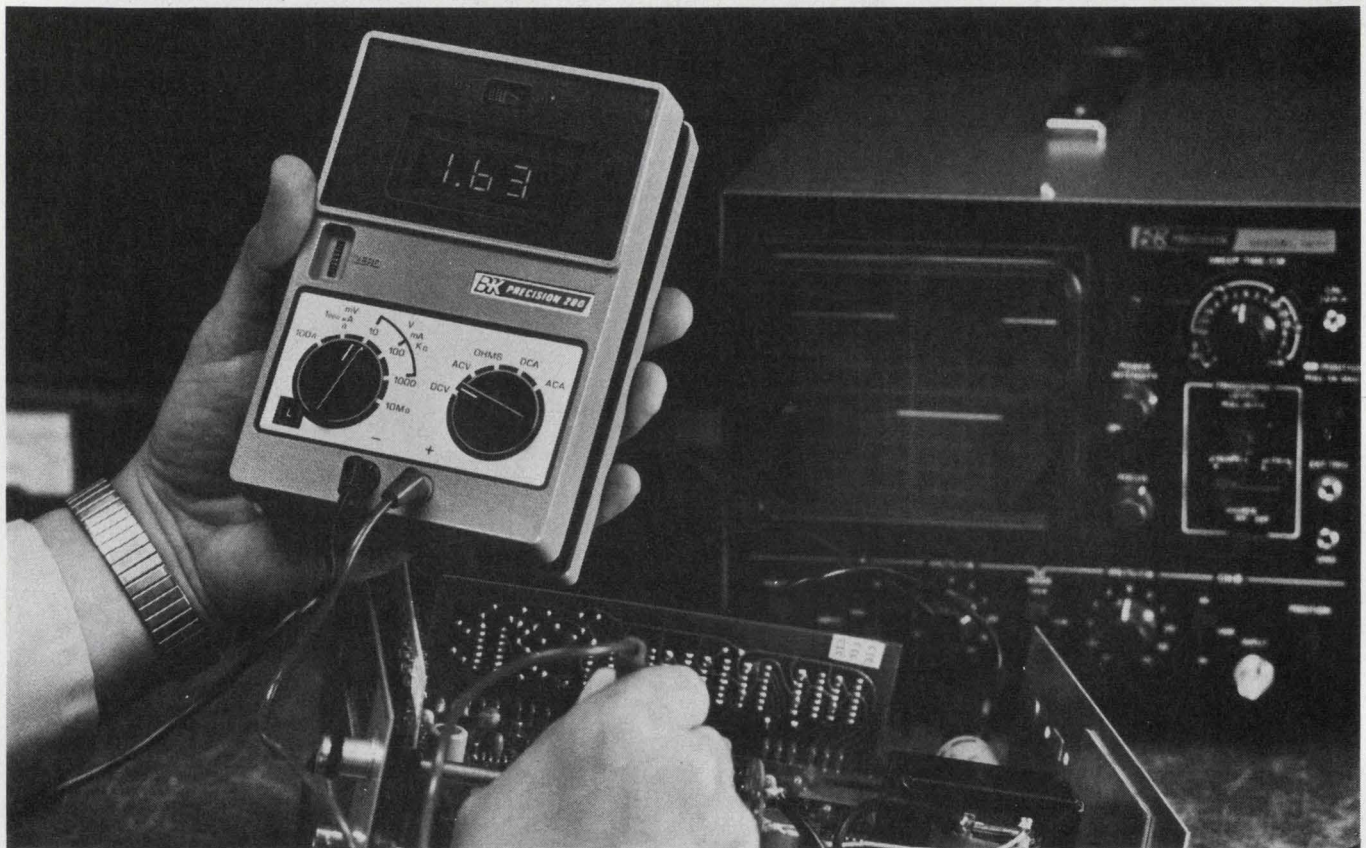


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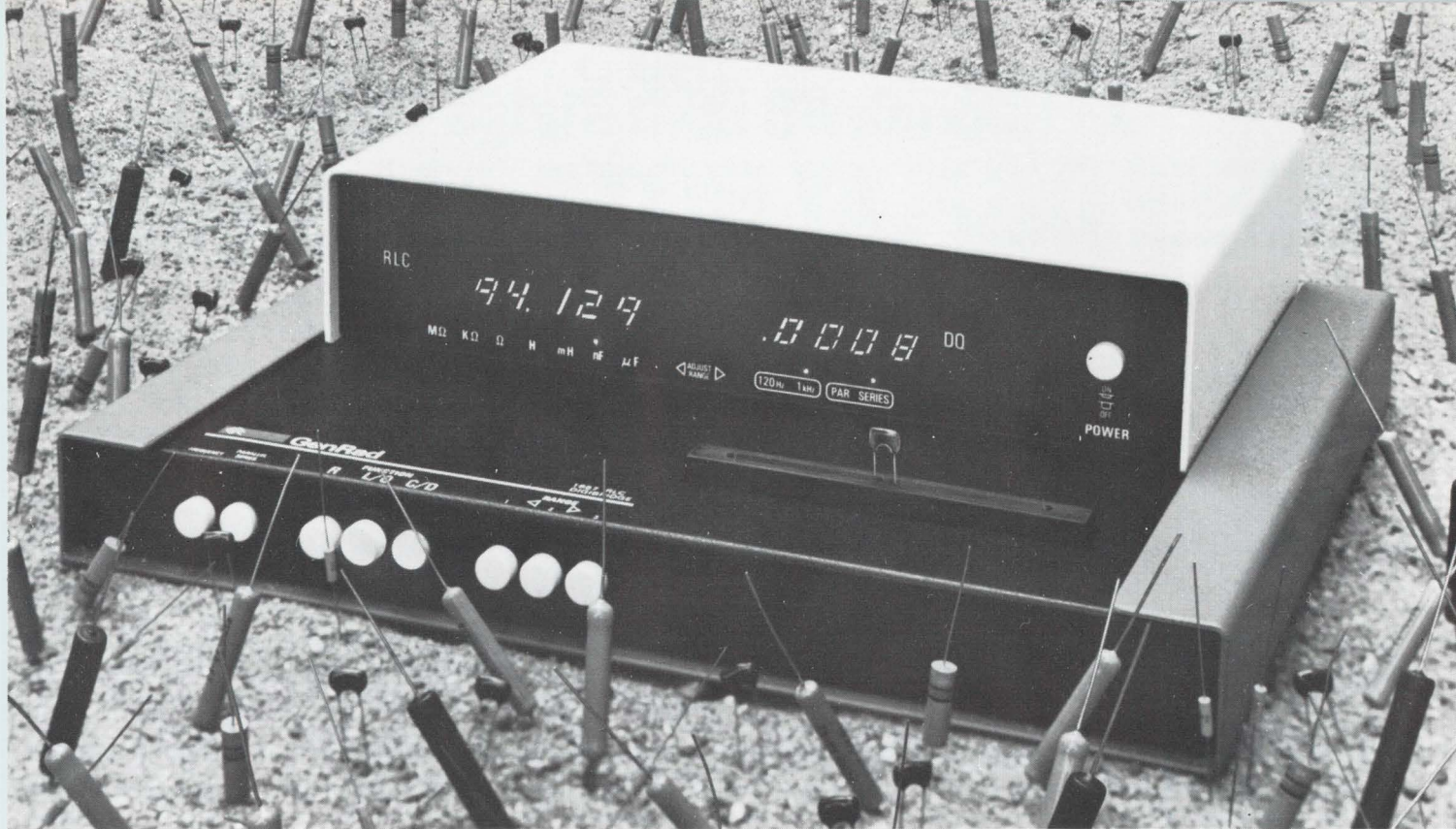
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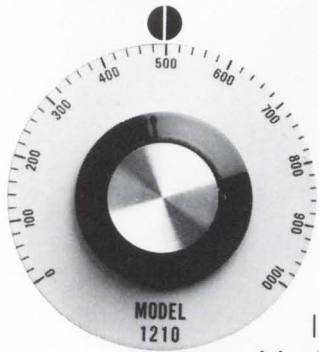
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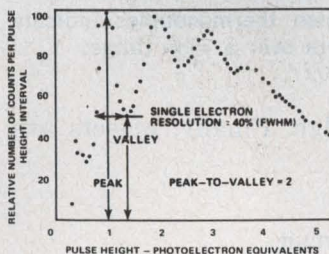
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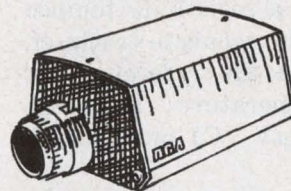
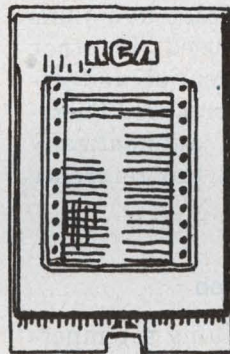
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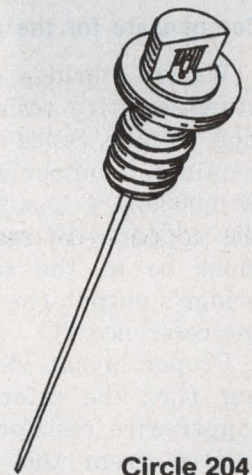
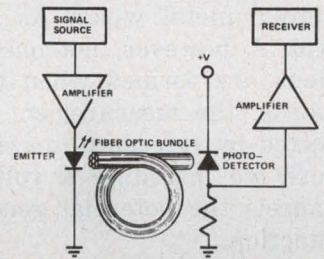
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RCA

Don't sweat with thermocouple thermometers.

CMOS analog and digital devices make it easy to design an inexpensive thermometer.

Thermocouples (TCs) are reliable and low-cost temperature transducers, but they have two major disadvantages:

- Low output (millivolts).
- Reference-junction drift.

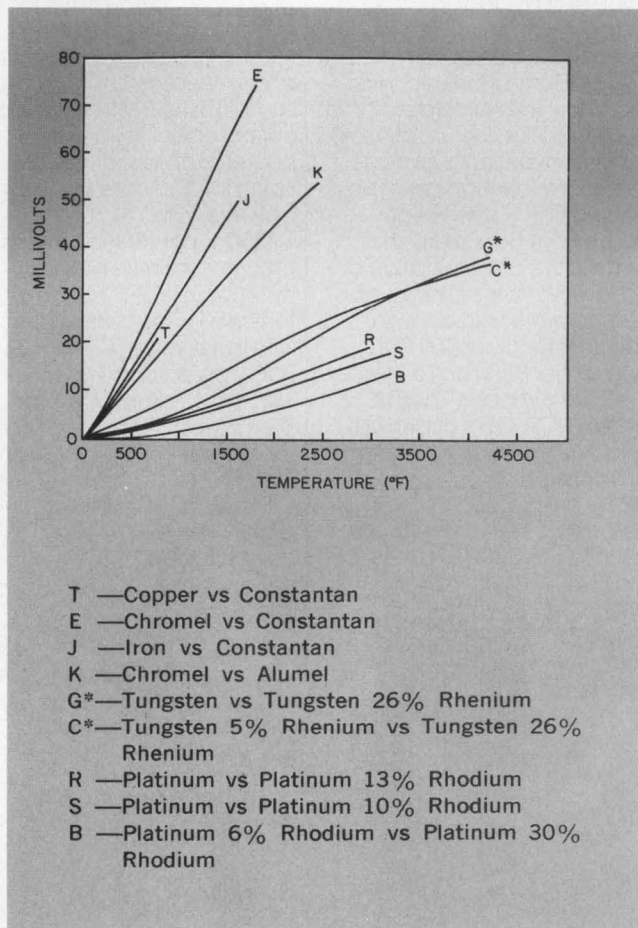
The problems can be avoided by using inexpensive linear-CMOS-chips as low-level signal conditioners, and a bucking voltage for reference-junction compensation. The complex electronics and temperature control of past designs are not needed. Thus TCs are now attractive transducers, even for temperatures as low as 0 to 100 C (see Fig. 1).

Thermocouple probes, as we know, are made by simply welding together the ends of two dissimilar-metal wires. As shown schematically in Fig. 2, however, not one but at least two junctions are formed when a TC is used. In other words, the measurement is differential and affected by reference-junction temperature. Therefore we introduce a voltage that automatically cancels the potential generated at the reference junction.

Compensate for the reference junction

We use a bridge (Fig. 3) containing a temperature-sensitive resistor to generate a compensation voltage. Since only a small output voltage is required, a copper wire with a resistivity tempo of $0.00393/^\circ\text{C}$ is sufficient. For accurate tracking, the copper-wire resistor and the reference TC must be at the same temperature; also, the bridge's output (in terms of $\mu\text{V}/^\circ\text{C}$) must match the reference TC.

Proper layout yields good temperature tracking (i.e., the reference TC is placed near the copper-wire resistor, and both are thermally insulated from the ambient.) The temperature sensitivity of the bridge is then matched to the reference TC by R_{adj} (Fig. 3), which controls the



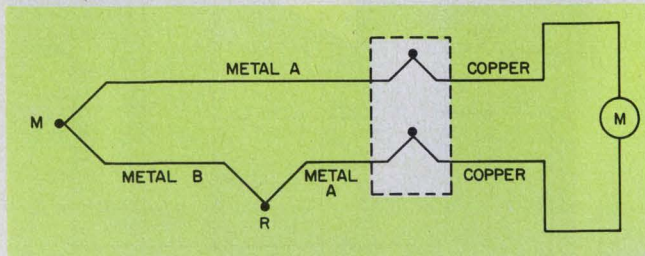
1. The sensitivities of common thermocouples indicate that the thermometer can work over a wide range.

current through the bridge. Finally, offsets are adjusted using R_{offset} .

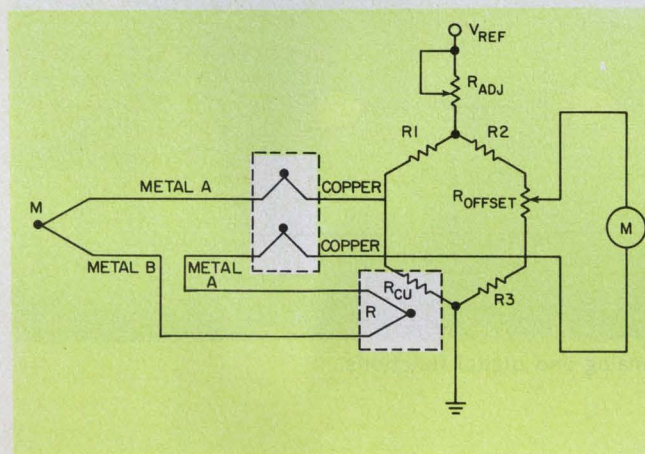
Design a compensation circuit

Let's analyze the circuit for automatic reference TC compensation (Fig. 3). For illustration, we will use a Chromel/Alumel couple. The TC's sensitivity at room temperature (S_{TC}) is $39 \mu\text{V}/^\circ\text{C}$. This must be matched by the voltage variation across the copper-wire resistor (R_{Cu}) as a function of temperature. If a $15\text{-}\Omega$ copper-wire resistor is selected, the current through it (I_{Cu}) is

Dr. S. Ben-Yaakov, Head, and Y. Sanandagi, R & D Technician, Institute of Electronics, Ben-Gurion University of the Negev, Beer-Sheva, Israel.



2. Thermocouple temperature measuring involves a measuring-junction M, and a reference-junction R. If the junctions with the copper wire are kept at the same temperature, their potentials cancel.



3. The bridge, using a copper-wire resistor (R_{Cu}), produces a temperature dependent output voltage for reference-junction compensation. The voltage is made equal and of opposite polarity to the reference junction.

$$I_{Cu} = \frac{S_{TC}}{R_{Cu} \times S_{Cu}}$$

where S_{Cu} is the temperature coefficient of resistivity of copper, which is equal to $0.00393 / ^\circ C$. The required current is

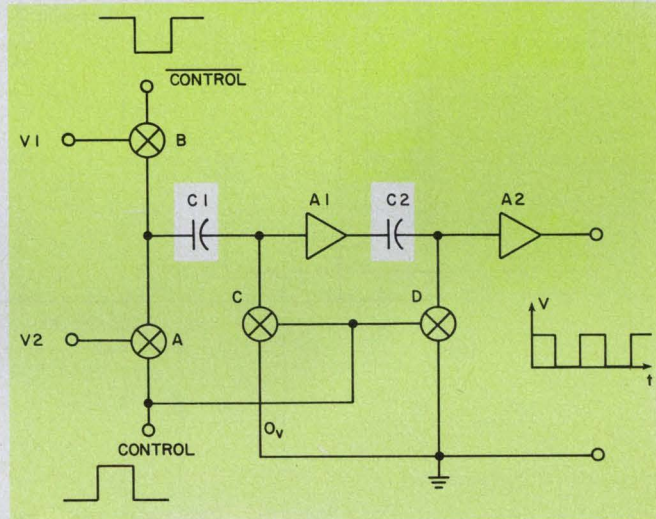
$$I_{Cu} = \frac{40 \times 10^{-6}}{3.93 \times 10^{-3} \times 15} = 0.678 \text{ mA}$$

Assuming a symmetrical bridge, the current through R_{adj} (I_{adj}) should be

$$I_{adj} = 2 \times I_{Cu} = 1.36 \text{ mA}$$

and the expression for R_{adj} :

$$R_{adj} = \frac{V_{ref} - I_{Cu} (R_1 + R_{Cu})}{I_{adj}}$$



4. Automatic-offset-correcting dc amplifier's output is proportional to the difference of V_1 and V_2 . The analog switches conduct when their control line is high.

Selecting R_1 to be $5 \text{ k}\Omega$ and assuming a reference voltage (V_{ref}) of 5 V ,

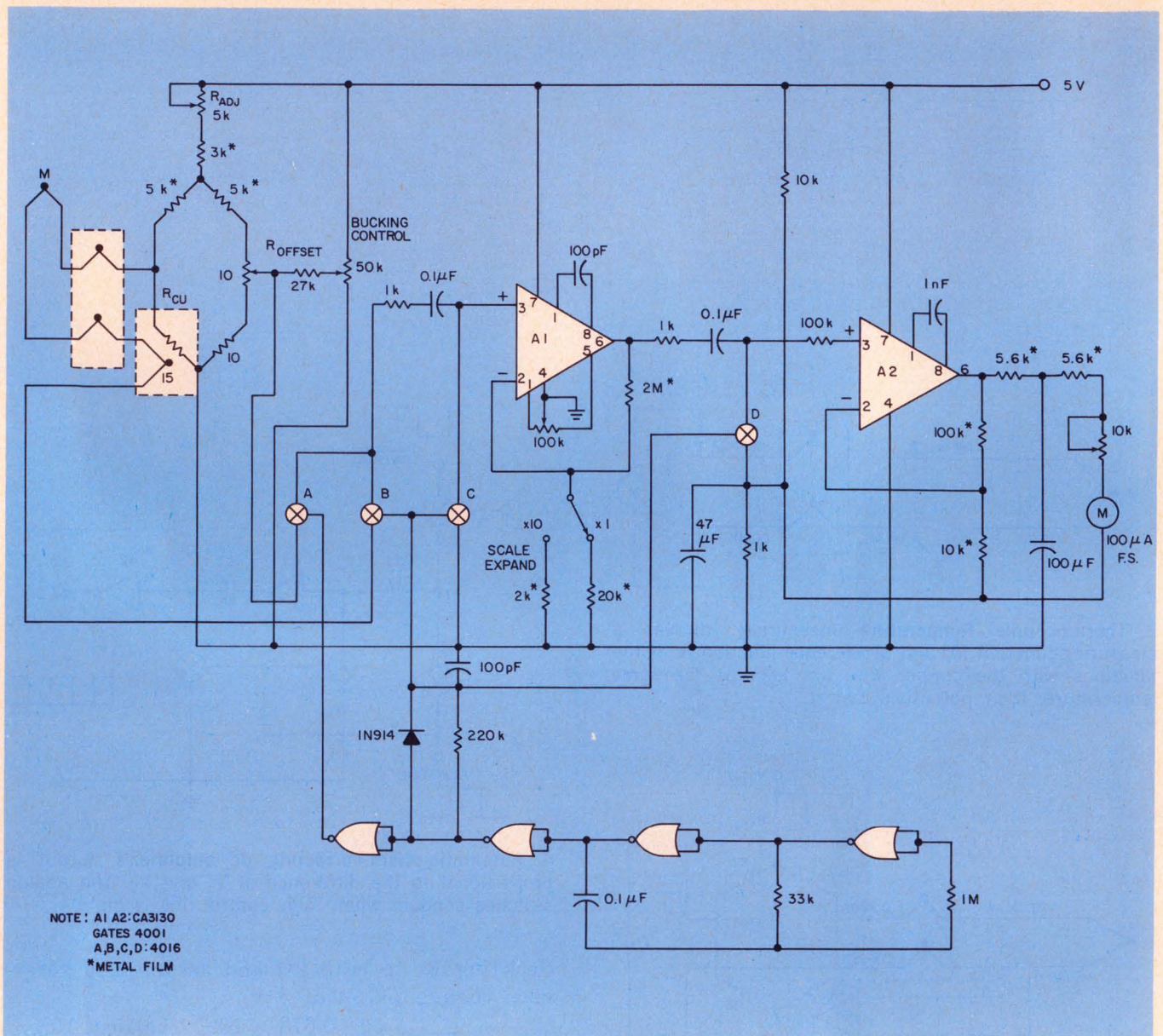
$$R_{adj} = \frac{5 - 0.678 \times 10^{-3} \times 5.015 \times 10^{-3}}{1.36 \times 10^{-3}}$$

$$R_{adj} = 1.18 \text{ k}\Omega.$$

Eliminate dc-amplifier offset

A major problem in the design of TC thermometers stems from the extremely low dc levels involved. Offsets in dc amps tend to mask the signal. We overcome this problem, while using standard CMOS op amps, with an automatic offset-correction circuit. The major components of the circuit are shown in block form (Fig. 4). Operational amplifiers, analog switches and series capacitors are used.

The switches are driven by a square-wave (see Fig. 4). The switches conduct when the drive is high. During the offset-adjustment period, switches A, C, and D conduct. C_1 charges to V_1 , and C_2 charges to the offset-dc error at the output of A_1 . The charge on C_1 and C_2 is maintained during the temperature-measuring half-cycle. The output voltage of A_2 is therefore proportional to



5. Thermocouple thermometer uses all CMOS chips for both analog and digital functions.

$V_1 - V_2$ and is free of the offset voltage at A_1 , which is subtracted out by the voltage across C_2 .

Use CMOS circuits throughout

The design principles presented here are applied in the all-CMOS circuit of Fig. 5. It includes an RC oscillator, analog gates and op amps. The op amps' CMOS input-and-output stages have two useful features:

- *Very low input bias current.* A value of 10 pA is typical. Hence, capacitor discharge (the droop) is negligible during the 5-ms temperature measuring cycle.

- *Ability to operate from a single supply.* The op amps' input-and-output terminals are permitted to reach ground potential. This simplifies the power supply, an important feature in bat-

tery-operated instruments.

With the values shown in Fig. 5, the amplifier has an over-all gain of about 1000 and an offset-voltage drift of less than $0.3 \mu\text{V}/^\circ\text{C}$. Assuming a duty cycle of 50%, the over-all gain to the filtered output is 500. Use of a Chromel/Alumel TC produces a full scale of 400 mV for a 0-to-100-C temperature span. With a proper series resistor, the signal conditioner can drive a 100- μA moving-coil meter.

Two additional features are:

- Expanded-scale capability.
- Variable bucking voltage.

Using these features together, you can buck out a reading, then expand the scale to measure small superimposed temperature fluctuations with a sensitivity greater than 0.1 C. This procedure produces a resolution less than $4 \mu\text{V}$. ■■

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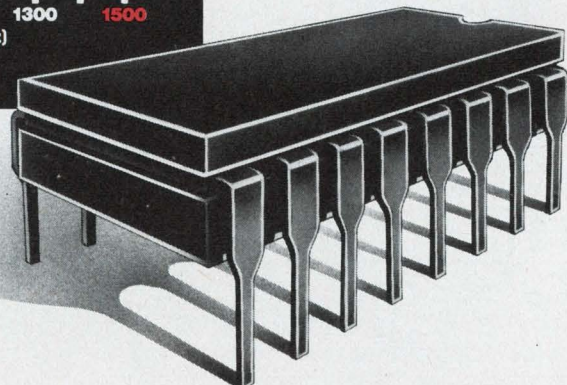
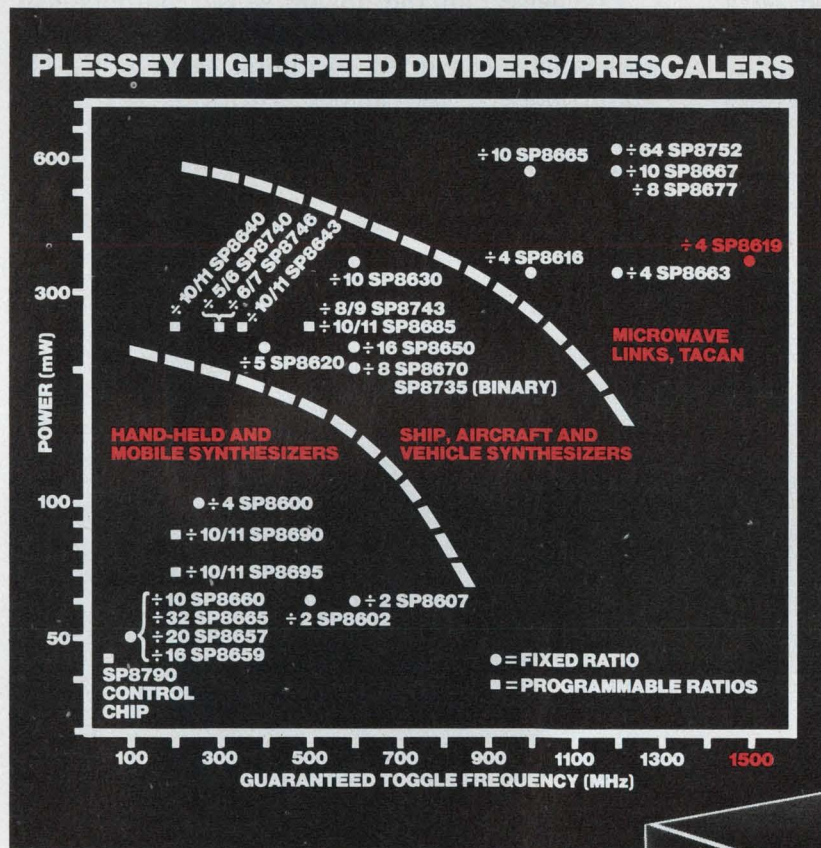
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need not transmit analog signals. Two-chip integrating a/d converters need only two wires for data handling.

Putting together a low-cost data-acquisition system is getting easier all the time, especially when it's based on a microprocessor. By placing the analog half of a two-chip integrating analog-to-digital converter at each monitoring point, you can get the benefits of all-digital communications and still maintain good accuracy.

Potential advantages of a system based on a two-chip a/d converter include:

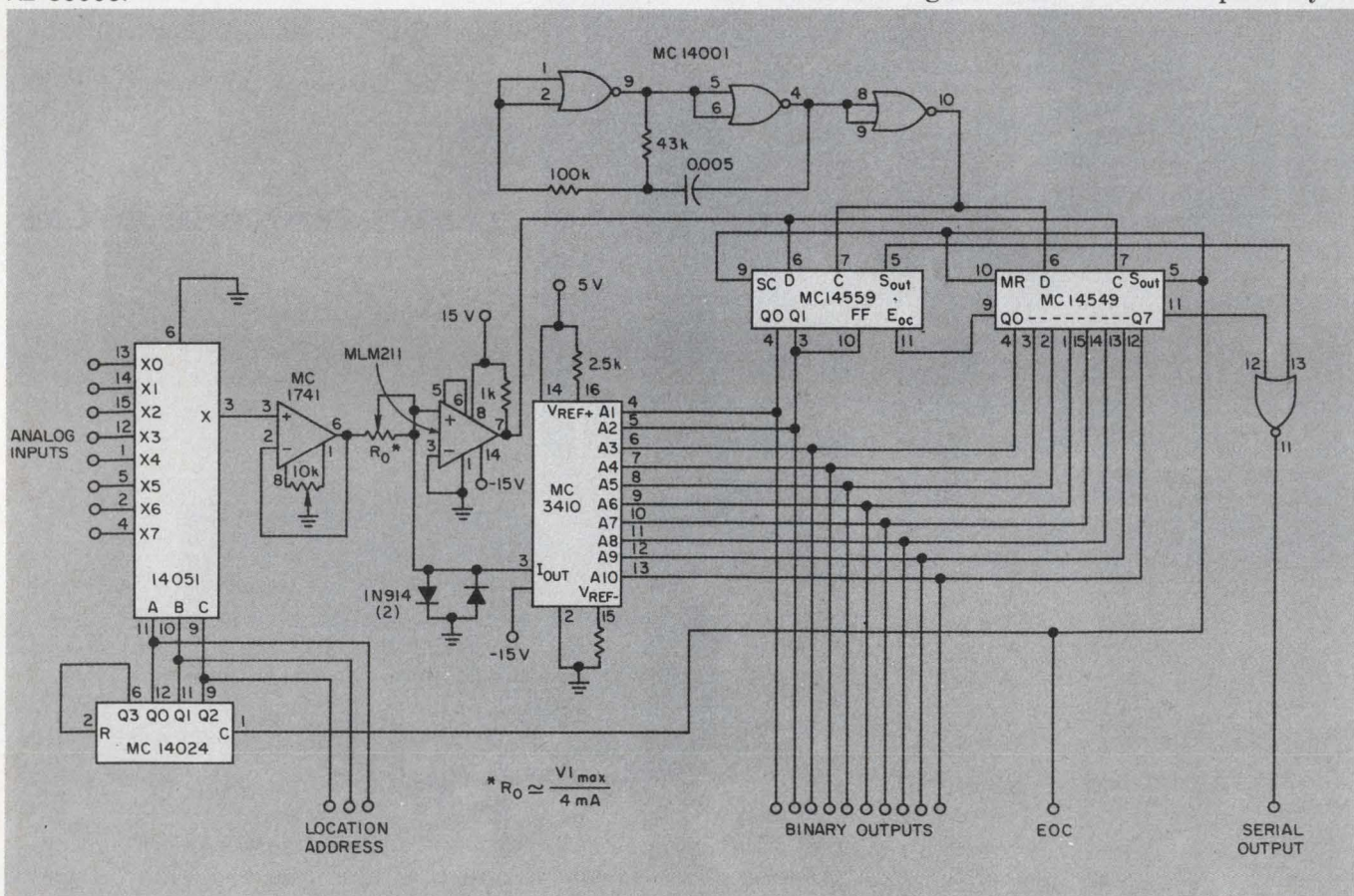
- Accuracy to better than 0.1%.
- Communication and control with only two digital signals.

- Noise immunity of digital signals.
- Multiple remotes can be easily multiplexed.
- Convert-command capability with no extra leads.
- Simple interface to monitors or a processor.
- Small hardware commitment at the remote sites.

Previously, all the analog sensor outputs had to be routed to one central point, multiplexed and sequentially converted to digital form (Fig. 1). Unfortunately, the analog variables are often widely dispersed—and must be transmitted over long cable runs where signal losses and noise pickup can occur.

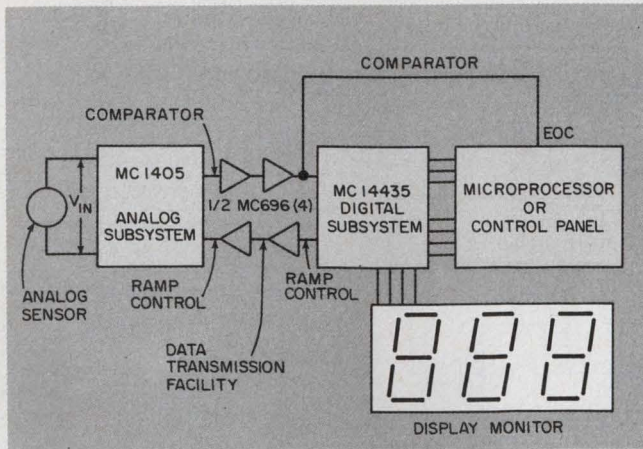
By using an a/d converter at each point and then transmitting the words to a multiplexer you

Steve Kelly, Applications Engineer, Motorola Semiconductor Products Inc., 5005 E. McDowell Rd., Phoenix, AZ 85008.



1. A simple 8-channel data-acquisition system requires that the analog signals from each monitored point be

sent over long cable runs to the multiplexing and conversion circuits.



2. The 1405 analog-converter subsystem permits you to remotely locate a small part of the total data collection system, yet still retain complete control of conversion.

solve the transmission problem, but increase the costs.

A two-chip a/d converter system—the MC-1405/14435, for example—can provide an intermediate solution when up to 3-1/2 digit resolution is needed (Fig. 2). The 1405 analog subsystem and the 14435 digital subsystem communicate through only two digital signal lines—a ramp control and a comparator output. As a result, the analog subsystem can be remotely located from the digital half.

To multiplex the different 1405 subsystems to a single 14435, a central controller must be able to start and stop the conversion process of each 1405 at any time. This is easy enough to do: just bring the ramp control line HIGH and the 1405 comparator output will be LOW. However, in this idle state there are two stringent requirements for the integrating capacitors.

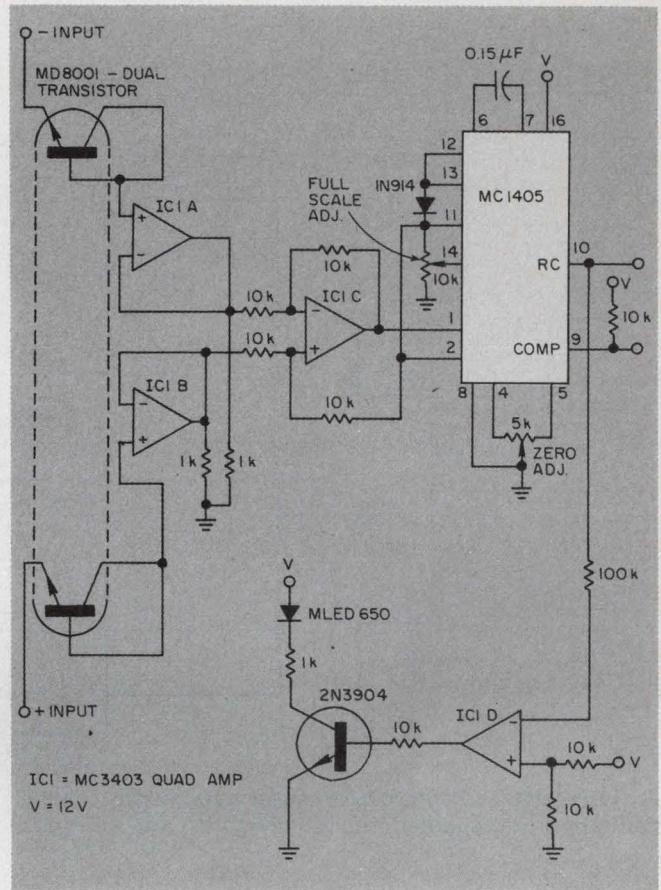
1. The capacitor, during idle conditions, will see reverse dc voltages and so must be nonpolar. The required capacitance is a function of supply voltage, clock frequency and maximum allowed input, and can be calculated from:

$$C_1 = (V_{IN(max)} / 2.7 \text{ k}\Omega) (1000 / [f (V_{CC} - 3.3)])$$

The system clock should be high enough in frequency to allow a convenient value of C_1 . (Frequencies between 100 kHz and 1 MHz are possible.) At a V_{IN} of 1 V, a V_{CC} of 12 V and an $f = 500$ kHz, C_1 is $0.15 \mu\text{F}$.

2. The dielectric absorption of the capacitor must be low if the first conversion after restart is to be accurate. If 0.1% accuracy for the first conversion is required, an expensive polycarbonate capacitor with a value in tenths of a microfarad must be used. You can get away with a lower cost Mylar capacitor if two conversions at each remote site are permitted. At a 500-kHz frequency, each conversion requires about 15 ms.

A typical remote a/d converter station using the 1405 can operate from a single supply, use



3. A typical remote station using the 1405 offers a full differential input and only uses two wires to communicate with the 14435 digital subsystem in the controller.

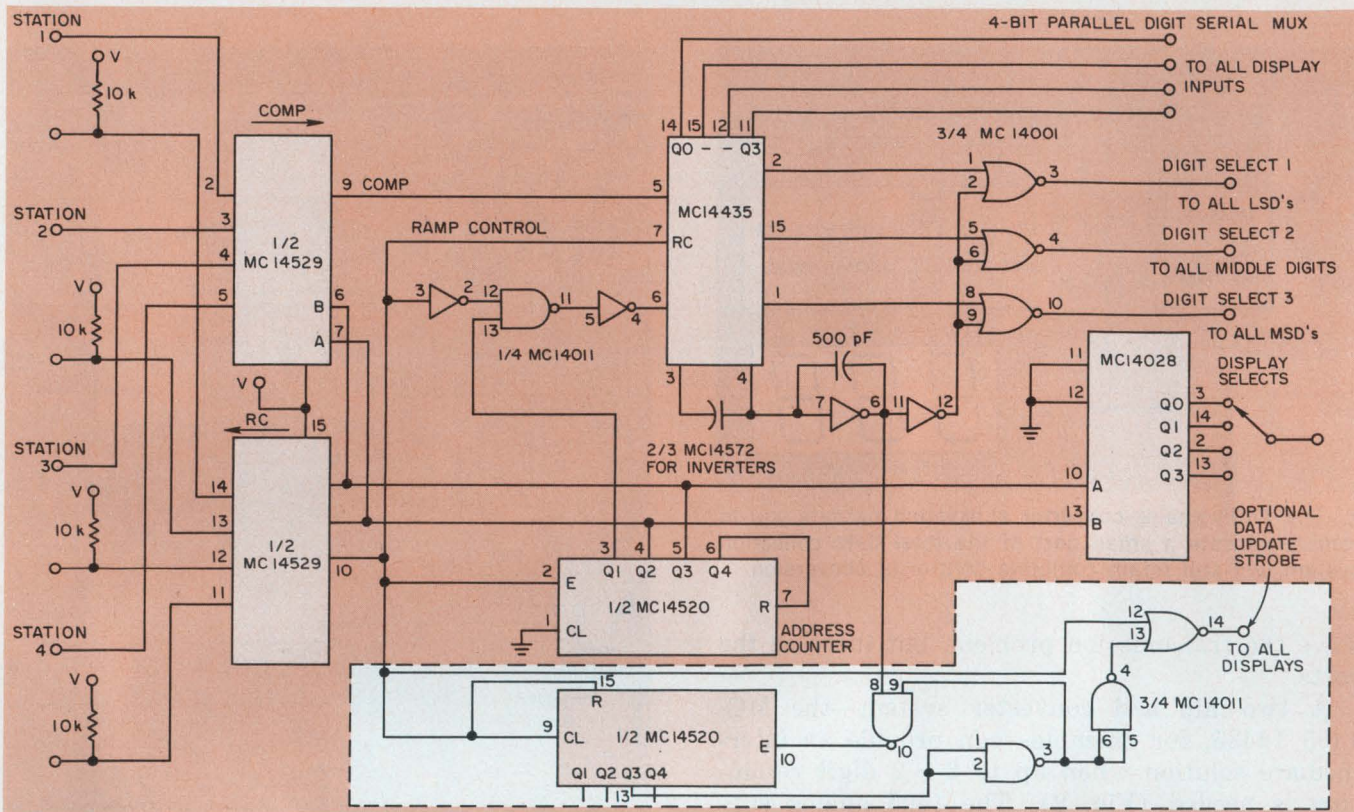
the MC3403 quad op amp as an input buffer, have true differential inputs and have a common-mode input range to zero (Fig. 3).

Multiplexing the 1405 is easy

The circuit shown in Fig. 4 can be used to multiplex four remote stations with a 14435 digital subsystem. By extending the counter chains and multiplexing gates, you can expand the system to 32 channels and provide three updates per second for each channel. The ramp control signal drives half of the 14520 dual binary counter. Outputs Q_2 and Q_3 from the 14520 provide the station scan addresses and commit the 14435 to the station for each conversion.

During the first conversion of each channel the strobe line remains LOW (controlled by Q_1 of the 14520), thus keeping the incorrect 14435 output from reaching a display or processor. The second conversion result gets strobed out since the Q_1 output goes LOW.

When the comparator signal from the remote 1405 goes LOW, it inhibits the 14435 clock. Data get strobed into the 14435 latches and the counters and ramp control are reset. The ramp control change also advances the address counter, which



4. To receive and control the sensor data, a four-channel multiplexer, a counter and some gates are all that's

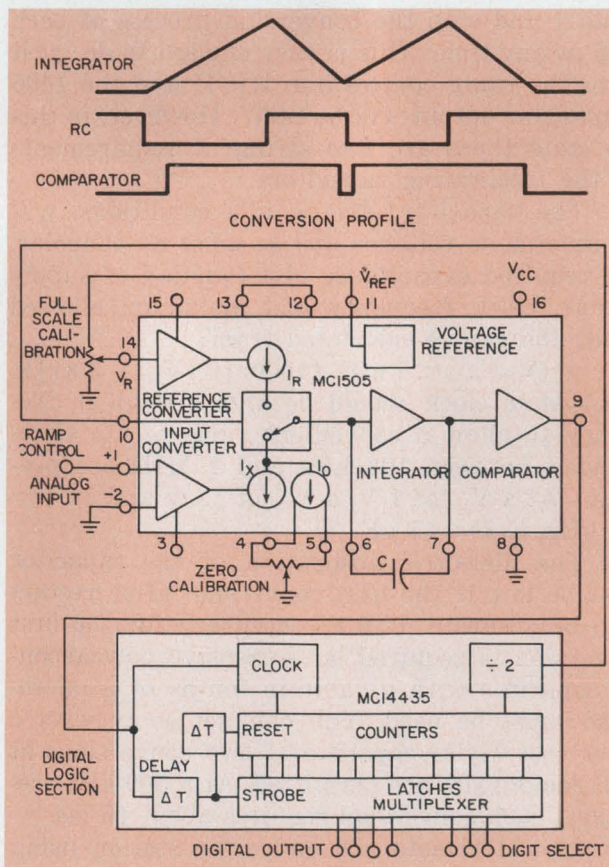
needed. The circuit delivers multiplexed BCD signals that can be fed to a display or to a processor.

Basic operation of the 1405/14435 a/d converter

The MC1405 and 14435 ICs form a dual-slope a/d converter that delivers a 3-1/2 digit BCD output (max. count 1999). The digital subsystem chip (14435) controls the direction of integration in the analog subsystem (1405) through its ramp control output. A logic ZERO initiates a ramp-up operation and a ONE starts the ramp-down function. A comparator output of the 1405 controls the clock of the 14435.

At the start of a conversion cycle, the ramp control and comparator lines are at ZERO. The integrator then ramps upward through the internal comparator threshold, changing the comparator output to ONE, and thus starting the clock in the 14435. The integrator in the 1405 continues to ramp upward until the internal counter of the 14435 reaches a count of 1000, at which point the ramp control line of the 14435 goes HIGH. Now, the integrator starts ramping down, with a slope determined by an internal reference.

The comparator output remains HIGH until the down-going ramp voltage crosses the comparator threshold. During the downward ramp the 14435 counts pulses from a stable oscillator and latches the count when the comparator output goes LOW. The counters and other internal control circuitry are also reset and the ramp control line returns to ZERO, thus initiating the next conversion.

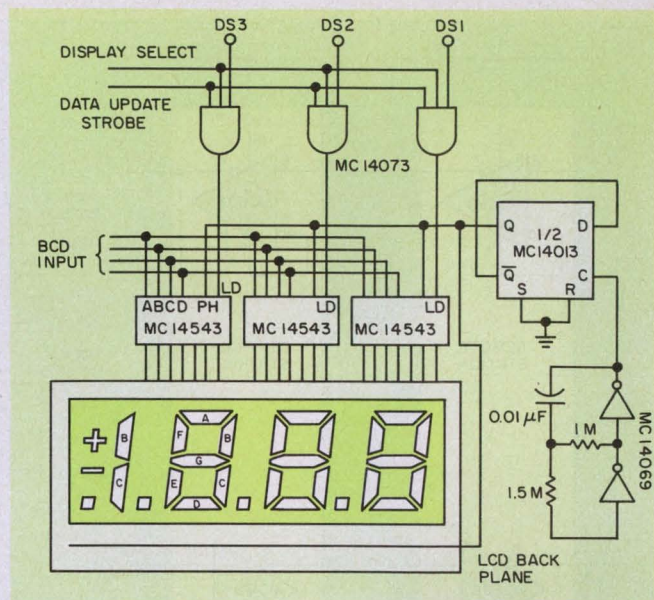


in turn opens the first channel's MC14529 transmission gate. With the transmission gate held open, the 10 kΩ resistor keeps the ramp control line HIGH and the 1405 integrator voltage ramps to zero and stays there.

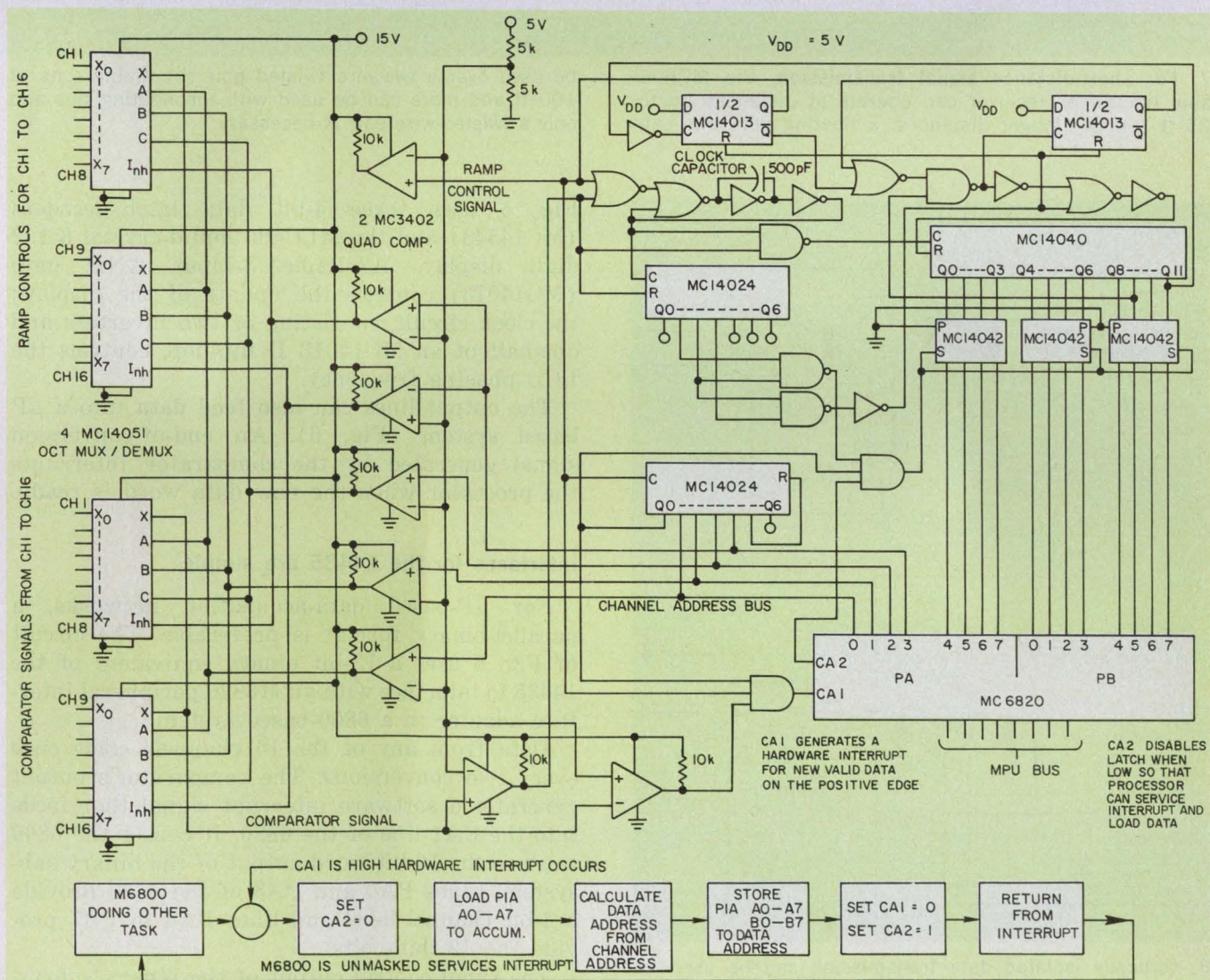
As the first channel's ramp voltage crosses the comparator threshold, the next channel gets a ramp-up command from the 14435 and the process repeats. The MC14028 binary-to-one-of-eight decoder monitors the address scanner and delivers a display-select output that is held HIGH during each conversion so that the display shows the results of any channel that is selected.

The half of the 14520 that hasn't been used yet can provide a data-update strobe signal that goes HIGH with the ramp-up command and returns to the LOW state after the third clock pulse of the conversion cycle. Thus, you can use it to enable and disable the redundant digit-select pulses available from the NOR gates in Fig. 4.

Interfacing the output data from the 14435 can be done in several different ways. The circuit of

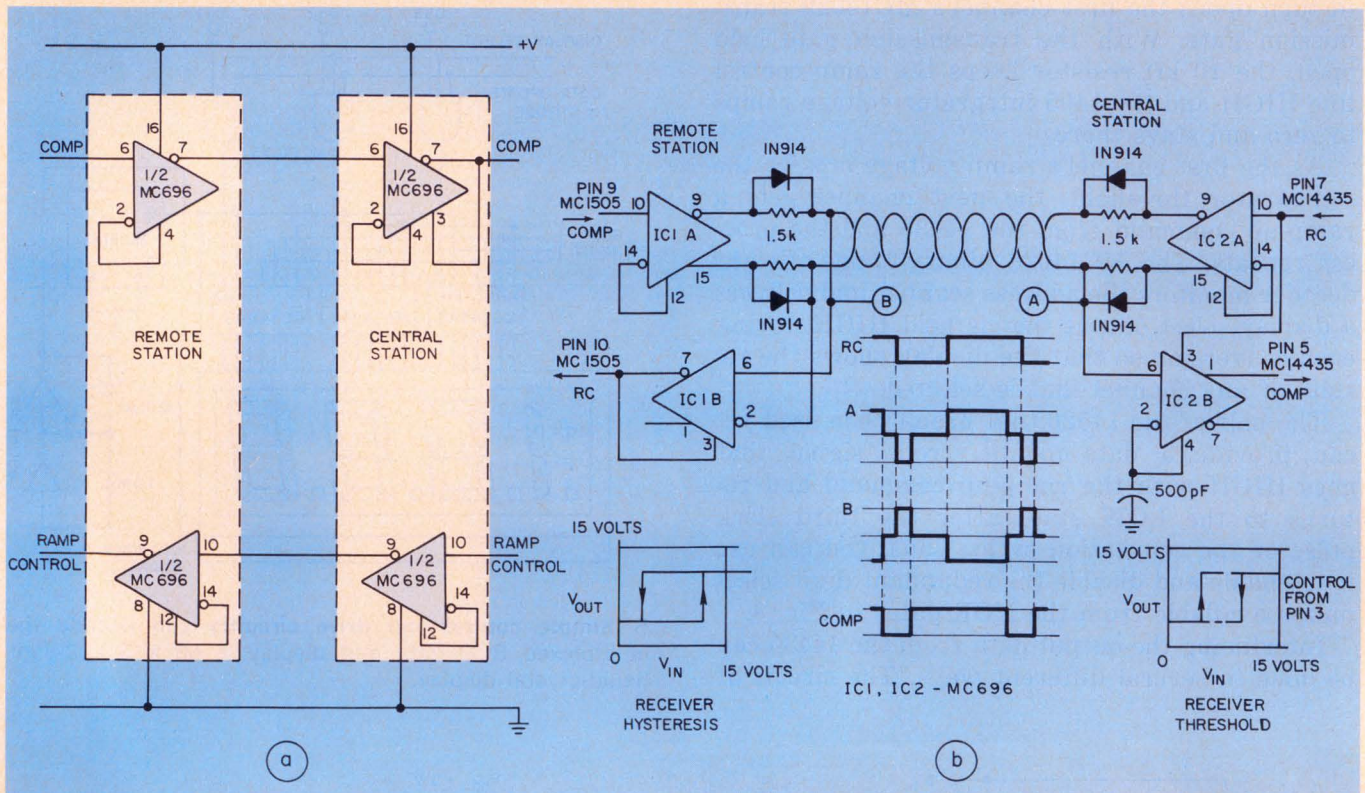


5. Simple control and drive circuitry can decode the multiplexed BCD data and display it on a 3-1/2-digit liquid-crystal display.



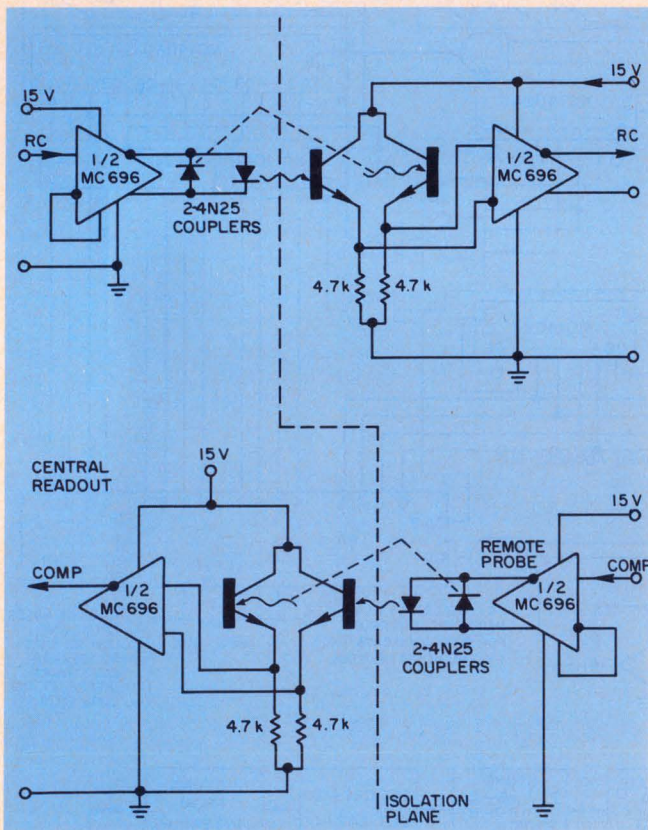
6. A complete 16-channel system using a binary-output digital subsystem can feed all data into a microproces-

sor-based controller under software command. The 6820 PIA generates the software interrupt.



7. For short-distance signal transmission, the MC696 dual line-driver/receiver can operate at distances up to 25 ft (a). For longer distances, a floating data bus can

be used over a two-wire twisted pair (b). Cable runs of 100 ft and more can be used with the floating bus and only a twisted-wire pair is necessary.



8. Optically isolated data transmission can be used in areas where ground potentials present damaging levels to the circuits. For long cable runs emitter followers provide the drive capability.

Fig. 5 uses three 4-bit data latch/decoders (MC14543) and the MLC400 liquid-crystal 3-1/2 digit display. A triple 3-input AND gate (MC14073) controls the update of the display; the clock circuit, consisting of two inverters and one-half of an MC14013 D flip-flop, controls the LCD phasing frequency.

The output lines can also feed data into a μ P based system (Fig. 6). An end-of-conversion signal generated by the comparator interrupts the processor when the new data word is ready.

Interfaces for the 14435 are simple

For μ P-based data-acquisition networks, a parallel-binary format is preferable. The circuit of Fig. 6 uses a 12-bit binary equivalent of the 14435 to interface with an M6820 peripheral interface adapter in a 6800-based system.

Data from any of the 16 channels come once every two conversions. The comparator's output generates a software interrupt signal that feeds into the CA1 line of the 6820. It causes the 6800 to store the 16-bit word output of the binary subsystem. Lines PA0 and PA3 of the 6820 provide a 4-bit channel label and lines PA4 to PB7 provide the 12 data bits.

The ramp control output of the binary subsystem advances the MC14024 counter, thus incrementing the scan address. If either the 14435 or

the binary subsystem is used, the processor can provide channel addresses under software control.

Digital CMOS signals are not ideal for long-distance transmission. Requirements will vary, of course, depending upon your application, but let's look at several line driving schemes using the MC696 dual line driver/receiver.

Do the signal transmission with line drivers

For distances of 25 ft or less the 696 can be used directly as a single-ended line driver (Fig. 7a). If capacitive decoupling of power supplies for the circuits is not possible at remote locations, you can use an MC7812 regulator to power the 696 circuit. Over short distances the cost of a four-wire cable is probably less than the cost of a remote supply.

When distances increase to more than 25 ft, a single twisted-wire pair can be used to transmit the digital data (Fig. 7b). This method parallels the output of one driver with the input of another and can send data over distances of more than 100 ft.

This "floating bus" method uses the real-time nature of the control signals. Conversion information is contained in the time between ramp control transitions and comparator signals, and the nature of these signals guarantees that the two will always alternate. Any voltage caused by the transmission-line delay can be calibrated out by the 1405's zero adjust.

The voltage between points A and B on the schematic of Fig. 7b can be positive, negative or zero depending on the outputs of IC_{1A} and IC_{2A}. The diode-resistor networks on each output modify the signals to form sink and source nodes.

You are still able to decode the information since the alternating-edge constraint keeps everything in sync. Also, one of the signals is locally generated and the other must be received and decoded at the sensor. IC_{1B} generates the ramp-control signal simply by using its internal hysteresis. The comparator signal at IC_{2B} is derived from the switching of the receiver threshold each time the ramp control line changes state. A 500-pF capacitor connected to IC_{2B} slightly delays the ramp control signal to ensure that the line driver cannot detect the edge that switches the threshold.

In many instrumentation systems, large ground-potential differences can create interconnect problems to a central collection point. Optoisolators can be used on the outputs or inputs of the 696s to provide isolation of up to 2500 V (Fig. 8). Back-to-back LEDs from two 4N25 couplers operate at about 8 mA and provide bi-directional signal handling. If extremely long lines are used, emitter followers can increase the line-driving capability. ■■

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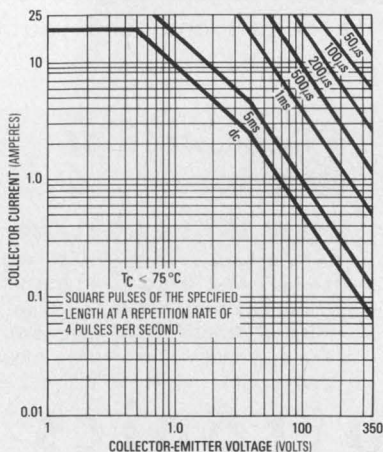
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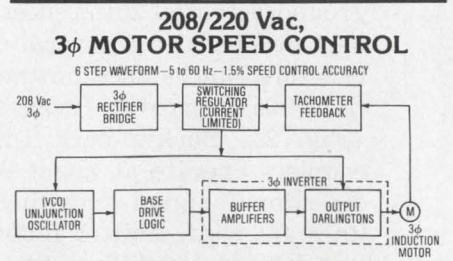
Our experience with tolerances, faults, transients, and start-stall conditions in most systems convinces us that these Darlington have the right trade-off between speed and peak power handling capability. Note the greater than 10 kVA region of the reverse bias safe operating graph. All this, and you still get Delco's traditional solid copper TO-3 hermetic package that has a conservative 0.75°C/W thermal resistance.

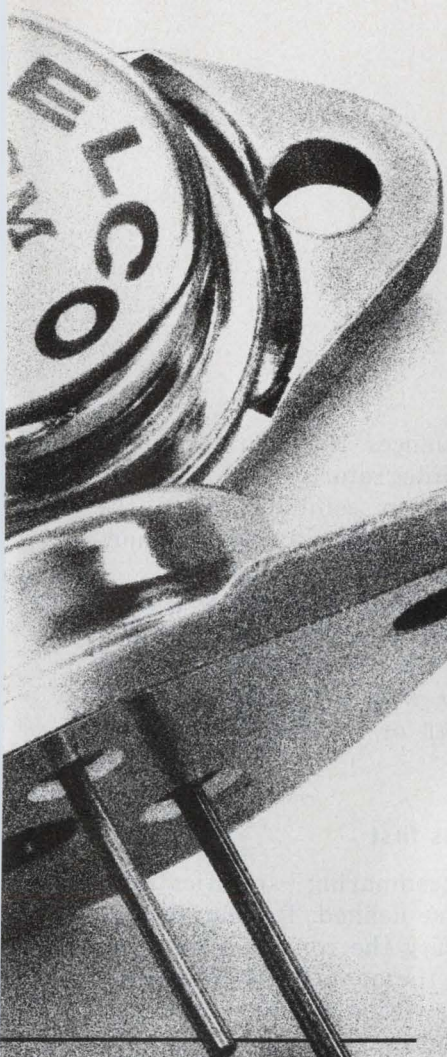
These Darlington are already in high volume production and are available on distributor shelves. Prices, applications literature, and data sheets from your nearest Delco sales office or Delco distributor can complete the story on these new Darlington.



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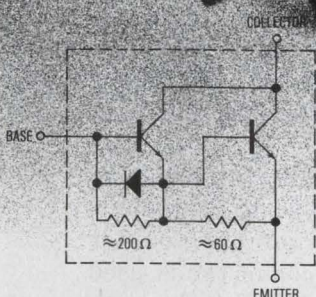
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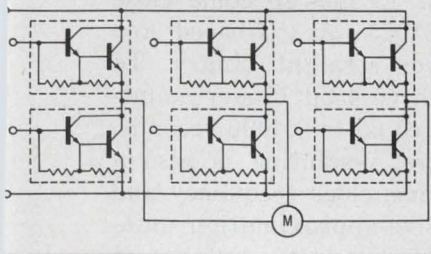
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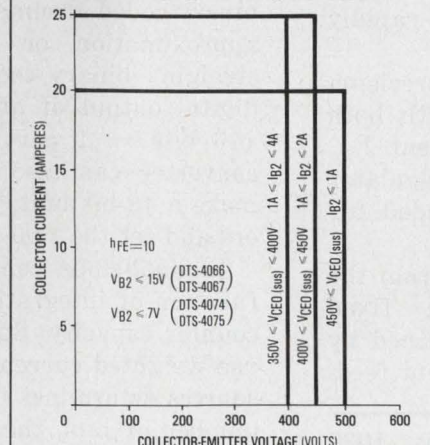


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Consider v/f converters for data-acquisition systems. They offer high resolution and accuracy when used as analog-to-digital converters.

Examine the performance specifications of voltage-to-frequency converters before you pick an analog-to-digital converter for your application. Three relatively inexpensive (under \$100) methods—the successive-approximation, dual-slope and voltage-to-frequency conversion schemes—can deliver equal accuracy, but each is used best in a different application (Table 1).

Look at the key converter specifications (Table 2) to evaluate the performance of v/f converters compared to the two other methods. Some of the most commonly specified parameters are resolution, linearity, conversion time, temperature stability and monotonicity (no missing codes).

V/f conversion: an alternative a/d method

Seldom used until a few years ago, v/f conversion techniques are rapidly becoming popular as an alternative to successive-approximation or dual-slope techniques. There are several ways to build a v/f conversion circuit, but the charge-balancing method (Fig. 1a) is the most popular.

If V_{in} is positive, the integrator output ramps down until its output voltage V_1 , crosses the comparator's threshold (ground, in this case) and causes the comparator to change state. The transition, in turn, triggers a precision timing circuit that delivers a constant-width pulse. The pulse gets fed to two places: a buffer circuit that then feeds the output; and the integrator, where the pulse causes the integrator output to rapidly ramp up (Fig. 1b).

The timing circuit is, in effect, a precision one-shot multivibrator that is stable with both time and temperature. The reference current, I_{ref} , must also be stable, and a precision regulator with a voltage reference source is included for that purpose.

Since the reference current is pulled from the integrator summing junction for a fixed amount of time, and at intervals determined by the input voltage, the positive-input current feed-

ing the integrator balances the current pulses being pulled out. The integrator can be made extremely linear and, when combined with the charge-balancing feedback loop, can achieve nonlinearities as low as 0.005%.

To form an a/d converter with the v/f technique, the output of the v/f circuit must feed a counter that is gated for the desired maximum count (for a converter with a 10-kHz output, a four-digit BCD counter or a four-stage binary counter can be used).

Nail down the definitions first

Before you start comparing specifications, make sure the specs are defined. Resolution tells you the smallest quantity the converter can distinguish. Even though the quantity is usually an analog voltage the resolution is given in terms of bits: 8, 10, 12 or more.

The usable resolution of a converter can be less than the stated resolution. However, because it's a function of linearity and stability, the usable resolution can often change with time and temperature.

In the v/f form of an a/d converter, the resolution is determined by the full-scale frequency, the time base and the capacity of the counter used (Fig. 2). If a 10-kHz v/f converter is used with a time base of 1 second and four decade counters, its resolution is one part in 10,000, or four binary-coded decimal (BCD) digits. Successive-approximation or dual-slope converters with straight binary coding would have to deliver a digital output of at least 13 bits to come close (13 bits = 1 part in 8192). A v/f-based a/d converter can also deliver straight binary. To make a 12-bit unit, use three 4-bit binary counters and set the time base equal to 0.4096 seconds.

In dual-slope converters, resolution is also a function of integration time, clock frequency and counter capacity. Successive-approximation units use weighted current sources, and the number of sources determines the resolution. The higher the number of bits, the harder it becomes to maintain the linearity of the weighted sources.

Table 1. Typical converter applications

A/d converter type	Common applications
Successive approximation	High-speed data-acquisition systems Pulse-code-modulation systems Waveform sampling & digitizing Automatic test systems Digital process control systems
Dual slope	Digital multimeters Digital panel meters Laboratory measurements Slow-speed data-acquisition systems Monitoring systems Ratiometric measurements Measurements in high-noise environments
Voltage to frequency	Digital multimeters Digital panel meters Remote data transmission Totalizing measurements Measurements in high-noise environments High-voltage isolation measurements Ratiometric measurements

Table 2. Comparison of a/d converter types

Specification	Successive approximation	Dual slope	Voltage to frequency
Resolution	12 bits	12 bits	12 bits
Missing codes	none by careful design	none, inherent	none, inherent
Nonlinearity	$\pm 0.012\%$ max.	± 0.05 to 0.01% max.	$\pm 0.005\%$ max.
Diff. nonlinearity	$\pm 1/2$ LSB	≈ 0	≈ 0
Tempco	10 to 50 ppm/ $^{\circ}$ C	10 to 50 ppm/ $^{\circ}$ C	10 to 50 ppm/ $^{\circ}$ C
Conversion time	2 to 50 μ s	5 to 77 ms	0.041 to 0.41 s
Noise rejection, 60 Hz	None	40 to 60 dB	33.8 dB*

*For 0.41-s conversion time.

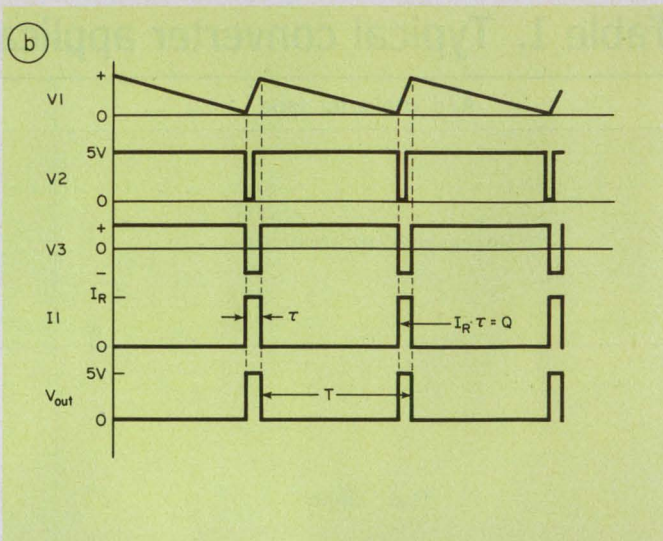
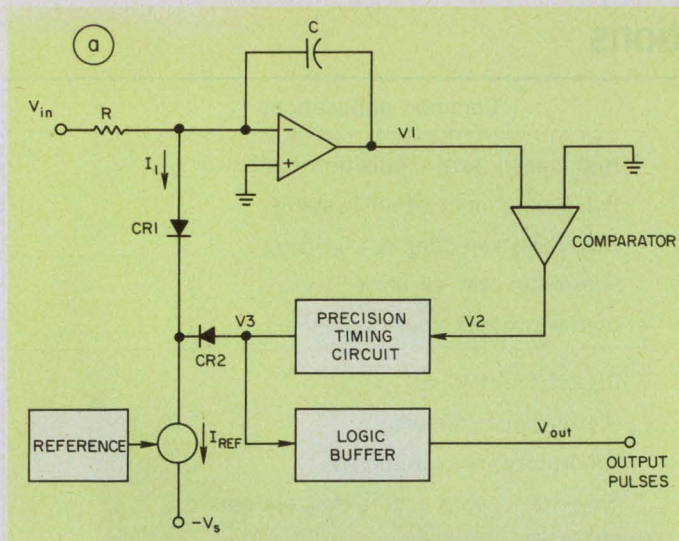
Linearity is the acid test of any a/d converter specification since resolution can be unusable if linearity error doesn't hold to less than ± 0.5 LSB (1 LSB at the worst). At a fixed temperature, linearity is the only error that remains after offset and gain errors have been adjusted out.

The linearity error of a converter is the maximum deviation of the output values from a straight line drawn from zero to the maximum output. For 12-bit a/d converters a "good-quality," successive-approximation unit has a non-

linearity of about $\pm 0.012\%$, a dual-slope unit about ± 0.05 to $\pm 0.01\%$ and a v/f converter about ± 0.01 to $\pm 0.005\%$.

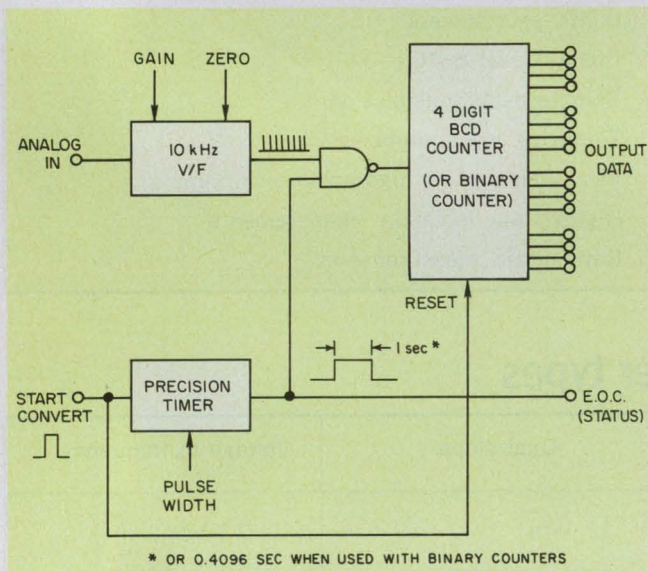
The nonlinearity characteristic of successive-approximation converters differs fundamentally from that of the dual-slope or v/f. Typical nonlinearity curves are shown (slightly exaggerated) in Fig. 3.

Both the v/f and dual-slope converter linearity characteristics tend to have a bow that is caused by the operational integrators used in the con-

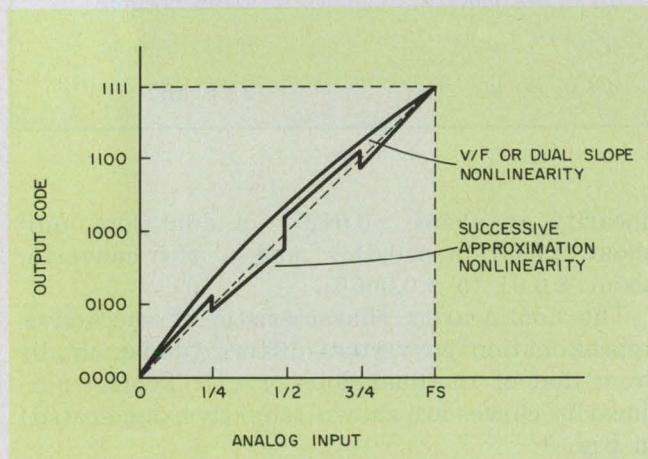


1. The basic charge balancing v/f converter (a) uses an operational integrator with a precision timing circuit con-

nected in a feedback loop. The output pulse width (b) is proportional to the charge stored in the capacitor.



2. By using a v/f converter and a precision timer, you can build an a/d converter that delivers a BCD output.



3. Nonlinearities of v/f and dual-slope a/d converters appear as a slight bow in the curve. However, successive approximation nonlinearities make the curve jagged.

verters. By contrast, the successive-approximation converter's linearity is determined by the major-carry transitions of the weighted current sources. These points are located chiefly where $1/2$ and $1/4$ -scale current values are switched in or out during the conversion process.

As shown in the graph of Fig. 3, a jump in the curve signifies when a major-carry current value is slightly off its correct value. A very linear converter restricts these jumps to very small amounts ($\pm 0.012\%$ for a 12-bit converter).

Don't let the converter slow you down

The v/f converter takes the longest to do a complete conversion. The time base used in Fig. 1 is 1 second for a single conversion—rather slow for most applications. Dual-slope converters are faster, with conversion times ranging from 5 ms to 100 ms.

Successive-approximation converters are the fastest of the three, with conversion times as short as $2 \mu\text{s}$ for 12-bits. Most successive-approximation converters have conversion times between 3.5 and $50 \mu\text{s}$.

However, if time isn't a problem, you can increase the time base to 10 seconds, add another decade counter and, voila: a converter with a resolution of one part in 100,000. Such a long conversion time could cause difficulty in many applications. And, the linearity of the 10 kHz unit would not be commensurate ($\pm 1/2$ LSB) with the increased resolution.

Since the time for conversion can be made equal to the inverse of the line-voltage frequency, the dual-slope converter can be designed to reject much of the noise caused by the power line. The integrating technique used by dual-slope and v/f converters gives them the ability to reject

Successive approximation and dual slope conversion methods

The successive-approximation approach is the most widely used (Fig. A) of the three most popular conversion schemes. It compares the output of an internal d/a converter against the input signal, one bit at a time. Therefore, N fixed time periods are needed to deliver an output N bits long, but the total time needed is independent of input-voltage value.

The first step after the start pulse in a successive-approximation conversion cycle is turning on the MSB, which sets the d/a converter's output at half-scale (Fig. B). This analog signal is then fed back to the comparator. The MSB is left on if the d/a converter's output is smaller than the analog input, and turned off if the output is larger.

Next, the second bit is turned on, and the quarter-scale value added to the d/a converter output and the comparator again does its job. This process continues until the LSB has been tested and the final comparison made. When the process is complete, the converter signals this by changing the state of its end-of-conversion (status) output. The final digital output can then be read from the output of the successive-approximation register of the converter.

Successive-approximation converters can achieve conversion speeds of 100 ns/bit in medium-priced

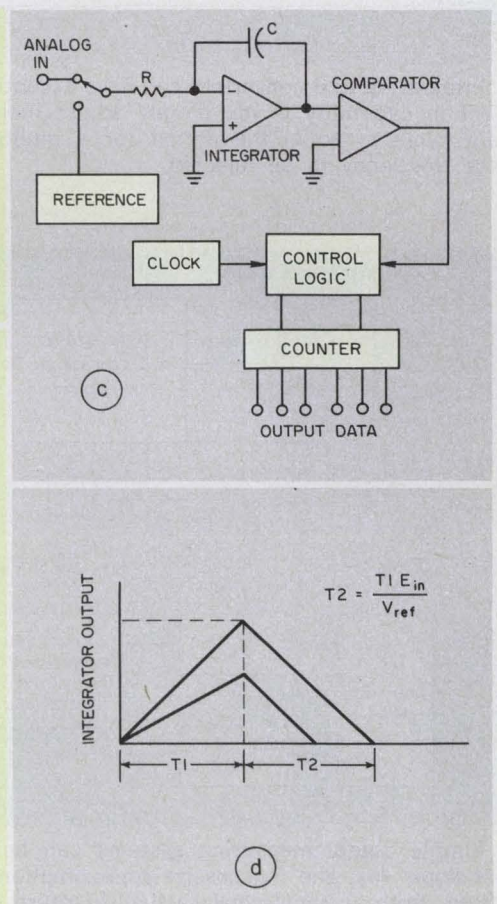
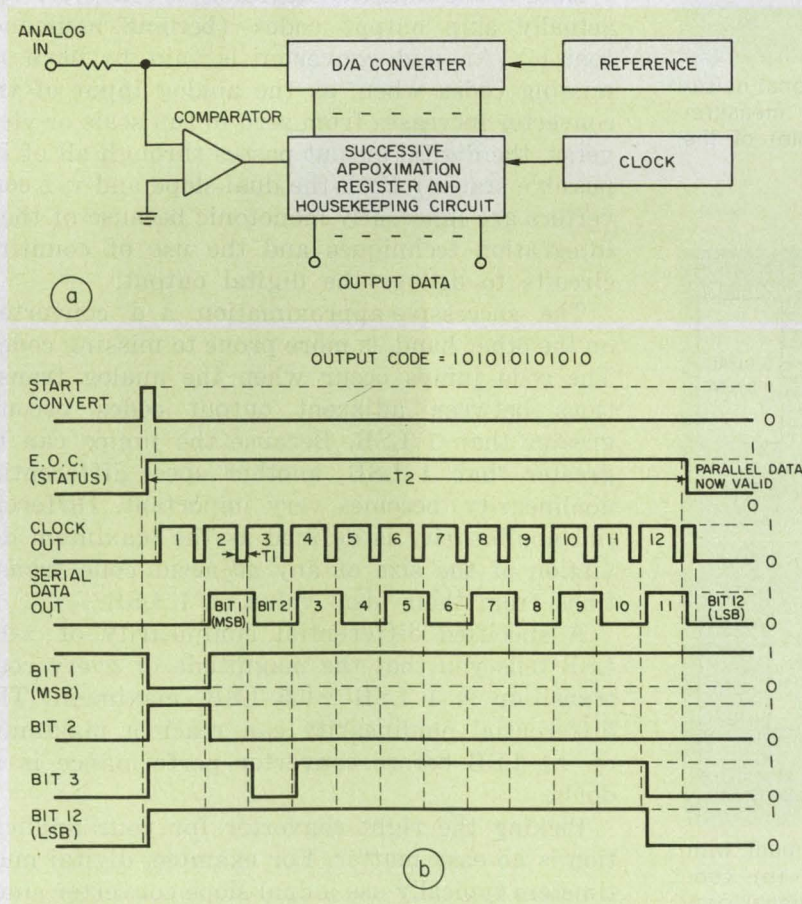
(\$250 to \$350) 8 and 10-bit units. Converters with 12-bit outputs are typically available with conversion times ranging from 2 to 50 μ s.

Dual-slope units slow the pace

The dual-slope converter uses a simple counter to indirectly measure the input signal after an operational integrator converts a voltage into a time period (Fig. C). This scheme is the second most commonly employed method and is used, almost exclusively, in such instruments as digital multimeters and panel meters.

The conversion cycle begins when the analog-input signal is switched to the input of the operational integrator. The voltage is integrated (Fig. D) for a fixed time period determined by the clock frequency and the counter size. At the end of the period, the integrator input is switched to an internal reference whose polarity is opposite that of the original analog input. The reference is then integrated until the output reaches zero and triggers the comparator.

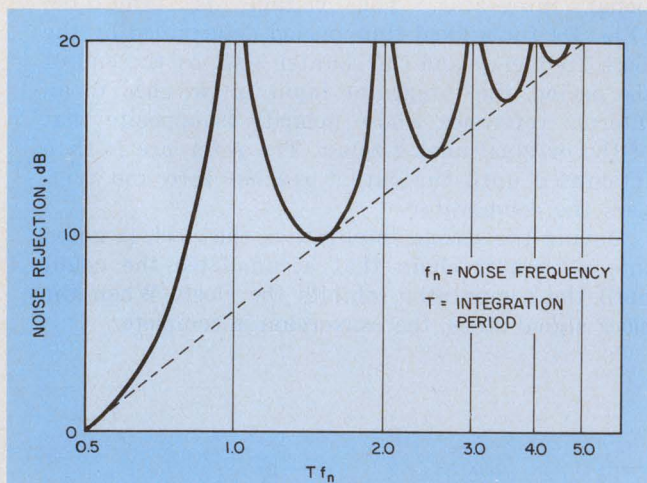
During the second integration, the clock is gated into a counter chain that accumulates the count until the comparator inhibits the clock. When the clock signal stops, the conversion is complete.



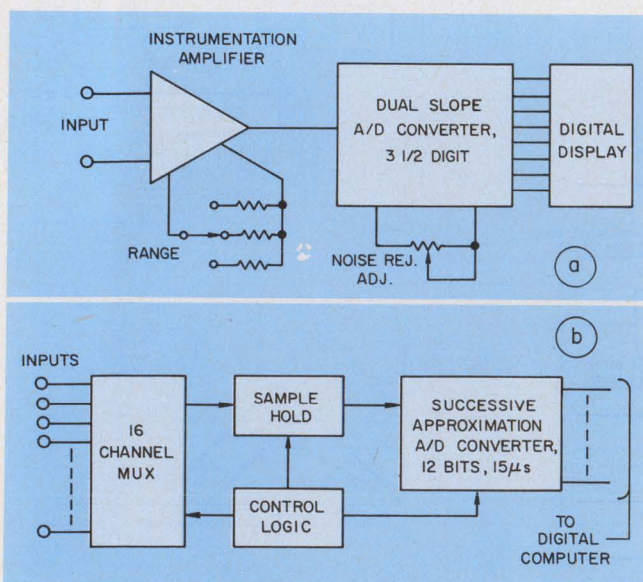
high levels of input noise.

For these two integrating converters, the longer the signal is integrated, the better the noise attenuation. When the integration period equals a multiple of the inverse of the line frequency (for dual-slope units), the noise rejection becomes infinite at integral values Tf_n , where T is the integration period and f_n is the noise frequency (Fig. 4). V/f converters don't, in general, use a period that is a multiple of any periodic noise, and so the asymptote of the noise-rejection curve is used to determine the rejection at a given Tf_n .

The v/f converter's noise-rejection asymptote rises by 20 dB per decade, and, for a 60-Hz power



4. Integrating a/d converters can have exceptional noise-rejection capability if you merely adjust their measurement cycle to equal the period (or a multiple) of the noise frequency to be rejected.



5. Simple digital measuring systems can be built with dual-slope (a) and successive-approximation (b) converters. Both systems shown usually require signal conditioning for each input.

line and a 0.41-s conversion time, the rejection can be computed at 33.8 dB. Dual-slope converters have rejection ratios as high as 60 dB when conversion is synchronized with the noise frequency.

Successive-approximation converters have no noise-rejection capability whatsoever. Input noise at any time during the conversion process can cause significant conversion errors. (Noise feeds directly to the comparator and can change the decision point.) The only way to minimize noise is to add an input noise filter to the converter.

Temperature coefficients change converter specs

Operation at different temperatures can tremendously alter converter performance, no matter which converter type you select. These changes affect offset and gain, two important converter parameters. Even though offset and gain are adjusted during calibration, they can change significantly with temperature.

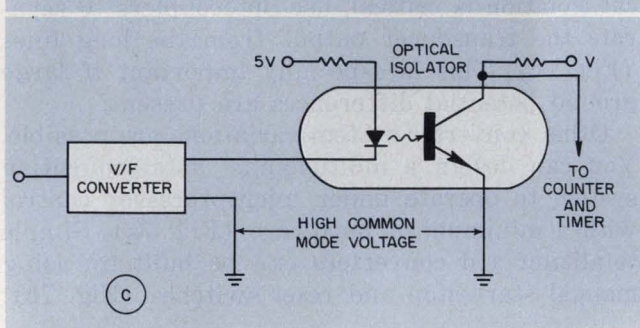
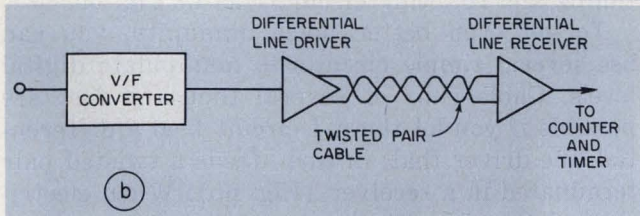
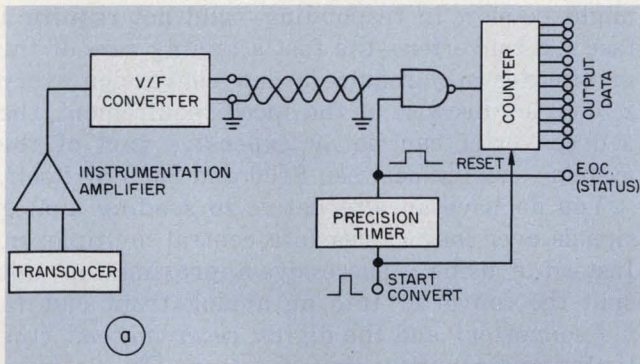
Offset is a function of current-source leakage, comparator bias current and comparator input voltage offset. Gain (sometimes called scale factor) is a function of the voltage reference, resistor tracking and semiconductor-junction matching—and is usually the most difficult parameter to control. Absolute accuracy is affected by offset and gain changes, so if these change during operation, output errors will occur.

And, if the linearity degrades, a converter can actually skip output codes (become nonmonotonic). (An a/d converter is said to have no missing codes when, as the analog input of the converter increases from zero to full scale or vice-versa, the digital output passes through all of its possible states.) Both the dual-slope and v/f converters are inherently monotonic because of their integration techniques and the use of counting circuits to deliver the digital output.

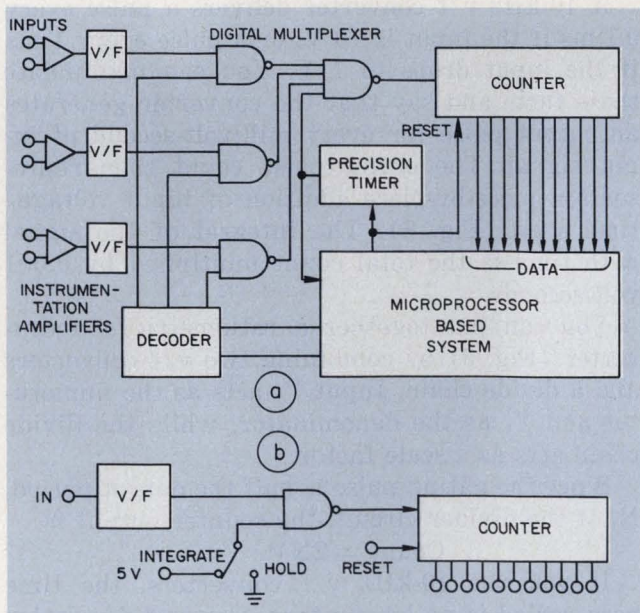
The successive-approximation a/d converter, on the other hand, is more prone to missing codes. The code jumps occur when the analog transitions between adjacent output codes become greater than 1 LSB. Because the jumps can be greater than 1 LSB, another spec. differential nonlinearity, becomes very important. Differential nonlinearity is defined as the maximum deviation of the size of any adjacent code transitions from their ideal value of 1 LSB.

A specified differential nonlinearity of ± 0.5 LSB tells you that the magnitude of every code transition is $1 \text{ LSB} \pm 0.5 \text{ LSB}$, maximum. The differential nonlinearity can reach a maximum of ± 1 LSB before converter performance is in doubt.

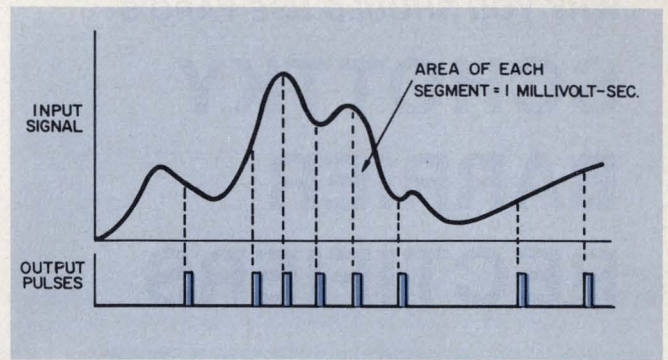
Picking the right converter for your application is no easy matter. For example, digital multimeters typically use a dual-slope converter since high speed isn't necessary but high noise rejection



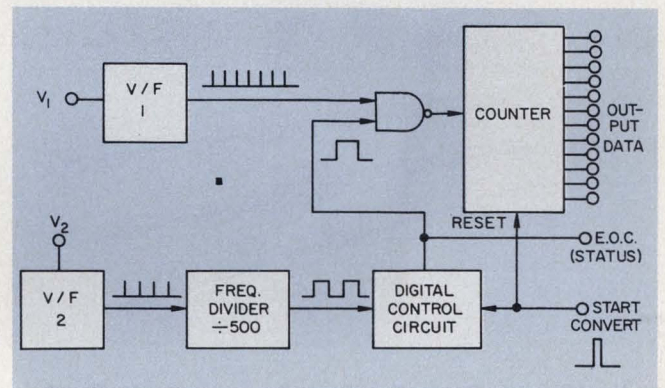
6. V/f converters can be used in simple, remote data-gathering applications since only a twisted pair of wires is needed to transmit the signals (a). Differential line drivers can be added if long transmission distances are required (b), or an opto-isolator can be used to eliminate large, common-mode voltage problems (c).



7. A microprocessor or computer-based controller can be used to make a multiple-channel data-collection system with a v/f converter at each point (a). If manual switches are used instead of a timer, you can turn a v/f-based a/d converter into an "infinite" integrator (b).



8. The integration process in a v/f converter can be defined in terms of millivolt-seconds for each pulse delivered. To get the total area, simply multiply the total count by 0.001.



9. If you use two v/f converters, you can make a high-accuracy, ratiometric a/d converter. Because of the wide frequency span covered, the dynamic range of the converter can reach 10,000:1.

tion is. However, in other applications, such as in fast-throughput data acquisition, the successive-approximation converter must be used.

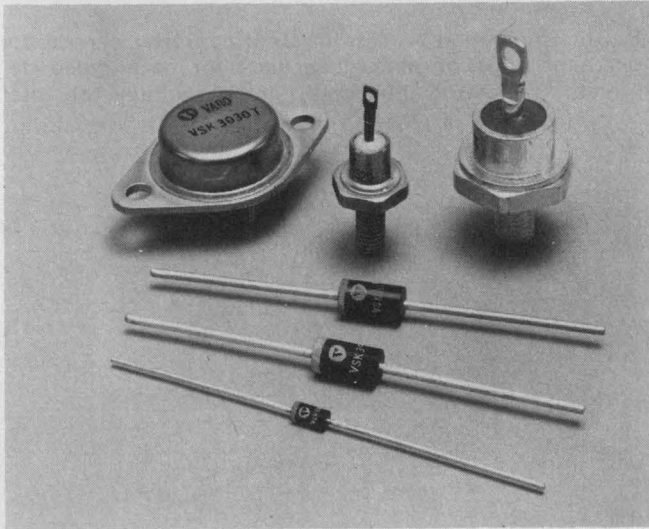
Dual-slope converters are widely used in applications requiring human interface in measurement and control. A simple digital measurement system (Fig. 5a) that uses a 3-1/2 digit, BCD-output converter can handle various signal inputs. The instrumentation amplifier used on the front end offers flexible gain settings with a single resistor value change.

The converter can be either a modular unit manufactured by several vendors or one made from the various IC building blocks. In many industrial and even in some lab environments, pick-up from 60-Hz radiation or magnetic coupling can cause measurement problems. By including a conversion time adjustment, you can synchronize the clock to the 60-Hz line and obtain noise rejection of more than 40 dB.

When multiple channels of data must be handled and you need all the data quickly, use the speedy successive-approximation converter. The circuit shown in Fig. 5b is a commonly used system organization for multichannel data acquisition. Although various analog-input devices

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CIRCLE NUMBER 82

might be slow in responding—and not require a fast a/d converter—the fast scanning rate of the multiplexer may require a new conversion every 2 to 30 μ s. Because of the speed requirement, the a/d converter can be an expensive part of the system—costing between \$100 and \$300 by itself.

You do have an alternative to sending analog signals over long cables to a central multiplexer. Instead of using a successive-approximation unit split the converter into an analog front end (a v/f converter) and the digital receiving end (the timing and counting circuits) as in Fig. 6a.

To get even better noise immunity, you can use several simple circuits to manipulate digital levels. Cable runs of several thousand feet are possible if you let the v/f circuit feed a differential line driver that, in turn, feeds a twisted pair terminated in a receiver (Fig. 6b). When electrical isolation is critical, use optocouplers to separate the transducer output from the long lines (Fig. 6c). This is especially important if large ground potential differences are present.

Other converter-system variations are possible. You can design a multichannel data-acquisition system to operate under microprocessor control with a minimum of hardware (Fig. 7a). Simple totalizing a/d converters can be built by using manual start/stop and reset switches (Fig. 7b).

Drift-free integration is only one bonus

Unlike analog integrators that must use "super high quality" components when the integration period extends past several minutes, the v/f integrator uses inexpensive components and can even hold its value indefinitely.

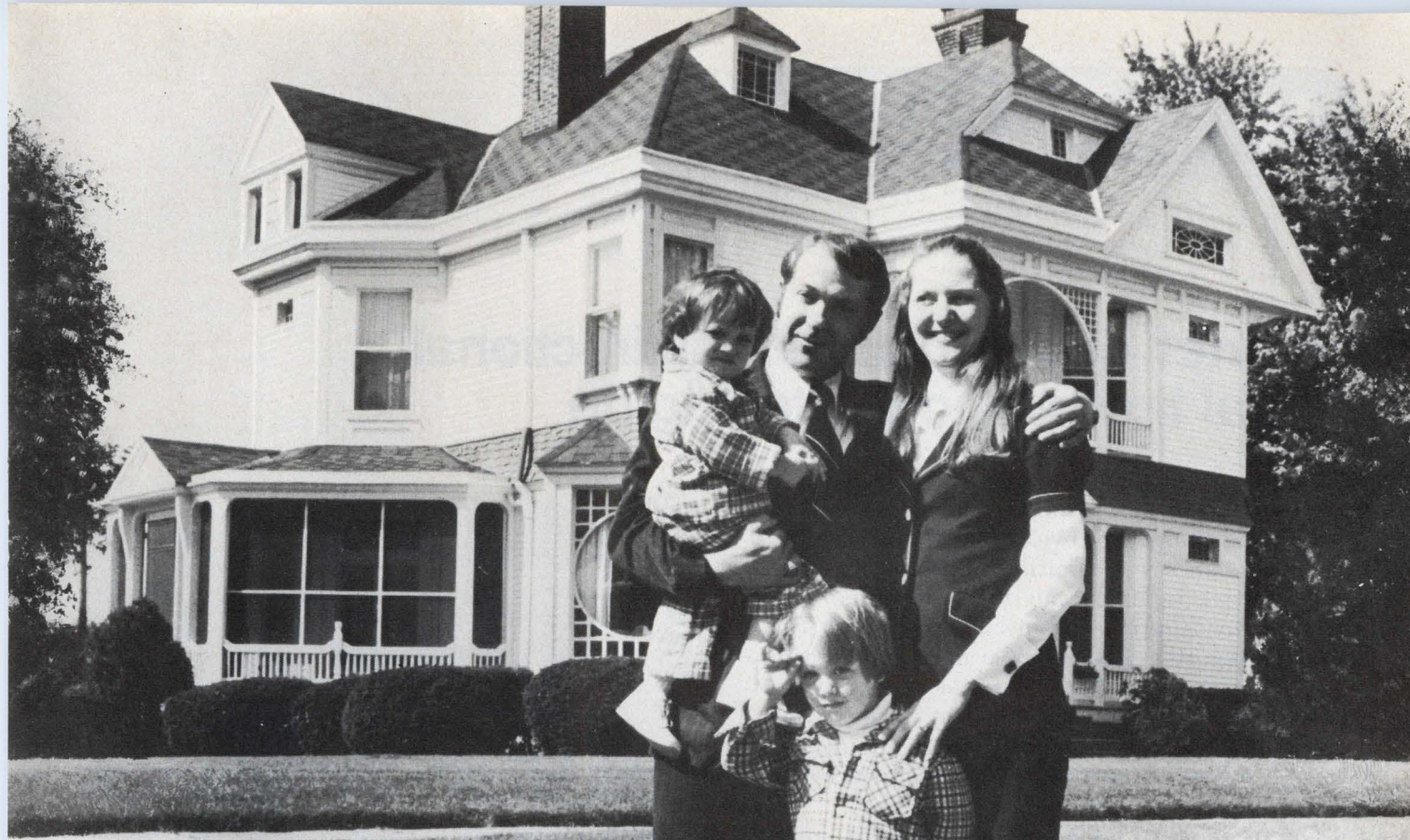
A 10-kHz v/f converter delivers a pulse every 0.1 ms if the input is 10 V, or a pulse every 1 ms if the input drops to 1 V. You can manipulate these facts and say that the converter generates an output pulse for every millivolt-second of input signal. The output-pulse count then represents a piece-by-piece addition of input voltage/time area (Fig. 8). The integral of the signal with time is the total count multiplied by 0.001 volt-seconds.

You can put together a ratiometric a/d converter (Fig. 9) by combining two v/f converters and a divide chain. Input V_1 acts as the numerator and V_2 as the denominator, while the divide chain acts as a scale factor.

Since the gating pulse is half the output period, N , of the divider circuit, the counter output is

$$\text{Count} = 2NV_1/V_2.$$

If you use 10-kHz v/f converters, the time base period is no longer than 1 second for ratios of up to 1000 to 1. Unlike other ratio-measurement methods that have rather limited dynamic ranges, using two v/f converters permits a possible dynamic range of 10,000 to 1. ■■



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Ideas for Design

Inverter circuit handles bidirectional signal flow without latching up

This unusual two-terminal circuit not only inverts logic pulses or levels, but also each of its terminals can serve as either an input or an output. Positive input signals to its terminal 1 are inverted to negative outputs at terminal 2. Conversely, negative-input signals must enter terminal 2 to provide positive outputs at terminal 1. This bidirectional circuit can be used in low-power applications such as CMOS circuits, because it draws current only when a signal level is being inverted.

The problem of latch-up that results if such a circuit is built with the usual logic modules is solved with one inhibitor circuit, Q_2 or Q_3 , for each inverter. As a result, only one inverter, Q_1 or Q_4 , respectively, functions at a time.

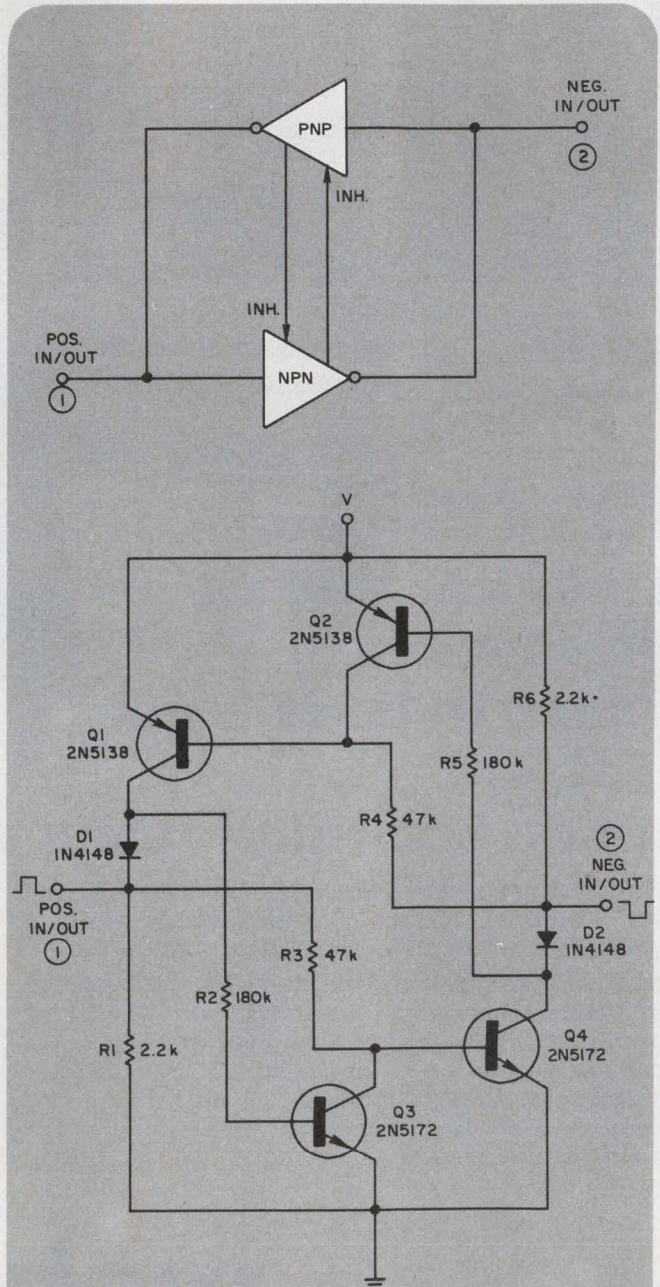
Diodes D_1 and D_2 discriminate between incoming and outgoing logic levels at their respective terminals; therefore, corresponding inverters turn ON only when an input terminal has a signal.

For example, with a positive pulse applied to terminal 1, D_1 becomes reversed-biased, and Q_3 remains cut off, but inverter Q_4 turns ON to bring terminal 2 near ground. Thus, the positive signal at terminal 1 is inverted. Transistor Q_2 also turns ON and keeps inverter Q_1 OFF, which prevents Q_1 from latching Q_4 ON.

Similarly, a negative signal into terminal 2 reverse biases D_2 to keep Q_2 OFF and also turns Q_1 ON. Transistor Q_1 turns Q_3 ON, which then holds Q_4 OFF to prevent Q_1 from latching. Terminal 1, therefore, is now the output and provides a negative signal.

Component values for the circuit are not critical. They can be chosen to conform to individual power-supply and logic-drive requirements. Diodes D_1 and D_2 can be general-purpose germanium switching diodes when used with low-threshold logic, such as TTL.

Larry Acker, Engineering Associate, Steiner-Parker Co., 356 S. 900 East C, Salt Lake City, UT 84102.

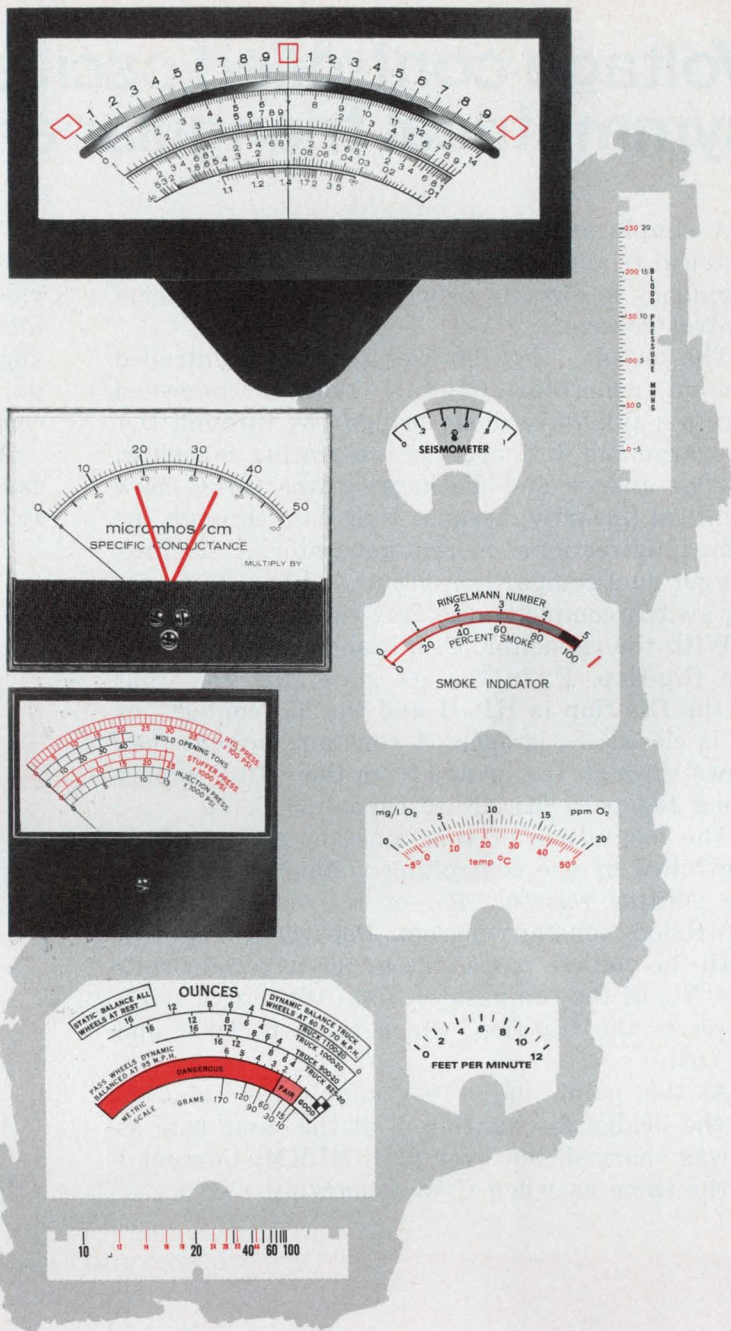


A bidirectional inverter is prevented from latching by the use of inhibitor circuits that allow only one inverter at a time to be turned ON.

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Voltage-controlled oscillator provides symmetrical triangular and square waveforms

A simple technique accurately generates symmetrical triangular and square waveforms whose frequency is directly proportional to an external control voltage.

The circuit (Fig. 1) uses a voltage-controlled current generator (VCCG) that is connected across a full-wave diode bridge (D_1 through D_4) to charge and discharge an integrating capacitor, C. The charge and discharge paths for C have identical linearity, because they pass through the same unidirectional current generator. A Schmitt-trigger dual-comparator circuit and an SPDT analog switch completes the free-running circuit.

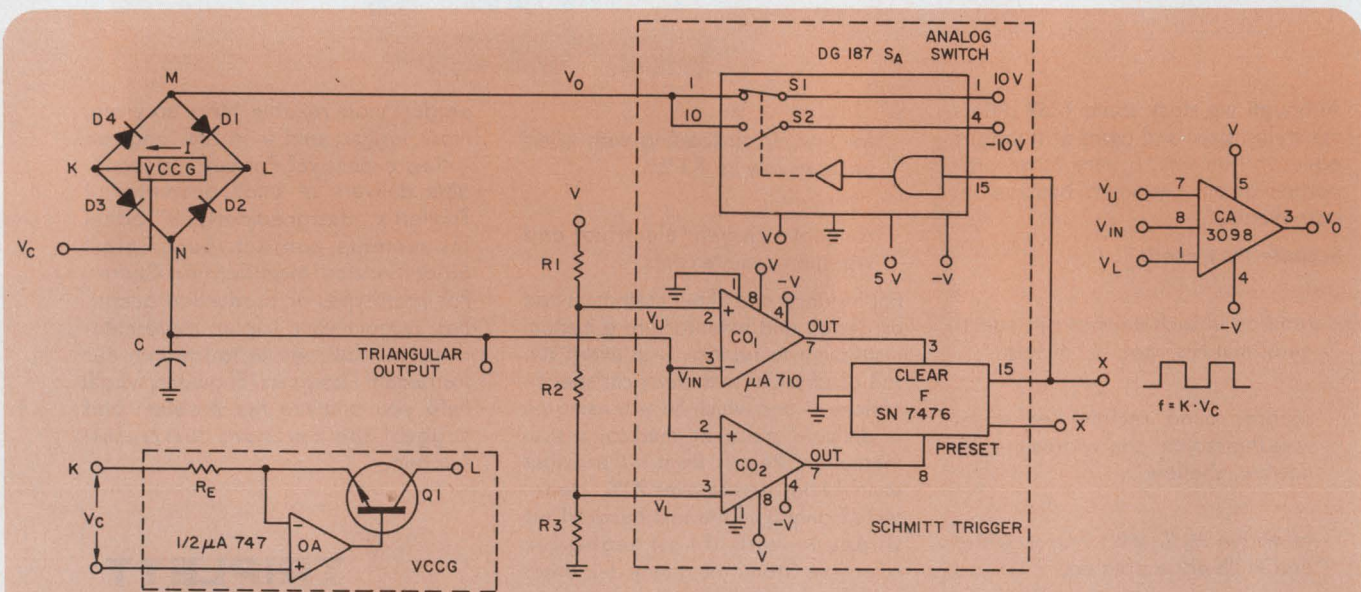
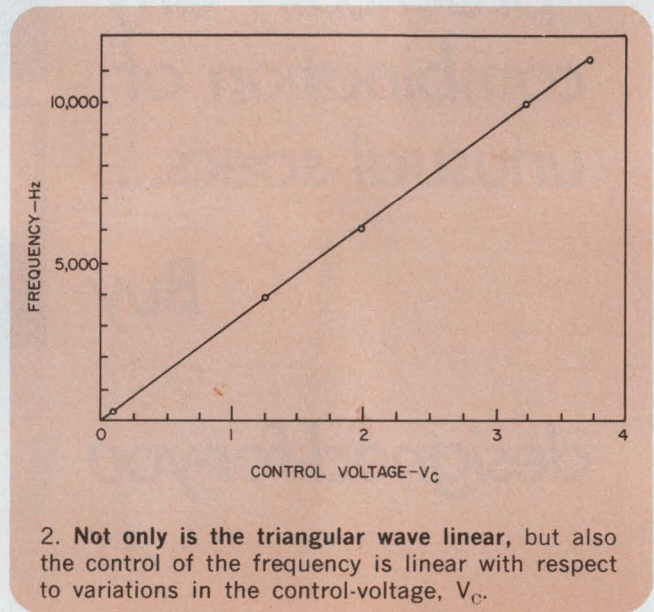
With the capacitor, C, initially discharged and the flip-flop, F, in the set state, the X output of the flip-flop is HIGH and the S_1 "contact" of S_A is closed; S_2 is open. A constant current then flows through the bridge from the +10-V supply along the path MLKN to capacitor C.

The magnitude of this constant current, I, is controlled by the controlling voltage, V_C , and by the emitter resistor, R_E , of transistor Q_1 . The controlled constant-current linearly charges C until the voltage passes the upper-trip-point voltage, V_U , of the comparator, CO_1 . When CO_1 trips, it resets the flip-flop, which turns S_1 OFF and S_2 ON.

At this point, the -10-V supply rail connects to the bridge discharging C at the same rate as it was charged, but over path NLKM. Current I is the same as when C was charging.

When the discharging voltage at node N crosses the lower trip-point voltage, V_L , CO_2 provides a signal that sets the flip-flop back to the initial condition. A free-running symmetrical triangular waveform appears at node N. The output terminal of the flip-flop provides a TTL-compatible square waveform.

A CA 3098 dual-level detector with memory can be used to replace the Schmitt and analog switch and thus reduce the number of required



1. A triangular and square-waveform generator is linearly voltage controlled by a constant-current generator. A diode bridge allows the use of the

same current generator for both charging and discharging the timing capacitor—and thus produces symmetrical waves.

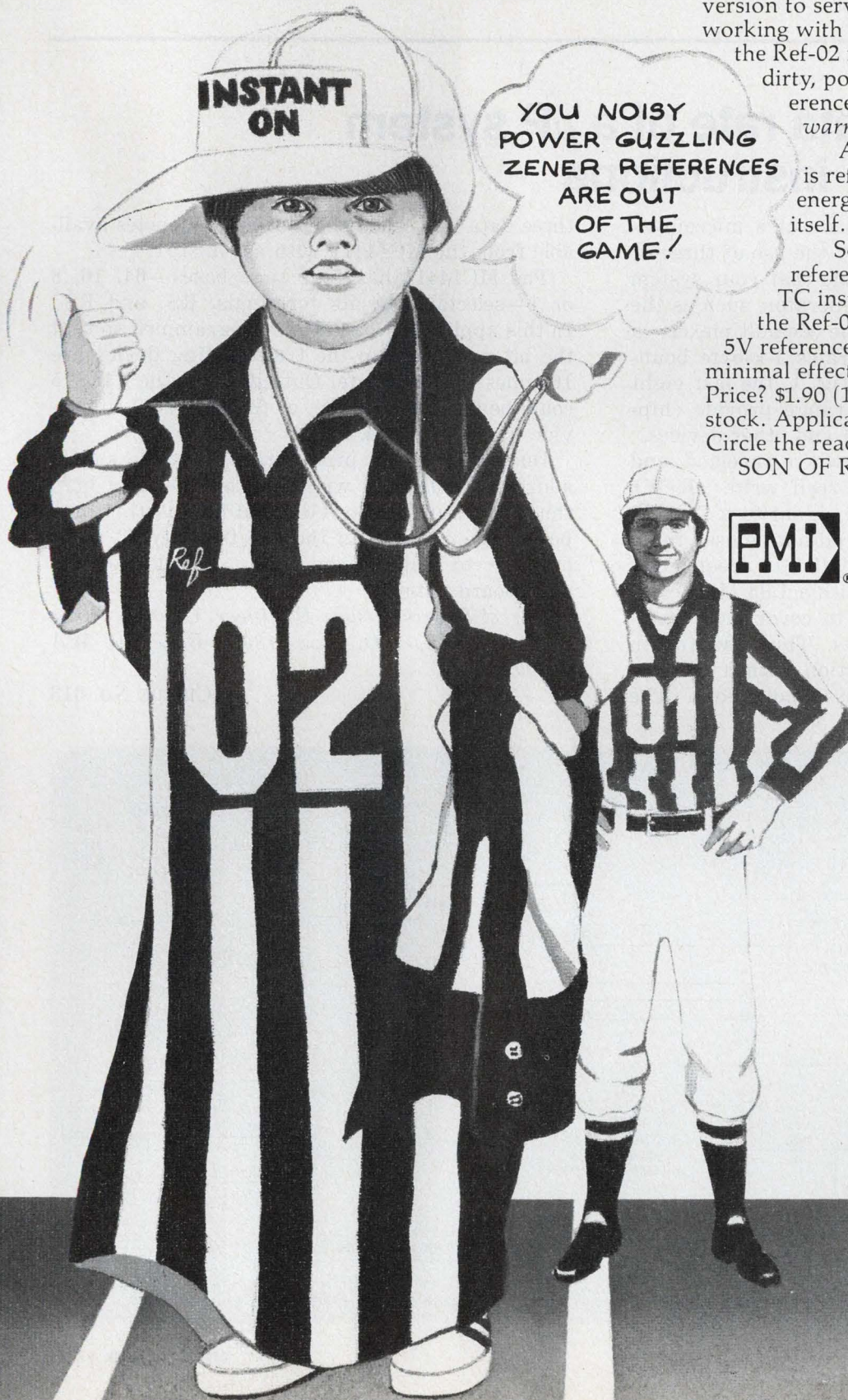
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components. Also, the CA 3098 has a large driving capability, so its output square waveform can swing almost fully from +V to -V and thereby eliminate the requirement for an analog switch.

The charging time, T_1 , of the capacitor C is

$$T_1 = \frac{(V_U - V_L) C}{V_C/R_E} = V \cdot C \cdot R_E / V_C,$$

where, $V = (V_U - V_L) =$ peak-to-peak amplitude of the triangular waveform. Similarly, the

discharging time, T_2 , of the capacitor is

$$T_2 = V \cdot C \cdot R_E / V_C.$$

The frequency of oscillation is then

$$f = 1/T = 1/(T_1 + T_2) = V_C / 2 \cdot C \cdot R_E \cdot V = k \cdot V_C.$$

Fig. 2 shows the linear f-vs.- V_C output that the circuit can deliver.

Rana Dattagupta, Dipak K. Basu, and Pradip K. Das Computer Centre, Jadavpur University, Calcutta, India 700032. CIRCLE NO. 312

Control the data rate of a μP system with software instructions

You can control the data rate of a microprocessor system with software by the use of three or four ICs (Fig. 1). It's possible that your system already contains a bit-rate generator, such as the MC14411, and a 3-to-8 line demultiplexer—a 74LS138. The 74LS138 generates 1-k-byte boundary chip-select signals. In Fig. 1, the last eight 1-k steps of the addressing range provide chip-select signals for ROM, RAM and other devices.

One of these bytes, Y_1 , when inverted and NANDed with an inverted read/write (R/W) signal, provides a new write signal to a 74LS75 four-bit latch. The 74LS75 need not be used to its full capability, since eight of the 16 frequencies generated by the MC14411 with a 1.84-MHz crystal are more than adequate to cover most data-communications requirements. Thus the fourth bit could be used in conjunction with a LED to provide diagnostics or status indications. The

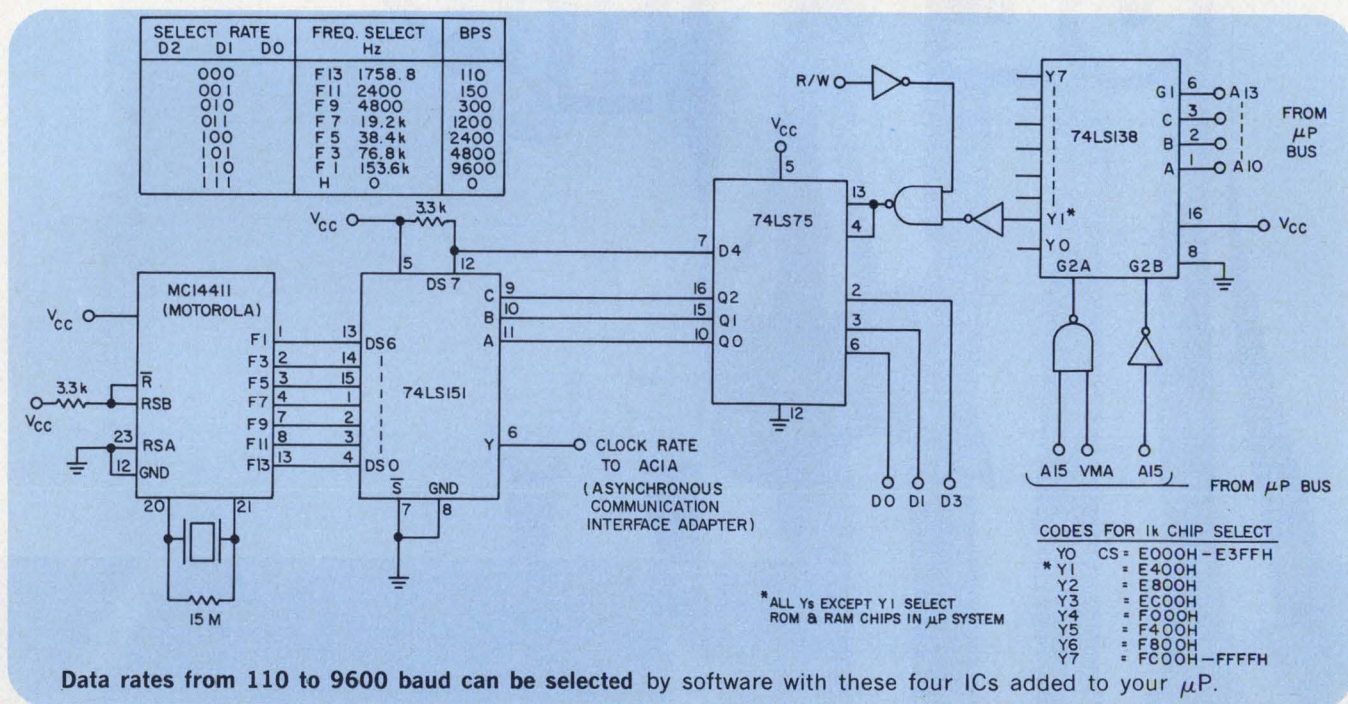
three data bits select the 1-of-8 frequencies available from the MC14411 with a 74LS151.

The MC14411 has four time bases—64, 16, 8 or 1—selectable by its terminals, RS_n and $RS_{\bar{n}}$. In this application base 16 is programmed so that the bit rates sent to the transmitting device are 16 times the data rate. Output Q_3 of the 74LS75 could be connected to RS_n of the MC14411 to provide bases 16 or 64.

During power-on procedures, firmware should address E400H and write 000 on the data bus; thus the circuit selects 110 baud for starting purposes. The control can then be transferred to an operator to make a new data-rate selection via a keyboard entry.

Garret Spears, Senior Engineer, Chem-Nuclear Systems, Inc., P.O. Box 1866, Bellevue, WA 98009.

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Use TTY or CRT interchangeably on μP system

The 6800 microprocessor family contains an Asynchronous Communication Interface Adapter (ACIA). The ACIA provides data formatting and control to interface to the microprocessor such serial I/O devices as TTYs, CRTs, and thermal printers.

A problem arises when the ACIA is used in a system in which a TTY or CRT terminal may be interchanged. A TTY requires 11 bits of serial data (2 stop bits) at 110 baud, while most other serial I/O devices—such as CRTs or thermal printers—require 10 bits of serial data (1 stop bit) at rates above 300 baud.

Although the baud rate can be readily varied manually with a switch, the 10 or 11-bit (1 or 2 stop bits) format must be programmed into the ACIA by the microprocessor. Since there are no external inputs to the ACIA for identifying whether 10 or 11 bits are required by the I/O device, a simple method was devised to inform the microprocessor how to program the ACIA.

The method uses the image locations created by "don't cares" in the address decoding. A typical addressing technique for ACIAs is shown in Table 1. Other images—8014-8017, 8024-8027, . . .—may be eliminated by decoding address bits A14 through A4, as required.

Locations 8004 through 8007 are used as examples only; this technique may be used at any address. By not decoding address bit A1, locations 8004 and 8006 respond identically and are images of the Control and Status registers. Locations 8005 and 8007 are images of the Input/Output registers.

If the register-select (RS) pin of that ACIA is tied to A1 rather than A0, then locations 8004 and 8005 are images of the Status and Control register while 8006 and 8007 become images of the Input/Output register.

During initialization, the MPU compares locations 8004 and 8006 (Table 2). If they are equal, the ACIA is programmed for 11 bits, otherwise the ACIA is programmed for 10 bits. Locations 8004 and 8007 are always used as Control/Status and Input/Output, respectively.

Fig. 1 is a block diagram of a typical ACIA implementation. The advantages of this method are:

- No address decoding, other than switch S₁, is required.



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- Switch S₁ does not load address lines.
 - Switch S₁ may be incorporated with the baud rate switch, S₂ at the 110-baud position.
- No tests need be made on locations 8005 or 8006 after initialization, since 8004 is always Status and Control and 8007 is always I/O.

The method allows software to remain the same when hardware changes.

Wallace E. DeShon, Engineer, Applied Automation, Inc., Pawhuska Rd., Bartlesville, OK 74004.

CIRCLE No. 314

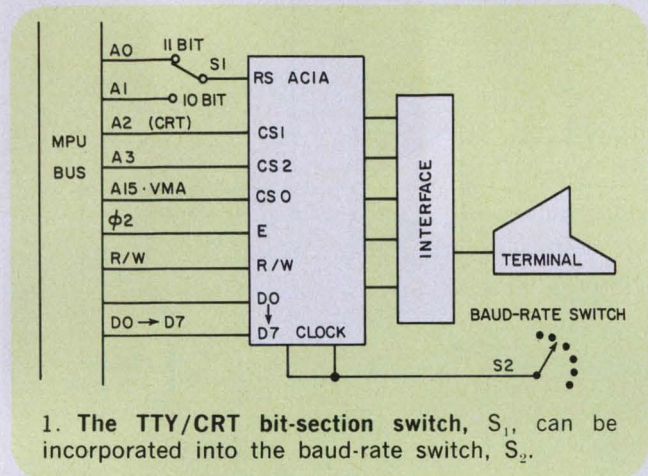


TABLE 1. ACIA ADDRESSING TECHNIQUE

CS0	CS2	CS1	DON'T CARE X	RS	LOCATIONS
A15-VMA	A3	A2	A1	A0	8004-8006 8005-8007
A15-VMA	A3	A2	A0	A1	8004-8005 8006-8007

TABLE 2. ACIA INITIALIZATION ROUTINE

n+0	CE	LDA I	
n+1	80		SETS INDEX REGISTER ON ACIA
n+2	04		
n+3	86	LDA I	
n+4	03		MASTER RESET ACIA
n+5	A7	STA X	
n+6	00	(8004)	
n+7	44	LSR A	
n+8	A7	STA X	STORES A0I IN ACIA CONTROL REGISTER FOR TTY (11 BITS)
n+9	00	(8004)	
n+A	A6	LDA X	
n+B	00	(8004)	
n+C	A1	CMPA X	READS ACIA STATUS AND COMPARES IT TO LOCATION 8006
n+D	02	(8006)	
n+E	27	BEQ	IF EQUAL LEAVE ACIA PROGRAMMED FOR TTY
n+F	04	(n+14)	
n+10	86	LDA I	
n+11	09	RS232 CONTROL WORD STA X	IF NOT PROGRAM ACIA FOR IO BIT OPERATION
n+12	A7	(8004)	
n+13	00		



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CIRCLE NUMBER 206

Stable constant-voltage supply uses current source to establish reference

The circuit shown employs a FET and an op amp to achieve low output resistance, high supply rejection and a low temperature coefficient (TC). A 7.5-V avalanche diode is used only to force the circuit into the correct mode at switch-on, so the circuit is free of avalanche noise.

The FET, Q_1 , is a low pinch-off p-channel device. It serves as a current source for reference current I_c , which establishes a reference voltage across R_x . A variable resistor, R_1 , can adjust the gate-source voltage of Q_1 to a region of its characteristic curve where its drain current doesn't vary significantly with temperature. Over a limited temperature range, R_1 can be adjusted to compensate for the TC of both the op amp and the circuit resistors by operating the FET in a region where its current changes are in opposition.

The reference current typically is less than 1 mA, and doesn't appreciably reduce the available output current. A common op amp, such as a 741 or a 101, can source and sink 3 mA as well as provide sufficient gain to attain a load coefficient of less than $10 \mu\text{V}/\text{mA}$ for the regulator circuit.

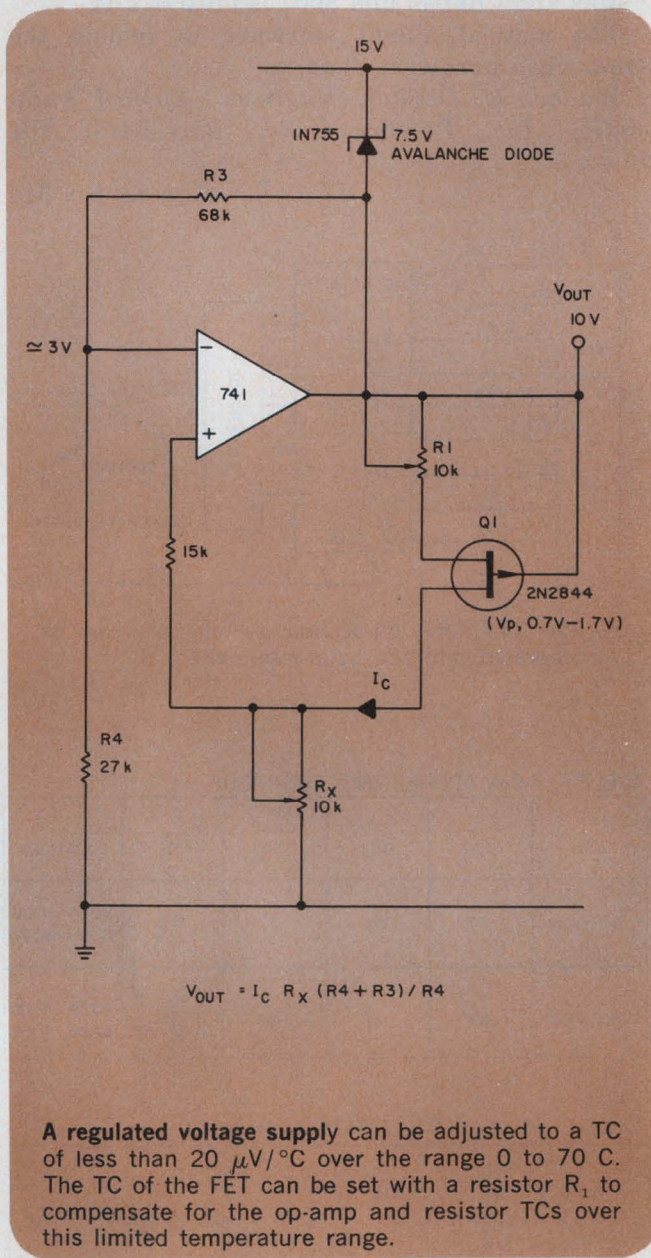
Because the FET is terminated between two constant-voltage points, the regulator's voltage coefficient is less than $10 \mu\text{V}/\text{V}$. Also, an over-all TC of less than $20 \mu\text{V}/^\circ\text{C}$ can be achieved over the temperature range of 0 to 70 C.

With op amps that were selected at random, and not particularly for low noise, a noise voltage of only 20 to 30 μV rms was measured in a noise bandwidth of 10 Hz to 10 kHz.

A convenient alternative to the FET is the recently introduced Siliconix CR068 current-regulator diode. The diode passes 680 μA and features a typical TC of $0.02\%/^\circ\text{C}$.

John A. Roberts, Senior Engineer, Computing Devices Co., P.O. Box 8508, Ottawa, Ontario, Canada K1G3M9.

CIRCLE No. 315



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More efficient diode developed by Siemens

New double-drift Impatt diodes with outputs of 3 W at 7 GHz are expected to be applied where semiconductors hitherto have not been used—i.e., in radio relay systems. Developed by Siemens, West Germany, these diodes have relatively high efficiencies of 11% and result in high outputs. The diode's case contains four mesas, which are mounted on a silver heat sink that can handle thermal losses of up to 30 W. But only two of the four mesas are actually bonded to the heat sink, and these two are selected only after extensive performance tests on the multi-mesa

configuration. The result of this approach, says Siemens, is a high-efficiency diode.

Fabricating a double-drift Impatt diode requires such advanced techniques as multilayer epitaxy and ion implantation. The diode's two drift regions are accurately matched to the resonant frequency. Electrons pass through an n-type region, while holes pass through a p-type region.

Further improvements, predicts Siemens, will lead eventually to 10-W devices and will displace traveling-wave tubes in many applications.

vehicles located in bad-reception areas. Error-correcting codes known to reduce the error rate considerably can do nothing in this situation.

A combination of error-correcting codes and sideband diversity transmissions might give the best possible results for data transmission, according to Professor Gash-ing, head of the Bath Electronics School.

'Sideband diversity' cuts transmission-error rate

A 10⁴ improvement in the data transmission error rate has been achieved with an experimental mobile radio system using "sideband diversity," a data-modulation method developed at Bath University, England.

The new method, which can be used for speech transmission as well, has been tested by placing three fixed transmitters about 15 miles apart. Vehicles equipped with the special receiving equipment (also developed at Bath) and traveling in areas of varied terrain have obtained signals with error rates of only 6.8×10^{-3} .

Sideband diversity can be operated with two or more transmitters. Identical signals are sent out from each transmitter, but the modulations on the transmitters are phase-shifted relative to each other.

In the three-transmitter experimental system, the modulators are phase shifted 120° with respect to each other, but this angle is not critical.

At the receiver, an amplitude comparator looks for the strongest sideband and automatically selects the strongest part of the signal. This selection ensures that any interruption in the signal that might occur because of the terrain will not result in a total loss of signal at the receiver. At least one sideband of the signal will always get through to carry the transmitted information.

The results of the trials conducted so far have shown that errors are almost random, with only slight variations caused by terrain.

One advantage of the sideband-diversity method is that it overcomes the problem of stationary

Acoustic wave oscillator works at high frequency

An acoustic-wave oscillator developed by Thomson-CSF is said by the company to exhibit noise and short-term stability characteristics on a par with those of resonating bulk-crystal types—but without the latter's upper-frequency limitation.

The fundamental acoustic-wave oscillator operates from 100 to 800 MHz, and work is in progress to push the upper limit up to 2 GHz. Combining this oscillator with a frequency multiplier can produce signals of up to 10 GHz.

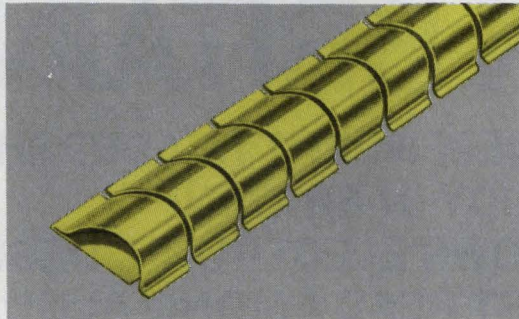
To provide acoustic-wave oscillation, an acoustic-wave delay line is connected in the feedback loop of an amplifier adjusted to yield a net loop gain greater than unity.

Unlike a conventional, crystal-controlled oscillator, the acoustic, delay-line control element does not resonate. Its operating frequency and mode selection are determined by delay-line parameters, which provide design flexibility.

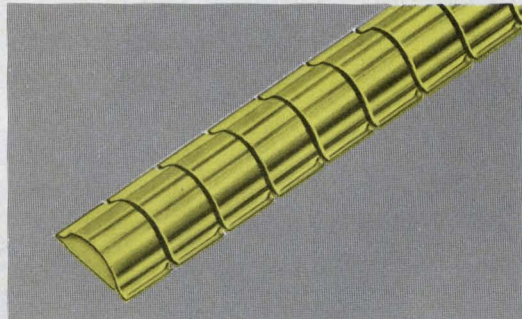
Long and short-term stabilities of 1 in 10⁻⁵ and 1 in 10⁻⁶ parts per year, respectively, have been demonstrated. The noise figure is -120 dB/Hz, with respect to the fundamental. Output power up to +20 dBm is possible as well as the ability to modulate frequency.

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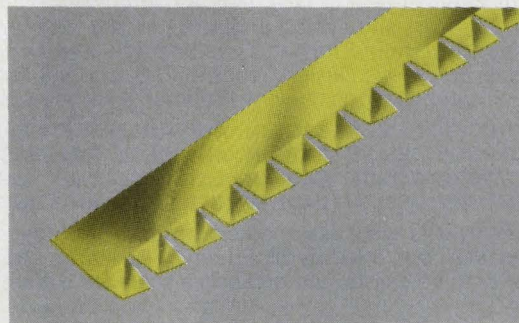
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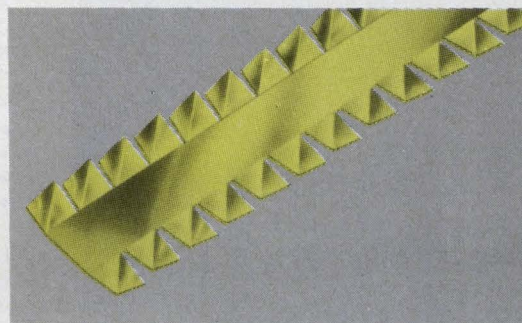
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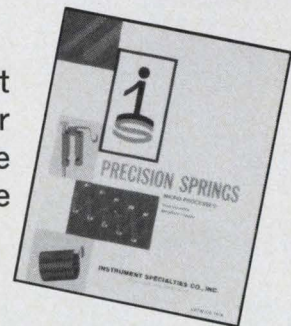


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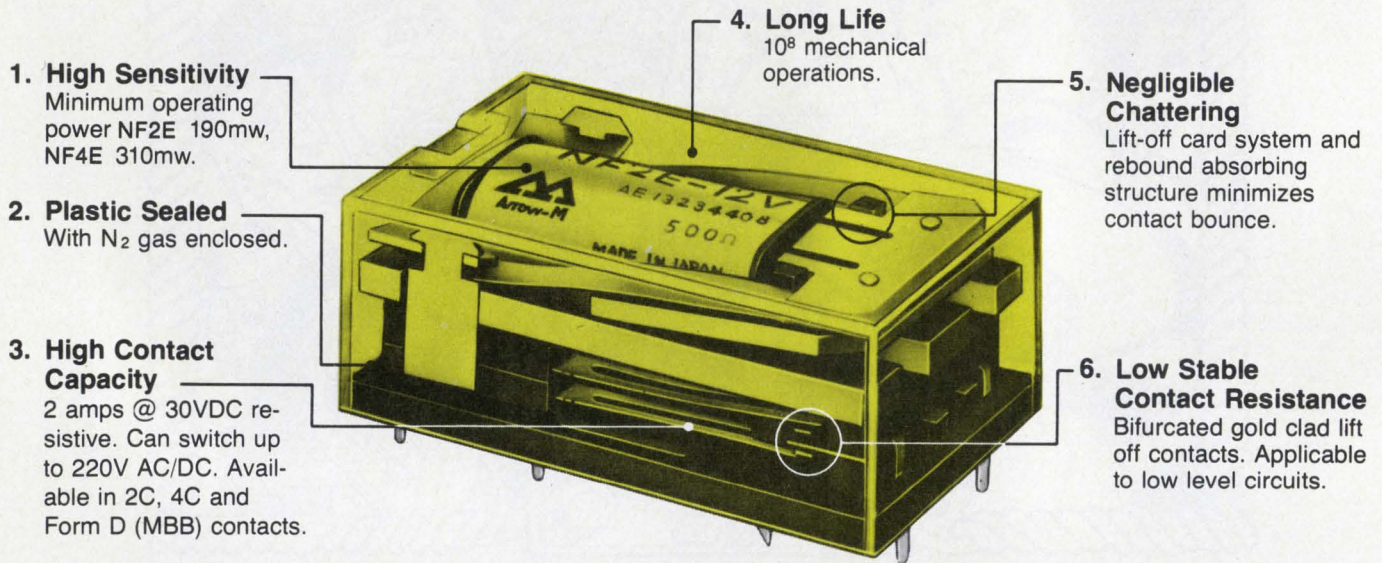
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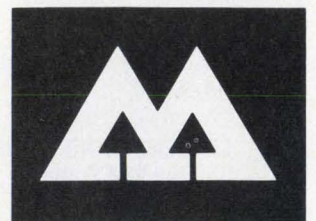
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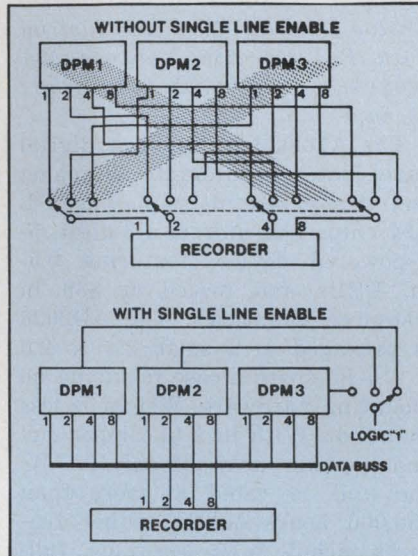
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The adapter modules attach to the rear of the DPM and condition the input signal. All adapters are interchangeable with either of the basic DPMs. By changing the adapter, you can shift, say, from thermocouple temperature measurements to scaled-and-offset millivolt readings.

With the three-state logic BCD, or single-line enable, you can hook up any number of outputs in parallel on a common data bus. Then, by energizing a single TTL-compatible control line, you can call up coded output data from any instrument (see illustration). Thus cumbersome external switching of many BCD lines is avoided.

The comparator building block,



an internal PC board, watches for alarm conditions, and it can monitor any number of points. Alarms are "sounded" by relay closure or by a logic-level output when a predetermined, programmable limit is exceeded.

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Prices of the basic DPMs run from \$139 to \$229, the adapter ranges from \$79 to \$170, and the comparator sells for \$129 (2770) or \$149 (2780). The single-line enable feature costs \$60 in the 3-1/2-digit 2770 and \$75 in the 4-1/2 2780.

CIRCLE NO. 305

Unit shows single events to ± 100 -ps resolution

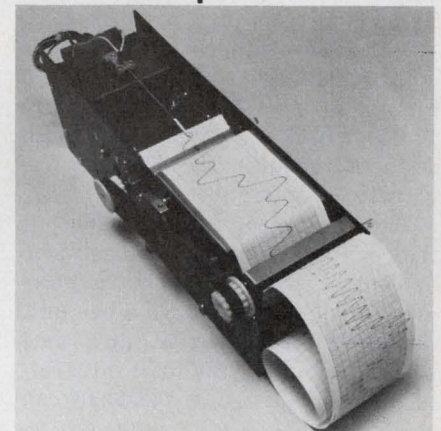


Eldorado, 2495 Estand Way, Pleasant Hill, CA 94523. (415) 682-2100. \$4850; 12 wks.

Model 797 time-interval meter is specifically designed for single-event measurement and provides an accuracy and resolution of ± 100 ps throughout the measurement range of 0 to 999,999,999.9 ns. In addition to measuring the time interval between two separate pulses, the 797 measures the width of a single pulse or one period of a repetitive signal. The start and stop points can be independently controlled so that pulse parameter or waveform measurements can be made. In a programmable system, the 797 can be sequenced to measure rise time, pulse width, and period. BCD or IEEE Std 488-1975 (GPIB) and remote programming are available.

CIRCLE NO. 320

Chart recorder operates from 12-V power source



Astro-Med, Atlan-Tol Industrial Park, West Warwick, RI 02893. (401) 828-4000. \$425; 2 wk.

A single-channel chart recorder operates directly from a 12-V-dc power source. The recorder, Model 102 XLA, takes 6 W of power. It provides an accuracy of 0.5% of full scale and meets the frequency-response specifications of the American Heart Association. The 102 XLA uses no ink; it writes on thermal paper. The trace width is 50 mm. The recorder dimensions are 4 x 6 x 6.25 in.

CIRCLE NO. 321

INSTRUMENTATION

Digital integrator reads watt or amp-hours



Yokogawa Corp. of America, 5 Westchester Plaza, Elmsford, NY 10523. (914) 592-6767. \$1200.

With energy conservation on everyone's mind these days, a digital integrator that keeps track of watt-hours or ampere-hours is right in tune with the times. The Model 2513 from Yokogawa attaches to the company's 2504 digital ac meter and provides a 6-digit display of any equipment's energy consumption.

Resolution of the 2513 always matches that of its companion. If the 2504 (which measures true-rms voltage, current and power) is set to resolve 0.1 W, the integrator will resolve 0.1 W-h. The combined accuracy of the sister meters is about 0.35% of full rated input. Repeatability is 0.1% or better.

The 2513's integration time runs from about 100 to 833 h at rated input, so the top readings are 10,000 kW-h or 10,000 A-h. With dc-input modules, the 2513 can integrate dc current as well.

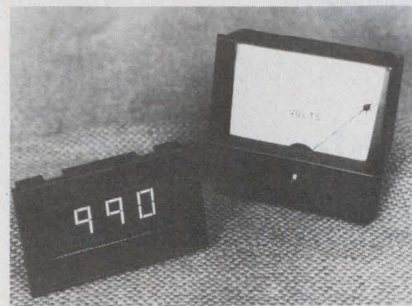
The integrator has BCD output that can be used in a feedback loop to control current flow in a process-control application. The unit can be interrogated at any time without affecting the total integrated value. Addressing the 2513 can be accomplished manually or remotely with a rear connector.

Operation is simple. Three front-panel pushbuttons are used to start, stop or reset the unit. Range of the 2504 varies from 15 W fs (30 V, 0.5 A) to 12 kW fs (600 V, 20 A) so that almost any equipment can be monitored. Five input modules provide single or multi-range operation or combined dc and ac operation.

The 2513-2504 combination prices out under \$4000, depending on the choice of input plug-in. Delivery takes 6 to 8 weeks.

CIRCLE NO. 304

Compact DPM aims at analog meter market



Analog Devices, Route 1 Industrial Park, P.O. Box 280, Norwood, MA 02062. (617) 329-4700. \$39 (100s); 30 days.

The AD2026 is the first digital panel meter to integrate all analog and digital circuitry on one I²L LSI chip. The unit is a 3-digit, 5-V-powered device, featuring 0.5-in. LEDs and priced at \$39 in 100-piece quantities. The AD2026 is packaged in a small 3.4 × 2.0 × 0.7-in. snap-in case requiring no mounting hardware. Weight is less than 2 oz. With just 14 components and a power draw of only 0.6 W, the unit is rated at more than 250,000 hours MTBF. Other features include 0.1% accuracy, full-scale range of -99 mV to 999 mV, bias current of 110 nA, balanced differential input and overvoltage protection of ±15 V dc. Gain tempo is 50 ppm/°C and zero tempo is 10 μV/°C.

CIRCLE NO. 322

Logic analyzer accepts 16 channels

Biomation, 10411 Bubb Rd., Cupertino, CA 95014. (408) 255-9500. \$5000; 30-60 days.

Model 1650-D, a 16-channel, 50-MHz logic analyzer, is functionally similar to the company's 851-D eight-channel unit. The 1650-D can freeze the input signals in its 16 × 512-bit memory. The unit then displays the stored data in a 16-line timing-diagram format on a CRT display or oscilloscope. Also offered is an accessory, the 116 display control, which expands the unit into a full data-domain analyzer. The display control produces a truth-table data format, complete with hex or octal characters, plus a vector-map display format and data-compare function.

CIRCLE NO. 323

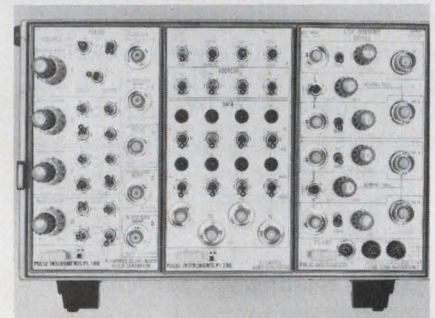
4-terminal probes test PC boards

Electro Scientific Industries, 13900 N.W. Science Park Dr., Portland, OR 97229. (503) 641-4141. \$95; stock to 60 days.

You can use these probes for making four-terminal resistance measurements on microcircuits. Small enough to probe a pad of 20 mils square, they are useful for checking PC board stripes as well as components. The probe tips are spring loaded into a pen-sized holder. They can be used for extremely low-ohm measurement at high accuracy because a true four-terminal technique, which eliminates lead resistance effects, is employed. Slivers on printed circuit boards, shorts in ICs and open conductor stripes under dual-in-line packages can be detected with these probes, when used with the company's Model-1700 digital ohmmeter. These probes are also useful for resistance measurement of physically large parts such as rods and cable couplings.

CIRCLE NO. 324

Instruments compatible with TM-500 line



Pulse Instruments, P.O. Box 1655, San Pedro, CA 90733. (213) 541-3204. PI-100, \$695; PI-200, \$850; PI-400, \$595; January to March, 1977.

Three plug-in units are designed to fit the Tektronix TM-500 series of modular instruments. The units are the PI-100 four-channel, 50-MHz delay width clock generator; the PI-200 four-channel × 32-bit, 50-MHz word generator; and the PI-400, a four-channel, 5-V interface driver with ±5-V offset. The units are intended for high-speed digital and analog testing applications. When used together they form a compact, but expandable, multichannel signal source system.

CIRCLE NO. 325



**You'll like
Burr-Brown's
one word price story...
Down.**

You've always expected high quality from Burr-Brown. Now you can expect Burr-Brown to keep your costs down, too. Take a look at the prices of these high quality Burr-Brown units:

ADC 80: Lowest priced hybrid 12 bit A/D on the market. ADC 80 is complete with clock, comparator and reference, and is especially applicable in designs where space is crucial. With a conversion speed of 25 μ sec, price is only \$47.50 (in 100's).

DAC 80: 12 bit DAC's price cut by half. The DAC 80 is a truly self-contained D/A converter with guaranteed monotonicity. It includes internal reference source, output buffer amplifier, maximum non-linearity of $\pm 1/2$ LSB, and a price of only \$19.50 (in 100's).

3650/3652 Isolation Amp: Breakthrough in price and size. Thanks to a new optical coupling technique, you now have a low cost alternative. Under one cubic inch in volume, the 3650HG, with 0.3% gain non-linearity and 1500V continuous isolation is only \$26.50 (in 100's).

3626 Instrumentation Amp: Modular performance at lower cost. The laser-trimmed 3626 family offers the performance you need. Input offset drift as low as 1 μ V/ $^{\circ}$ C at G = 1000, <2 μ V/ $^{\circ}$ C at G = 5, gain non-linearity is 0.01%. Prices start at \$13.00 (in 100's).

4127 Log Amp: Low-cost solution to signal processing problems. 4127 is the first hybrid log amp to accept inputs of either polarity—up to 4 decades of voltage or 6 decades of current input. It functions as a logarithmic, log ratio, or antilog amplifier, and is only \$26.00 (in 100's). **Five circuits**—typical examples of Burr-Brown's commitment to cost savings. Over the past year, Burr-Brown has cut prices on a substantial number of products, some by more than 50%.

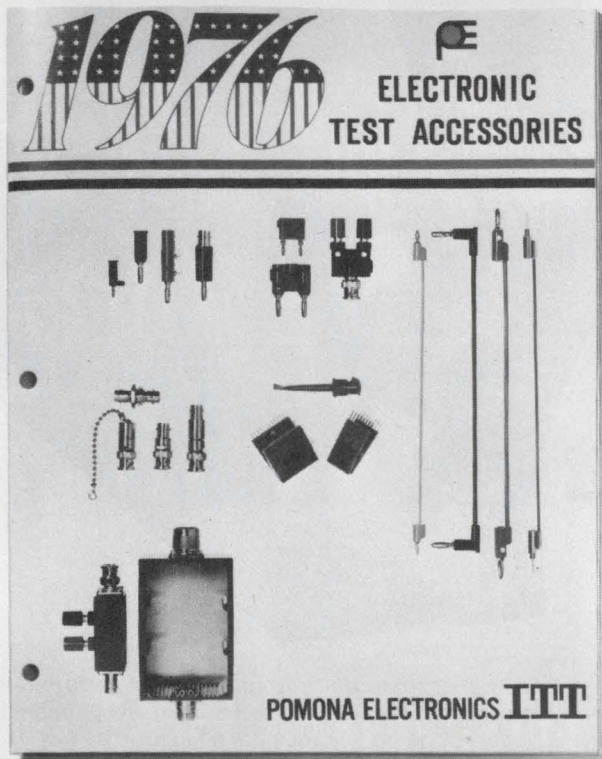
To find out more on how Burr-Brown can help you meet those crucial cost vs. performance specifications, write or call: Burr-Brown, International Airport Industrial Park, Tucson, Arizona 85734. (602) 294-1431.



**Still at the top,
except in price**

CIRCLE NUMBER 92

MEET OUR FAMILY OF ELECTRONIC TEST ACCESSORIES



This new General Catalog is our latest family portrait. In the past twenty-five years (1976 is our Silver Anniversary year) it has grown from a handful of items to almost 500 products for the electronics industry.

Our catalog has grown to 76 pages for 1976, and we are introducing 65 new items this year. It describes and illustrates every member of our family. You're bound to find the solution to your testing problem with one or more of these quality products.

For your free copy, circle the reader service number listed below, or write:

IIT POMONA ELECTRONICS

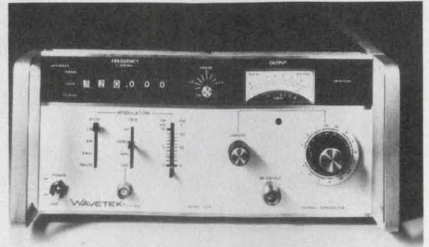
1500 East Ninth St., Pomona, Calif. 91766
Telephone (714) 623-3463, TWX: 910-581-3822



CIRCLE NUMBER 93

INSTRUMENTATION

Phase locked sig gen costs only \$2600



Wavetek Indiana, 66 N. First Ave., Beech Grove, IN 46107. (317) 783-3221. \$2600.

Model 3001 signal generator operates from 1 to 520 MHz and is phase-locked in the FM mode. Built-in frequency programmability is standard. An optional external reference input enhances the unit's accuracy of $\pm 0.001\%$. Stability is rated at 0.2 ppm/h. A 5×10^{-9} /day stability option is available. Price of the 3001 is said to be about half that of other phase-locked units.

CIRCLE NO. 326

PCM-link tester spans 5 Mbit/s range

EMR-Telemetry, P.O. Box 3041, Sarasota, FL 33578. (813) 371-0811. \$6000.

EMR's Model 721 bit-error-rate tester provides complete end-to-end performance testing of communication links, tape recorders, bit synchronizers, or any PCM system having a bit rate within 1 bit/s to 5 Mbit/s. Two basic data patterns are generated: (1) a 16-bit word with each bit front panel selectable and (2) a 2047-bit pseudorandom word. With either pattern, frame length is selectable from one to 512 words per frame, in increments of powers of two. A bit-blanking function is provided for bit synchronizer flywheeling or coasting measurement. An internal counter and front-panel display counts bit errors and gives clock slippage and acquisition periods. Jitter simulation is provided by an internal voltage-controlled oscillator. Other tests include threshold level, transition density, pattern sensitivity, capture and tracking limits and loop-width performance.

CIRCLE NO. 327

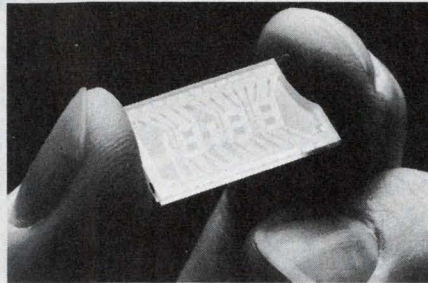
Electronic glass. All you need is vision.

Here is a designer's dream come true. Minimum form with maximum function.

It's PPG's electronic glass.

It lets you combine the sleek, simple elegance of glass and the dazzling magic of solid-state technology.

Which means you can literally change the faces of



Digital watches will never be the same. Electronic glass can make them more efficient and more affordable.

appliances, timepieces, visual displays, and instrumentation of every description.

The secret is the permanent conductive metallic-oxide coating on the glass.

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In short, if it can be done electronically, it can probably be done a little better with electronic glass.

And, since the coating can be applied to form letters, numbers, or any visual display imaginable, there's almost no end to what you can do.

Digital clocks, wristwatches, speedometers, odometers, oscilloscopes, and radar screens are just a few of the obvious possibilities.

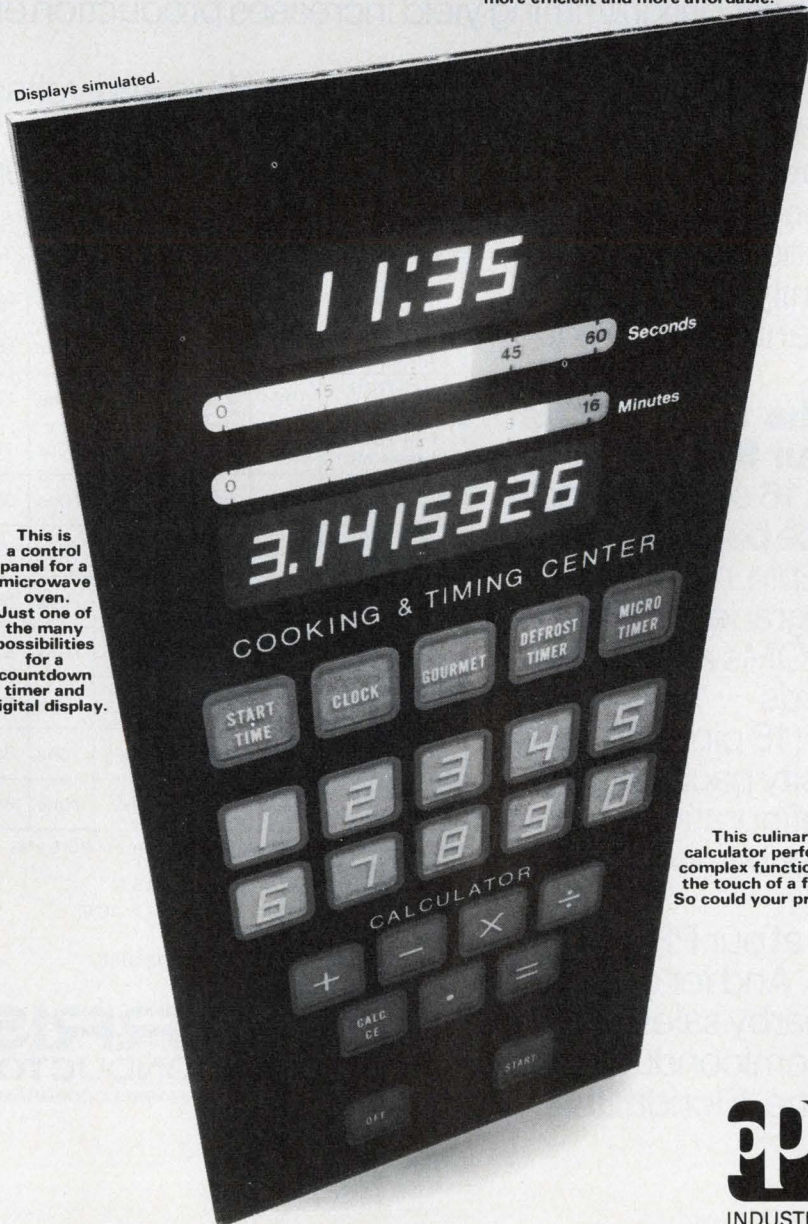
As for its reliability, there's really nothing to go wrong. No moving parts. No knobs, dials, switches, buttons—just glass.

It's here. It's now. It's ready. All it needs is you, and all you need is the vision to use it.

So test your vision. Send the coupon today.

Displays simulated.

This is a control panel for a microwave oven. Just one of the many possibilities for a countdown timer and digital display.



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Company _____

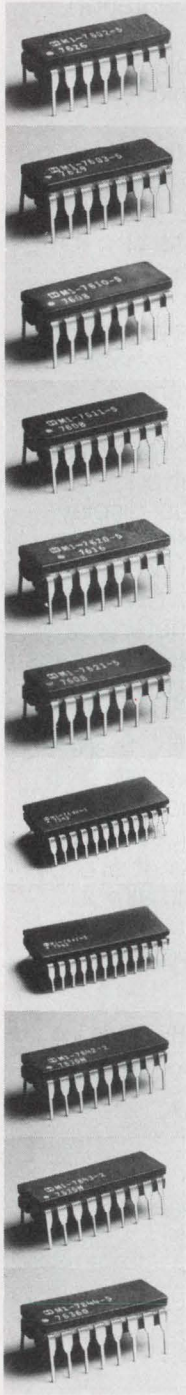
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Why Do More Top Designers Insist On Working With Harris Generic PROMs?



The compatibility and depth of our Generic PROM family simplifies selection, application, and production. But that's only the beginning. Here are a few specific reasons for choosing Harris.

- ✓ Identical programming specifications means that one programmer programs the entire family.
- ✓ Single pulse one millisecond per bit programming achieves fast programming and superior reliability.
- ✓ Industry's highest programming yield increases production efficiency, regardless of PROM size.
- ✓ Access times are guaranteed over full temperature and voltage ranges and any random addressing sequence.
- ✓ Harris is the only JAN-38510 QPL-1 approved PROM supplier.
- ✓ Proven Nicrome fuse design and Schottky technology.
- ✓ Complete family availability from prototype quantities to production volumes.

Now See How The 1Kx4 PROM Can Improve Your System.

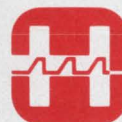
- ✓ High-density 16 or 18 pin packages greatly reduce board area.
- ✓ HM-7644 (16 pin, no enables) provides direct upgrade for systems using 1K or 2K PROMs and having less than 1024 words.
- ✓ HM-7642/43 (18 pin, 2 enables) extends high density packaging to large memory configurations.
- ✓ Low power per bit: ($I_{CC} < 140$ ma or $< 180 \mu W/bit$).

For a quick look at our PROM family check the chart. And for complete details call your nearby sales location or write to Harris Semiconductor, P.O. Box 883, Melbourne, Florida 32901.

Device #	No. of Bits	Organi- zation	No. of Pins	Max. Access Time*	
				Com.	Mil.
HM-7602 (open coll)	256	32x8	16	40ns	50ns
HM-7603 (three state)	256	32x8	16	40ns	50ns
HM-7610 (open coll)	1024	256x4	16	60ns	75ns
HM-7611 (three state)	1024	256x4	16	60ns	75ns
HM-7620 (open coll)	2048	512x4	16	70ns	85ns
HM-7621 (three state)	2048	512x4	16	70ns	85ns
HM-7640 (open coll)	4096	512x8	24	70ns	85ns
HM-7641 (three state)	4096	512x8	24	70ns	85ns
HM-7642 (open coll)	4096	1024x4	18	70ns	85ns
HM-7643 (three state)	4096	1024x4	18	70ns	85ns
HM-7644 (active pullup)	4096	1024x4	16	70ns	85ns

*Access time guaranteed over full temperature and voltage range.
 Industrial ($T_A = 0^\circ C$ to $70^\circ C$, $V_{CC} \pm 5\%$)
 Military ($T_A = -55^\circ C$ to $125^\circ C$, $V_{CC} \pm 10\%$)

Proven PROM Capability



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MARYLAND: Lanham (301) 459-1556

MASSACHUSETTS: Burlington (617) 273-1313

MICHIGAN: Farmington (313) 476-2446

MISSOURI: Hazelwood (314) 731-5799; Independence (816) 737-1100

NEW JERSEY: Keasbey (516) 567-5900; West Caldwell (516) 567-5900

NEW MEXICO: Albuquerque (505) 265-5655

NEW YORK: Albany (518) 489-7408 or 4777; Huntington Station (516) 567-5900

NORTH CAROLINA: Winston-Salem (919) 722-5151

OHIO: Cleveland (216) 831-8292; Dayton (513) 890-2150

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SOUTH CAROLINA: Greenville (803) 268-1125

TEXAS: Dallas (214) 691-4592; Houston (713) 661-3007

VIRGINIA: Charlottesville (804) 973-6672

WASHINGTON: Bellevue (206) 454-0300

CANADA: Mississauga (Toronto) (416) 676-1042, (416) 678-0401; Montreal (514) 626-6723, (514) 389-8051; Ottawa (613) 749-0740, (613) 226-3491

INSTRUMENTATION

**Logic clip eases
debugging of logic cards**



Micro, 10888 N. 19th Ave., Phoenix, AZ 85021. (602) 997-5931. \$40,000 to \$60,000; 2-4 wk.

The Magiclip system, with guided clip/probe, enables production workers to troubleshoot logic boards with a minimum of time and training. To locate a fault, the operator simply follows simple instructions which automatically appear on the CRT. The system rapidly detects faults to chip, node or run level. Magiclip is an option of the 6500 test/programming station, a modular turnkey system, which enables users to generate board-test programs in-house and perform comprehensive testing and troubleshooting. Optional peripherals include high speed printer, console with dual floppy discs, high speed paper tape punch/reader, card reader, CRT and keyboard, Magiclip guided clip/probe and 500-series test head.

CIRCLE NO. 328

**Scope trace drawn on
strip-chart recorder**

Gould Advance Ltd., Roebuck Rd., Hainault, Essex, England.

An output module, the 4001-1, for the company's OS4000 digital-storage scope, provides automatic printout of a trace onto a strip-chart recorder after an input has been stored. On receipt of a transient, the scope stores the input and switches to a "stored" condition. Immediately, the output unit switches to the printout condition and at the same time selects a predetermined speed for the recorder in use. Front-panel contacts start the strip-chart motor, and a single sweep is plotted. At the end of the sweep the scope automatically reverts to the primed condition, ready to accept, and then plot, a further input.

CIRCLE NO. 329

**Lightweight scope
features multiplication**



Philips Test & Measuring Instruments, 400 Crossways Park Dr., Woodbury, NY 11797. (516) 921-8880. \$3395.

A built-in 40-MHz multiplier and comprehensive storage facilities are features of a new, lightweight, 50-MHz scope. The PM-3243 has two channels with 5-mV sensitivities and both the product and one of the original signals can be displayed simultaneously. Variable persistence and variable storage allow the study of single-shot events. The use of a direct conversion power supply allows operation from almost any voltage or frequency, including dc, without switching. Any ac supply between 90 and 264 V from 46 to 440 Hz or any dc supply between 100 and 200 V suffice. Power consumption is 39 W.

CIRCLE NO. 330

**Ultracompact DMM
fits in attache case**



John Fluke Manufacturing Co., P.O. Box 43210, Mountlake Terrace, WA 98043. (206) 774-2211. \$250; 7 wks.

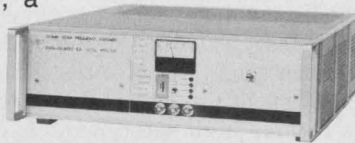
Model 8030A DMM is designed for service and maintenance applications and is said to be the first 3-1/2-digit instrument to offer features such as true rms ac voltage and current measurements and diode testing. The compact design lets the unit be easily carried in a tool kit or attache case. The diode measurement feature permits the forward drop (in millivolts) across a diode or transistor to be checked, with the semiconductor junction biased at 1 mA. Dc accuracy is $\pm 0.1\%$ of reading +1 digit.

CIRCLE NO. 331

The smaller, lighter self-contained Cesium Frequency Standard

...from OSCILLOQUARTZ

one of the world's largest and most technically competent manufacturers of quartz crystal oscillators, comes this new Primary Frequency Standard. Now, a new source of precision time and frequency generation and measurement systems plus a new standard of reliability and operating simplicity. Most competitively priced.



It is complete — with 110/220 VAC and 24 VDC Power Supplies, a 5-hour Internal Standby Battery, Monitoring and Control Devices — in a 19" rack with 1, 5 and 10 MHz outputs on front and rear.

Heart of this self-contained Primary Standard is the compact cesium beam tube developed by Frequency & Time Systems to permit the exceptional performance-to-size ratio of the Model 3200. ALSO NEW—the Oscilloquartz low-cost Model 3000 Cesium Beam Frequency Source in 1/2 ATR Rack Size.

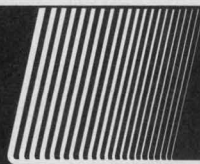
Complete engineering and performance specifications available on Model 3200 Cesium Frequency Standard and Model 2200 Quartz Frequency Standard and Clock.

Write: 182 Conant St., Danvers, MA 01923 or call (617) 777-1255
TELEX 94-0518

MODEL 3200

Accuracy (0°C to +50°C)	$\pm 1 \times 10^{-11}$
Reproducibility	$\pm 5 \times 10^{-12}$
Stability	$\pm 2 \times 10^{-13}$
Outputs	1, 5 & 10 MHz
Power Supplies	110/220 VAC $\pm 10\%$ primary (45 - 440 Hz) 20 - 30 VDC (floating) secondary
Standby Battery	5 hrs at 25°C (fast charging)

"A STEP AHEAD ... IN TIME"

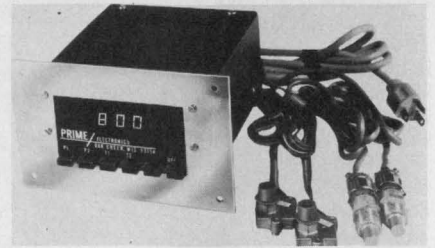


Frequency and Time Systems

CIRCLE NUMBER 96

INSTRUMENTATION

Digital unit reads pressure and temp



Prime Manufacturing, 7730 S. 6th St., Oak Creek, WI 53154. (414) 764-1400. \$400 to \$700; 4-7 wk.

The Model 769 digital gauge accurately measures both pressure and temperature from a single self-contained unit. The gauge measures absolute pressures up to 999 lb/in², with a $\pm 0.5\%$ variation over the entire range. And it measures temperatures up to 999 F with variations of $\pm 0.1\%$ over the range. The unit contains four probes for any pressure and temperature combination. Buttons on the display-front select one of the four sensors being monitored. Probes are easily installed and can be equipped for remote use, up to 200 ft, without loss of accuracy. Probes are available for almost any media. The unit has a zeroing button to check the system's calibration. It has an easily read display which accommodates rapid changes in pressure or temperature.

CIRCLE NO. 332

4-1/2-digit DMM ranges automatically

John Fluke, P.O. Box 43210, Mountlake Terrace, WA 98043. (206) 774-2211.

The 8040 is an ultracompact 20,000-count multimeter with five measurement facilities, autoranging and autozero. The design enables the unit to be carried conveniently in an attache case or as part of a service kit. Measurement capabilities include dc voltages from 200 mV fs to 1100 V fs, to an accuracy of $\pm 0.05\%$ of reading +2 digits; and ac voltages from 200 mV fs to 750 V fs using a true-rms conversion technique, to an accuracy of 0.5% of reading +10 digits. True rms is also used on ac-current ranges.

CIRCLE NO. 333

CRT YOKES FOR FLIGHT

Take a plane -military, commercial, or private. Chances are 9 out of 10 you'll find Syntronic Deflection Yokes and Focus Coils in critical cathode ray tube display equipment; weather radar, navigation, weapons systems, landing, monitoring, communicating. The U.S. Navy's/Lockheed S3A anti-submarine plane uses 14 Syntronic components in 7 critical displays.

Other aircraft display applications include the B52 Retrofit, F4 (D&E), F5E, A6, A7, F111, A10A, S3A, F14, F15, F16, AWACS, MCRA, Mirage, Viggen, 707, 727, 737, 747, DC-8, DC-9, DC-10, L1011 and many private aircraft. Call or write Syntronic Instruments, Inc. (312) 543-6444. Ask for Syntronic's Yoke Selection Guide to high-flying, high-performance yokes.




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SYNTRONIC INSTRUMENTS, INC.
100 Industrial Road • Addison, IL 60101
(312) 543-6444

IC tester checks DIPs at 1.3-MHz rate

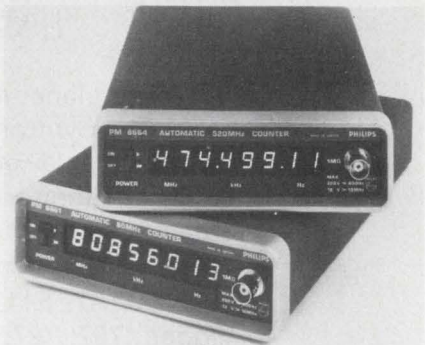
Biomation, 10411 Bubb Rd., Cupertino, CA 95014. (408) 255-9500. \$4500; 60 days.

Model 2400 benchtop digital IC tester is designed for those who use small quantities of many dif-

ferent digital IC types. The 2400 is primarily a functional tester with a test rate of up to 1.3 MHz. It is completely operator programmable and will handle a wide variety of ICs with up to 24 pins, including CMOS, NMOS, ECL and all TTL families, plus open-collector and three-state output devices. The price represents the cost of a 16-pin unit including a program library for over 1000 different devices. Model 2400 also measures some parametric values.

CIRCLE NO. 334

Counter line features 10 new models



Philips Test and Measuring Instruments, 400 Crossways Park Dr., Woodbury, NY 11797. (516) 921-8880. PM6661, \$325; PM6664, \$625.

A bunch of brand new timer/counters, universal counters and automatic frequency counters mark the company's attempt to capture a large chunk of the market for frequency/time-measuring products. Included are three timer counters, covering 80, 520 and 1000 MHz (PM6620 series), four universal counters (PM6610) and two automatic frequency counters, with an on-off switch as the only control. Both the 80-MHz PM6661 and the 520-MHz PM6664 offer automatic triggering, noise suppression, range selection and leading-zero blanking. The timer/counters feature nine digits, 20-mV sensitivity and resolution as low as 1 ns.

CIRCLE NO. 335

DMM uses LCDs, reads temperature, too



Gould Advance, Roebuck Rd., Hainault, Essex, England.

The Beta is a portable, battery-operated 3-1/2-digit multimeter using a large, liquid-crystal display and a single CMOS IC chip for all analog and digital functions. Among the Beta's 29 ranges is a 10 A ac and dc current range via a separate input, plus temperature-measurement capability with direct reading between -20 and 120 C. Beta operates for over 300 h from four C cells.

CIRCLE NO. 336

New from Standard Grigsby



P/relTM

the programmable rotary encoded logic switch everyone will be talking about...

... because no other rotary switch has as much versatility with as low a cost as Standard Grigsby's P/rel switch!

The economy is twofold. This switch not only lends itself to full automation, but installed costs are lower by the use of our printed circuit terminals (solder terminals are also available).

A specially processed printed circuit disc is fully

programmable to the truth table of any code. We provide 100% program disc inspection to customer specifications. Up to 60 detent positions are available with our new double ball Dual FlexTM detent. And, the use of concentric shafts allows up to 120 detent positions from a single switch!

Everyone will be talking about P/rel . . . so will you!

Send for your free "Yes" button and literature.



standard grigsby, inc.

920 Rathbone Avenue, Aurora, Illinois 60507, Phone (312) 897-8417

CIRCLE NUMBER 98

Some people just can't leave well enough alone.

Last March, while the other guys were making promises, Advanced Micro Devices was making Am9130's and Am9140's—the first family of 4K static RAM's.

Terrific. Everyone loved them. But were we satisfied? Did we stop there? No.

Advanced Micro Devices announces the 1Kx4/4Kx1 Am91L30/L40, low-power versions of our Am9130/40.

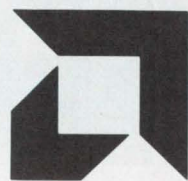
These new circuits provide access times down to 250 nanoseconds with power dissipation of only 367mW. That's half the power of the original. (And that's the same power

as the industry standard 1K static RAM. You're getting four times the memory for the same power. Wow!)

There's more. These beauties do everything on a 5-volt power supply. The logic levels are identical to TTL. You get all the features of the original, including full military temperature range availability and, as always, MIL-STD-883 for free. Plus: a freshly minted set of application notes and data sheets awaiting your call, wire or letter.

Some people just can't leave well enough alone.

Advanced MOS/LSI



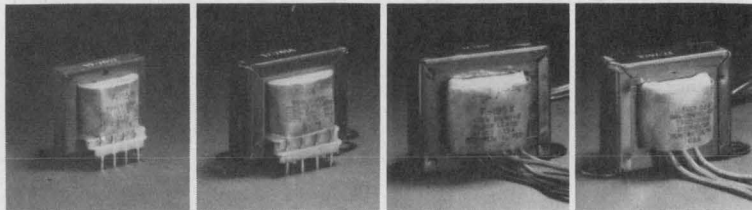
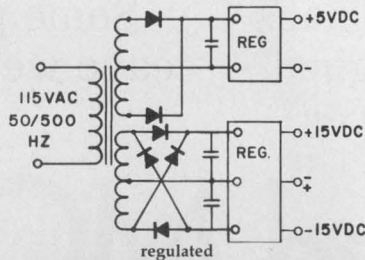
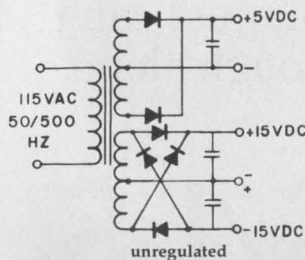
Advanced Micro Devices • 901 Thompson Place, Sunnyvale, California 94086 • Telephone (408) 732-2400 •
Distributed nationally by Hamilton/Avnet, Cramer and Schweber Electronics.

CIRCLE NUMBER 99



New Power Transformers For +5V and $\pm 15V$ Triple Output Five Plug-ins Five With Standard Leads

Triad has five new plug-ins and five units in open construction with leads for logic and op-amp power supplies—either regulated or unregulated. Dual secondaries of 9VCT and 24VCT, or 15VCT and 32VCT. Primaries, 115V, 50/500 Hz. Outputs: 1.5 W, 4.5 W, 7.5 W in plug-ins; 4.7 W, 20.3 W, 62 W, 92 W and 122 W in lead types. Specifically designed for "in-house" power supply construction where density packaging and flexibility are important. So call your distributor today for prices, delivery, technical information and Triad quality.



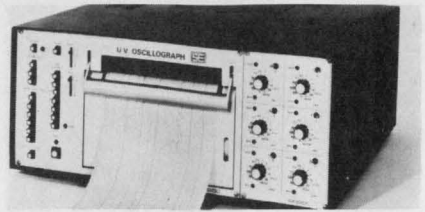
TRIAD-UTRAD
Litton Distributor Services

305 North Briant Street, Huntington, Indiana 46750

CIRCLE NUMBER 100

INSTRUMENTATION

UV outshines visible for oscillographs



EMI Technology, 20 Old Ridgebury Rd., Danbury, CT 06810. (203) 774-3500. From \$2000; stock to 30 days.

Unlike conventional light-beam designs, which sacrifice deflection to achieve wide bandwidth, series-SE6150 multichannel ultra-violet beam oscillographs feature writing speeds of 50,000 in/s, bandwidths of 0 to 10 kHz and deflections of more than 1.2 in. Each instrument in this series offers up to six recording channels, with access to galvanometers either directly or via built-in modular adjustable-gain drive-amplifiers which are calibrated directly in V/cm. Galvanometer modules (magnet blocks) are provided for up to 12 direct channels with 500-V-dc insulation, or up to six channels with 5 kV dc insulation. Modules are thermostatically stabilized at 45 ± 3 C for stability of sensitivity. Each instrument has auxiliary recording capabilities: to trace its own grids and timing lines over the full 6-in. width of the chart; to control trace and grid intensities; and to add reference markers and event markers. Timing intervals are selectable by panel push-buttons at 0.01, 0.1, 1, 10 and 100 s or may be controlled by external trigger. Twelve servo-regulated chart speeds from 0.008 to 39.37 in/s are selectable by panel push-buttons. Chart-drive linearity is $\pm 3\%$, in both automatic and continuous modes. The channel-amplifier panel-controls offer a selection of 10 attenuation steps, for sensitivities from 0.008 to 8 in/V, plus a 3:1 vernier adjustment. Input impedance is 10 M Ω up to 1 cm/V and 1 M Ω from 2 to 20 cm/V. The system frequency response is dc to 10 kHz (± 1 dB); noise and cross-talk are less than 0.2% of full-scale deflection. The instrument measures 17 \times 5 \times 18.5 in. and weighs 31 lb.

CIRCLE NO. 337

MHz	Service
4	RADIO NAVIGATION
	MARITIME MOBILE
10	AERONAUTICAL MOBILE
24	FIXED LAND MOBILE
25	C.B. - BUSINESS - GOVERNMENT
70	PUBLIC SAFETY
75	INDUSTRIAL
88	F.M.
100	COMMON CARRIER
170	TV - CATV
200	AMATEUR
215	FLIGHT LINE TELEMETERING
400	METEOROLOGICAL
450	LAND TRANSPORTATION
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960	UHF TV



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For under \$1200

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WB-713 SPECIFICATIONS

- Frequency Range — Band I: 1 to 500 MHz
Band II: 450 to 960 MHz
- Sweep Width — Bands I and II: 0.1 to 500 MHz
- Output: +10 dBm
- Flatness: ± 0.25 dB
- Distortion — Band I: -35 dB
Band II: -30 dB
- Residual FM: Less than 10 kHz
- Sweep Rate: 0.01 to 100 Hz variable
- Linearity: 1%
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Marker Tilt Control
Marker Clip Control
Marker Width Control from 20 kHz to 300 kHz
- Weight: 15 lbs.
- Size: 9" x 4 3/16" x 12 5/8"

Texscan has sweep generators covering from Audio to 2350 MHz. Please contact your local Texscan representative for a demonstration.

Texscan

Texscan Corporation 2446 North Shadeland Ave. Indianapolis, Indiana 46219 (317) 357-8781

CIRCLE NUMBER 101

INSTRUMENTATION

Low-cost pulser offers versatile operation

Viz Test Instruments Group, 335 E. Price St., Philadelphia, PA 19144. (215) 844-2626. \$119; stock.

Model WR549A pulse generator is continuously variable over a range of 5 Hz to 5 MHz, positive, negative, or pos/neg square wave.

Pulse width and repetition rate are independently adjustable. WR549A operates within 5% (at the calibration points) of the dial settings over the entire range and maintains a pulse width of 100 ns to 0.1 s over an unlimited cycle. Rise and fall time is less than 20 ns on all ranges. Output is adjustable for both TTL and CMOS, covering a range of 0 to 15 V pk-pk. Impedance is selectable at 50 or 600 Ω .

CIRCLE NO. 338

5½ DIGIT ACCURACY. 4½ DIGIT PRICE.

The 4600 is our brand new 4½ digit multimeter. It gives you the accuracy and resolution of typical 5½ digit multimeters. At half the cost.

And the 4600 stays accurate longer than other DVM's. DC accuracy stays within 0.01% \pm one digit for six months at a time. We guarantee it.

80dB normal mode noise rejection produces a 10,000:1 reduction of excess noise. A full decade better than the 1,000:1 reduction of comparable instruments.

Loading errors are virtually eliminated by the 4600's 10,000M Ω input impedance on the two lowest DC voltage ranges.

There's a lot more. Send for a free catalog on our new 4½ digit 4600 multimeter. And find out how to get 5½ digit accuracy without paying for it.

Dana Laboratories, Inc.,
2401 Campus Drive, Irvine,
California 92715. 714/833-1234.

DANA

Others measure by us.



"NOW AVAILABLE THROUGH ELECTRO RENT"

FOR PRODUCT DEMONSTRATION
CIRCLE # 102

FOR LITERATURE ONLY
CIRCLE # 103

Amplifier delivers 75 W from dc to 100 kHz

Krohn-Hite Corp., Avon Industrial Park/Bodwell St., Avon, MA 02322. (617) 580-1660. \$1500; 8 wks.

Model 7500 direct-coupled dc-to-1-MHz amplifier is said to be the first such amplifier to offer up to 75 W of continuous power (150 W at dc) and 125 V rms over a bandwidth from dc to 100 kHz. Output is 10 W at 1 MHz. Frequency response is flat to within ± 0.1 dB over most of the range. Total harmonic distortion at full power output is less than 0.05% from dc to 20 kHz. Voltage gain is noninverting, and can be selected for either fixed gains of 20 dB (X10) or 40 dB (X100). Gain is continuously adjustable from zero to 40 dB.

CIRCLE NO. 339

Unit checks your contact's chatter

Associated Testing Labs, Northwest Industrial Park, Burlington, MA 01803. (617) 272-9050. See text.

The Contact Monitor is a solid state, chatter checker capable of detecting openings between a set of normally closed contacts, or closure between a set of normally open contacts. The unit detects contact chatter in electrical and electronic components having movable electrical contacts, such as relays, switches, circuit breakers, etc., where it is required that the contacts do not open or close momentarily, for longer than a specified time duration under environmental conditions, such as vibration, shock or acceleration. Model NCNO 4-5, the four-channel device, meets the requirements of MIL-STD-202D, method 310, paragraph 2.1.2., test conditions A, B, C, D, and E. For calibration, an oscilloscope with calibrated time base from 1 μ s to 5 ms/cm and a dc-VTVM are needed. The instrument measures 5.25 \times 8.3 \times 13.25 in. It has a detection accuracy of $\pm 3\%$ and a detection ratio (normal time to detection time) of 10:1. Price of the four-channel unit is \$700 and a six-channel model is available for \$980.

CIRCLE NO. 340

SWAP MEET

CUSTOM "SWAP" CHIP ADVANTAGES

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2

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8

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"SWAP" is the major price breakthrough in custom logic circuits that makes it easy for you to take that first step. To climb aboard the bandwagon

with your buddies in the industry, all you need is \$25. That buys you your new SWAP Kit including the Design Manual, vellum work sheets, and 15 sample I²L devices illustrating some of the functional blocks that can be used in a SWAP design. Send for yours!

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Tell me about your standard off-the-shelf DTL, TTL, and CMOS circuits. (We have these in stock.)



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Here's a new permanent magnet stepper motor line created to meet the design needs of analytical instrumentation and computer peripherals. Applications include tape drives, printer and chart drives and optical disc drives. Both 5 volt and 12 volt models are available.

All utilize 4-phase stators and permanent magnet rotors. Most

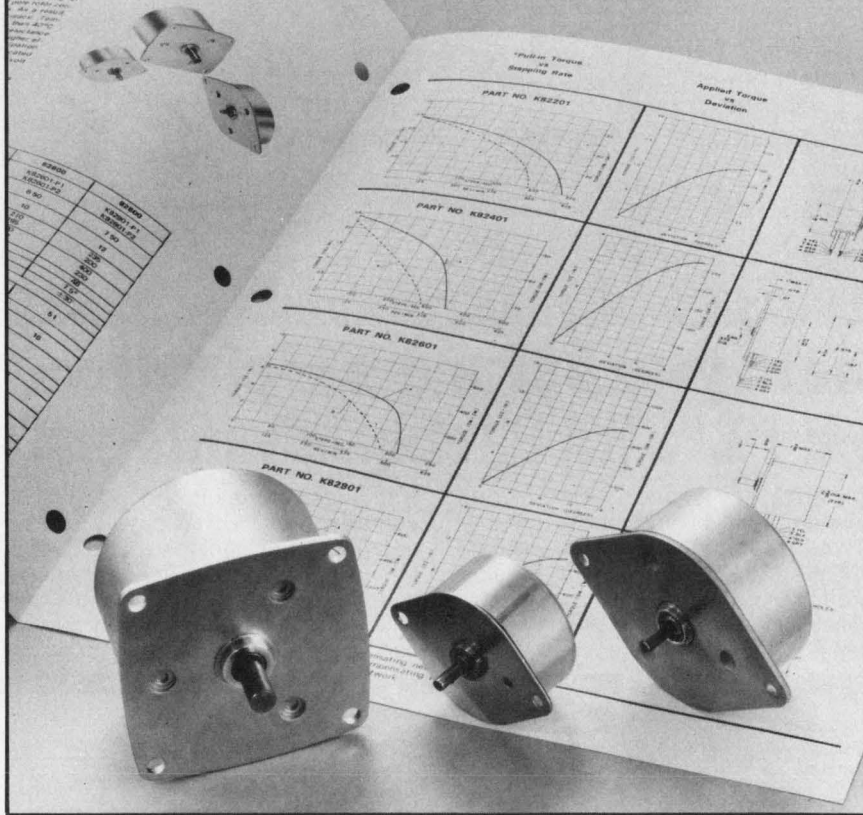
have 24-pole rotor construction. As a result, they offer excellent pull-in rates and good stepping accuracy. Another advantage is low temperature rise... over 50% lower than comparable variable reluctance stepper motors operating on a similar duty cycle. Gear boxes can be furnished to meet varying torque and speed requirements.

Write for information today!

Available pull-in torques from .750 oz-in. to 7.50 oz-in.
Available stepping rates from 210 steps/sec to 440 steps/sec.

Our 4-page *Permanent Magnet Logic Stepper Motor* catalog provides all basic details including performance data and charts, dimensional drawings, as well as electronic drive information. Send for a copy.

ES - 4-Phase Logic Drive
models for analytical
computer peripherals.



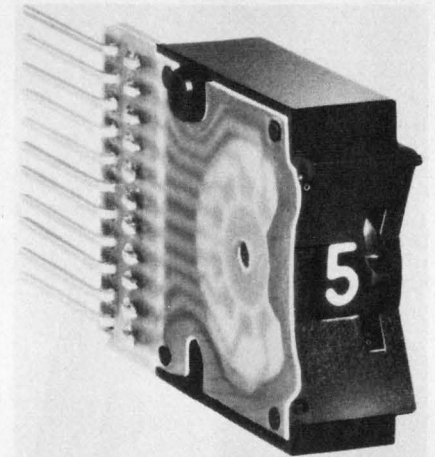
A. W. HAYDON CO. PRODUCTS

NORTH AMERICAN PHILIPS CONTROLS CORP.

Cheshire, Conn. 06410 • (203) 272-0301
CIRCLE NUMBER 105

COMPONENTS

Small thumbwheel switch features J-pin terminals



Cherry Electrical Products Corp.,
3600 Sunset Ave., Waukegan, IL
60085. (312) 689-7702. \$3.33 (2000
up).

The T50J-01M is the smallest thumbwheel switch on the market today with 1/2-in. J-shaped pin terminations, according to Cherry. This makes the thumbwheel readily adaptable for both motherboard and wire-wrapping applications. The J-pins are made of brass with a bright tin finish. The switch is matte finished, has a 10-position decimal thumbwheel with in-line readout, and is modular constructed to allow ganging large numbers of switches. A 40-switch assembly uses a panel opening only 3/4-in. high and less than 13-in. wide.

CIRCLE NO. 341

Thick-film pots now range to 100 MΩ

TRW Inc., 401 N. Broad St., Philadelphia, PA 19108. (215) 922-8900.
\$0.42 (10,000 up); 2 to 4 wks.

A high-voltage thick-film potentiometer with previously unavailable resistance and stability characteristics now has a resistance range of 1 to 100 MΩ. It also features a shield to minimize dust accumulation. Temperature coefficient is a low ± 400 ppm. Snap-in installation is standard, but mounting with a self-threading nut is also possible. For added flexibility, the control will accept different types of shafts. Over-all dimensions of the unit are 1-in. wide, 1.277-in. deep and 1.06-in. high.

CIRCLE NO. 342



TCX...the new aluminum capacitors with the super electrolyte.

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Our new electrolyte system is the key. It provides the properties that make TCX capacitors ideal for even the most demanding commercial duty — such as high frequency, power supply, EDP applications.

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temperature range up to 105°C. Which is about 20° higher than with almost every other capacitor of this type.

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Electrical and Electronic Components • Timing Devices and Motors • Metallurgical Products • Batteries

CIRCLE NUMBER 106

COMPONENTS

Switches and indicators receive seismic approval

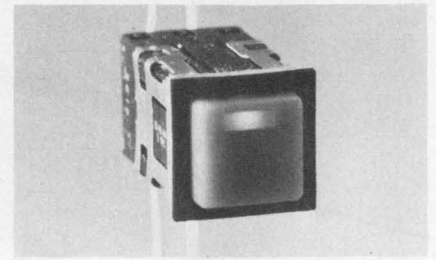
Stacoswitch Inc., 1139 Baker St., Costa Mesa, CA 92626. (714) 549-1616. \$8.95 to \$30 per channel; 4 to 8 wks.

Stacoswitch switches and indicators are now seismic qualified to requirements of IEEE Standard

344-1975 and TVA 2200 appendix "C" for use in nuclear-fueled power-generating plants. One-to-four lighted status-message displays per control channel and one-to-one-hundred channels per control unit are available as standard assemblies. Up to 4PDT circuit switching with momentary, maintained or magnetic-latching actions for each control channel provides wide control versatility.

CIRCLE NO. 343

Projected LED light brightens PB switches



Micro Switch, 11 W. Spring St., Freeport, IL 61032. (815) 232-1122. Under \$5 (OEM qty).

The projection of strong LED rays through a big indicator window gives the AML series lighted pushbuttons a bright look. The new design makes the LED easier to see in ambient light and visible from many angles denied most LED indicators, according to the manufacturer. A funnel-shaped reflector at the base of the diode helps beam red, yellow or green lights to the display surface of the pushbutton/indicator. Rated for 5, 10 or 15 V dc, the units have an internal resistor to maintain current at a nominal 20 mA. The switches are available with momentary or two-level alternate actions, and in one and two-pole form-C arrangements.

CIRCLE NO. 344

Anywhere high efficiency power conversion is needed . . . look to Arnold Magnetics!

Look at the performance: AC (115-230 VAC, 47-500 Hz) and DC (12, 28, 48, 115, and 150 VDC) inputs . . . 1 to 6 isolated and regulated DC outputs from 4.2 to 300 VDC . . . line and load regulation to 0.1% . . . efficiencies to 85% . . . 3.9 watts delivered per cubic inch . . . short circuit and transient protected.

Look at the design: Over 1200 input/output configurations are available using off-the-shelf sub-modules. You specify to your needs using our exclusive "Design-As-You-Order" specification form that eliminates engineering cost, lost design time and long delivery schedules.

Look at the package: Compact, lightweight . . . your complete Power Conversion System is provided in a tested and encapsulated miniaturized, conduction cooled package.

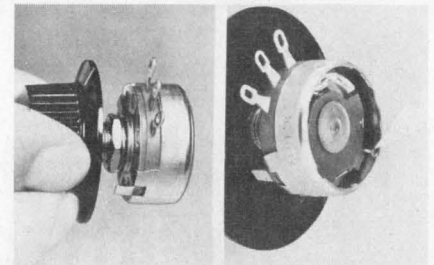
Looking for high efficiency power conversion? Look to Arnold Magnetics . . . today!



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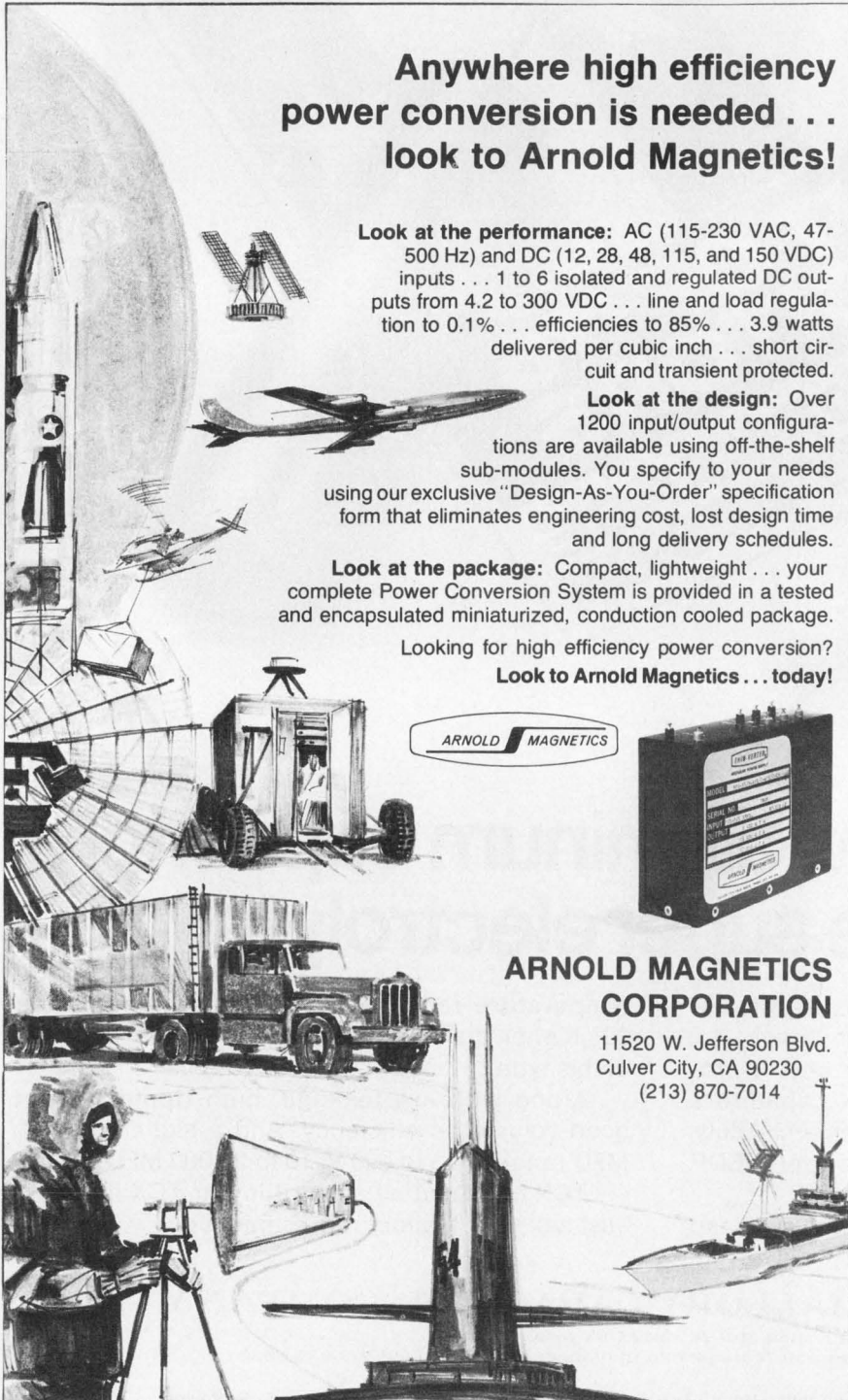
Popular potentiometer now has slip clutch



Allen-Bradley, 1201 S. Second St., Milwaukee, WI 53204. (414) 671-2000. \$1.50 (1000 up); 6 to 8 wks.

The type EJ potentiometer, a million-cycle rotational-life component, widely used in electronic games now is offered with an optional slip-clutch. The clutch prevents internal damage to the pot or the external knob if the shaft is turned with excessive force. Clutch action allows the shaft to be rotated beyond the stops, and then resume normal electrical operation when the rotating is reversed.

CIRCLE NO. 345



CIRCLE NUMBER 107

ChipStratesTM cost up to 40% less than other power SCRs and Triacs.

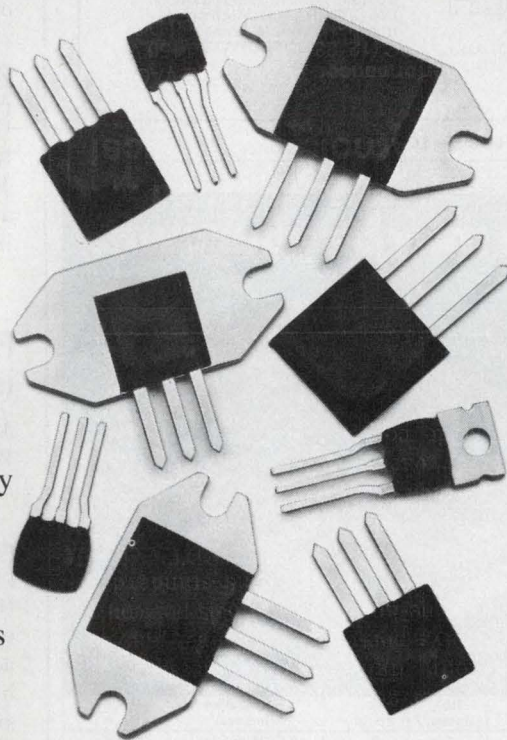
And that's only the beginning.

ChipStrates are glassivated power SCR or Triac chips mounted on solderable ceramic substrates. Since they eliminate the need for expensive metal packages, they cost up to 40% less than other power SCRs or Triacs.

For example, our 55A, 400V, ChipStrate goes for just \$3.80 in quantities of 5,000. The electrically equivalent press fit Triac will run you \$5.00 in the same quantity.

But that's not all.

ChipStrates are available in ratings from 3 to 55A and up to 800V

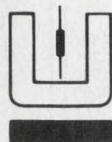


and come in a rugged, electrically insulated package.

Their exceptionally good form factor will simplify the packaging of your system.

And their reliability is unmatched. ChipStrate. The new concept in SCRs and Triacs that gives you more. And costs you less.

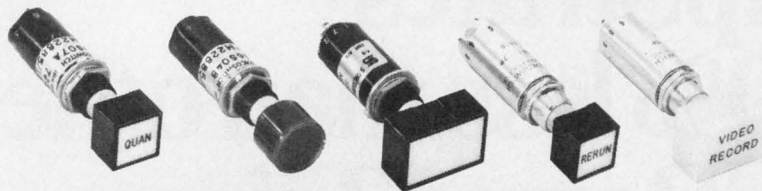
For the full story, just call or write: Carl Uretsky, Unitrode Corporation, 580 Pleasant St., Watertown, MA 02172. 617-926-0404.



UNITRODE

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CIRCLE NUMBER 108



STACOSWITCH...

dependability you can afford

SWITCHES Military or industrial/commercial single lamp switches built to exacting specifications for dependability and long service life. Choice of circuit control contact arrangement and solder or new PC terminations.

PUSHBUTTONS All sizes, styles, colors, and legend styles including new photographic film legends with visible or hidden messages. Color matched for visual recognition and operator convenience.

LOW COST Check the bottom line and you'll find Stacoswitch's low purchase price combined with quick and easy installation and maintenance make these your best buy in single lamp pushbutton switches. Write today for General Catalog giving complete description on single lamp and 4-lamp switches and indicators. When you think switch... think Stacoswitch.

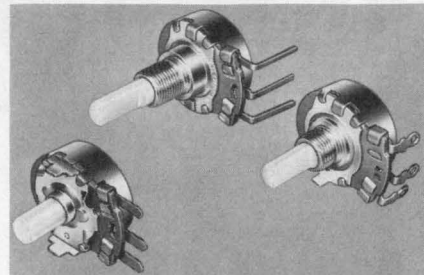


Other STACO Company products:
Custom Transformers, STACO,
INCORPORATED, Richmond,
Indiana; Variable Transformers,
STACO, INCORPORATED,
Dayton, Ohio.

CIRCLE NUMBER 109

COMPONENTS

New pots designed for electronic games



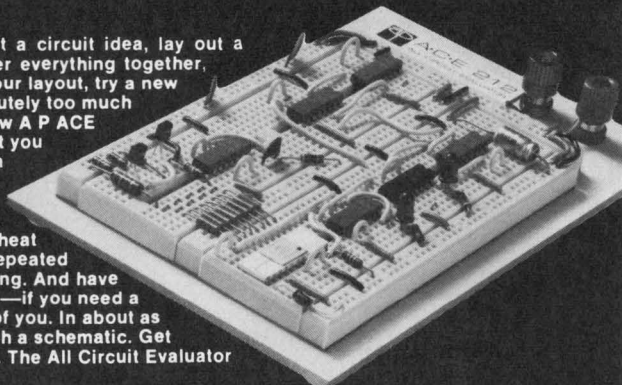
Centralab Electronics, Div. Globe-Union, 5757 North Green Bay Ave., Milwaukee, WI 53201. (414) 228-2911.

A new potentiometer designed for the electronic-game market (Ultralife Model 2) has excellent life and low-noise characteristics. Mechanical life is in excess of 250,000 cycles. Its contact-spring design results in an initial contact-resistance variation of 0.5%. End-of-life contact-resistance variation (CRV) is less than 1.5% of total resistance. The following additional features are provided: resistance range from 5000 Ω to 5 M Ω ; linear taper; a power rating of 1/2 W at 40 C; PC or solder-lug terminals; and a bushing for twist-tab mounting.

CIRCLE NO. 346

The time you save may be your own.

Used to be you'd get a circuit idea, lay out a pc board, print it, solder everything together, troubleshoot, change your layout, try a new board, and spend absolutely too much time breadboarding. Now A P ACE All Circuit Evaluators let you breadboard in a fraction of the time. Make your changes immediately. Keep full leads on your components. Avoid the heat damage possible with repeated soldering and desoldering. And have a pattern for your board—if you need a board—sitting in front of you. In about as long as it takes to sketch a schematic. Get cooking with ACE. ACE. The All Circuit Evaluator from A P Products.



Part No.	ACE Model No.	Tie Points	DIP Capacity	No. Buses.	No. Posts	Board Size (inches)	Price Each
923333	200-K (kit)	728	8 (16's)	2	2	4-9/16x5-9/16	\$18.95
923332	208 (assem.)	872	8 (16's)	8	2	4-9/16x5-9/16	28.95
923334	201-K (kit)	1032	12 (14's)	2	2	4-9/16x7	24.95
923331	212 (assem.)	1224	12 (14's)	8	2	4-9/16x7	34.95
923326	218 (assem.)	1760	18 (14's)	10	2	6-1/2x7-1/8	46.95
923325	227 (assem.)	2712	27 (14's)	28	4	8x9-1/4	59.95
923324	236 (assem.)	3648	36 (14's)	36	4	10-1/4x9-1/4	79.95

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Our Distributor List is growing daily. If none in your area call toll Free 800-321-9668.

CIRCLE NUMBER 110

Precision-pot element is conductive plastic

Maurey Instrument Corp., 4555 W. 60th St., Chicago, IL 60629. (312) 581-4555. \$21 (100 up).

The 112-P19 is a low-cost, solid-molded raised track, conductive-plastic potentiometer. It offers infinite resolution, long life and extremely rugged vibration characteristics. The unit features a high-pressure wiper-assembly design and high-quality wiper-contact material to obtain rotational life under extreme environment that exceeds conventional film devices. Gold-plated terminals, beryllium-copper wiper spring as well as a stainless-steel shaft and ball bearings are standard. Size is 1-1/8-in. dia. with a 1/8-in. dia. shaft. Resistance range is 500 Ω to 100 k Ω , standard linearity $\pm 0.5\%$ and life is in excess of 100-million revolutions.

CIRCLE NO. 347

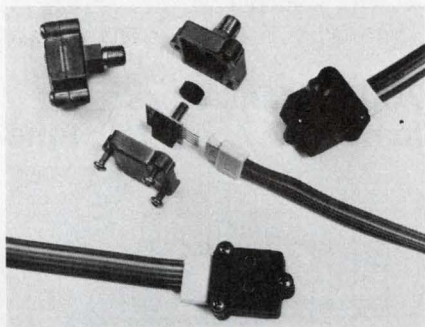
Panel controls set X-Y position

Cambridge Thermionic, 445 Concord Ave., Cambridge, MA 02138. (617) 734-1055. From \$2000; 4 wks.

Cambi-Grid is a two-axis positioning control for use where all movements along either axis are some multiple of a fixed increment such as 0.1 in. Applications include drilling, insertion, inspection, punching, packaging, etc. The system is programmed directly on its own control panel as opposed to paper-tape programmed systems. Features include nonvolatile program memory, programmable tool function, manual and automatic operation modes, adjustable control of positioning-motor speeds. The rack mountable unit has a G4 instruction memory, which allows the programming of up to 960 X-Y coordinates. A line of compatible stepping motor drivers is available.

CIRCLE NO. 348

Pressure transducer offered in new packages



National Semiconductor, 2900 Semiconductor Dr., Santa Clara, CA 95051. (408) 737-5000. \$79 (25 up); stock.

The LX1700 series pressure transducers, in new package designs, are designated PX7-1 in zinc packages and PX7N-1 and PX7D-1 in nylon packages. They feature internal captive O-rings that eliminate leakage. The devices are fully signal conditioned and temperature compensated (operating range 0 to 85 C). And they can measure pressure ranges from ± 5 psi to 0 to 300 psi. In addition a flexible cable is key locked so it can't be pulled out of the package. They come with five-pin connectors for easy insertion into a test socket or PC board.

CIRCLE NO. 349

Now, a single integrated circuit, our TAD-32 (Tapped Analog Delay), can provide filtering with passband-to-stopband ratios of 40 DB or more per device. Simple variation of the clock sampling rates over 5 decades will accordingly shift a given filter characteristic. Transversal or recursive filters can be constructed with over 60DB dynamic range and linear phase. Tapped delays up to several hundred milliseconds are possible.

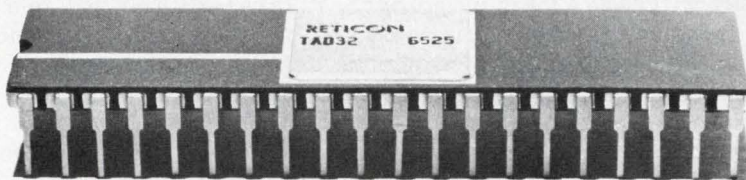
Discrete time analog signal processing using charge transfer devices is a reality at RETICON.

The TAD-32 is just one device in this growing family.

We don't just talk about them, we make them.

THIS DIP DOES IT ALL.

TAPPED DELAYS
MATCHED FILTERS
CORRELATION
CONVOLUTION



RETICON®

910 Benicia Avenue, Sunnyvale, California 94086
PHONE: (408) 738-4266 TWX: 910-339-9343

CIRCLE NUMBER 111

DISCRETE SEMICONDUCTORS

20-A rectifiers offer 35-ns turn-off time

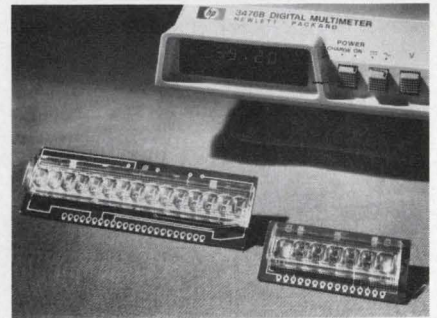
NAE, Inc. Semiconductors, 69 Bennett St., Lynn, MA 01905. (617) 598-4800. \$7.80 to \$16.25 (1-99); stock.

A new series of superfast 20-A rectifiers for dc applications—in-

verters, converters, choppers and switching regulators—handles up to 200 V. Designated 1N5812 through 1N5816 with voltage ratings from 50 to 150 V in 25-V increments, these new 35-ns units have a low forward drop of 0.9 V at 10 A, and they are housed in the JEDEC DO-4 packages. The 200-V version, designated NSR-7025, offers the same recovery features as the lower-voltage units.

CIRCLE NO. 350

LED numerical displays need 1/3 usual power

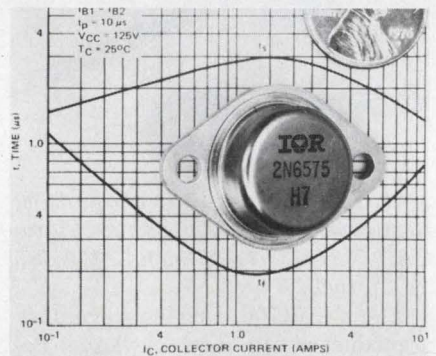


Hewlett-Packard, 1501 Page Mill Rd., Palo Alto, CA 94304. (415) 493-1501. \$11.25: 5 digits, \$31.95: 15 digits (200-999).

LED seven-segment numerical displays, 0.175-in. high, require only 2 mA per segment, about 1/3 the power required by presently available displays. These HP 5082-7265, 7275, 7285 and 7295 indicators are available in five and 15-digit packages. Models 5082-7265 and 7275 five and 15-digit clusters, respectively, have a center decimal point. Models 5082-7285 and 7295, also five and 15-digit clusters, have a right decimal point. Devices may be mounted with edge connectors or with soldered wires.

CIRCLE NO. 354

700-V transistors feature 0.7 μ s fall time



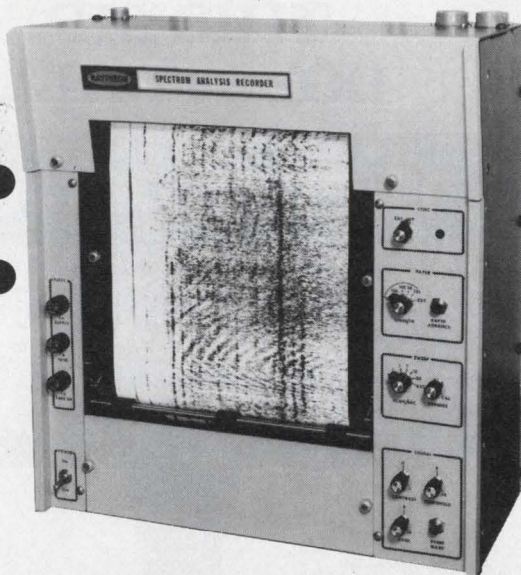
International Rectifier, 233 Kansas St., El Segundo, CA 90245. (213) 322-3331. \$3.78 to \$4.79 (100-999); stock.

A new series of power transistors, 2N6573 through 2N6575, with very fast switching times and ratings to 700 V at 15 A, features fall times as fast as 0.7 μ s. Hard-glass passivation of the chips provides high-temperature stability and long operating life for application in TV deflection circuits, switching regulators and high-voltage switching power supplies.

CIRCLE NO. 355

Q: Is there a recorder just for spectrum analyzers?

A:



The new 19" rack-mounting SPECTRUM ANALYSIS RECORDER from Raytheon. It's the first dry paper line scanning recorder specifically developed for direct plug-in operation with commercially available spectrum analyzers.

Any new or existing spectrum analyzer equipped with the SAR-097 will have a lot more going for it. Like infinitely variable 100:1 speed range—5 sec/scan to 50 milliscan... stylus position encoder... automatic recorder synchronization... computer/analyzer compatibility... high resolution and dynamic range... all-electronic drive. And more.

If you design and build—or buy and use—spectrum analyzers, you don't have to settle for multi-purpose recorders any more. The SAR-097 is here. For full details write the Marketing Manager, Raytheon Company, Ocean Systems Center, Portsmouth, Rhode Island, 02871. U.S.A. (401) 847-8000.

RAYTHEON

CIRCLE NUMBER 112

The best buy ever in an Autoranging Portable DMM

Look at what you
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for only \$195.



Performance, quality, reliability and price. The Weston Model 6000 is a total value package and the best buy ever in a portable digital multimeter. It offers the simplicity and speed of automatic ranging at 0.35% accuracy. Superior performance at minimum cost through use of custom LSI microcircuitry and laser trimmed resistor networks. Specially developed LCD display for long life and high legibility, even in bright sunlight. Powered by two inexpensive, easily available 9v transistor batteries with more than 200 hours of operating life. Weston has packed the Model 6000 with every type of performance and convenience feature...at an unbeatable price.

To get the full details, contact any Weston distributor. Or, write direct to Weston.

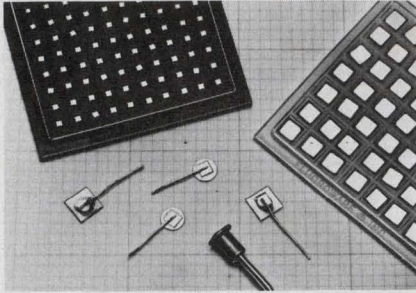
Weston Instruments, Inc., 614 Frelinghuysen Ave., Newark, N.J. 07114.
Canada: 1480 Dundas Highway, Mississauga, Ontario.
Europe: Ingolstadter Str. 67a 8 Munchen 46, W. Germany.

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Schlumberger

CIRCLE NUMBER 113

DISCRETE SEMICONDUCTORS

Fast diode chips rated to 100 A



Solid State Devices Inc., 14830 Valley View Ave., La Mirada, CA 90638. (213) 921-9660. \$0.25 to \$5 (100 up); stock.

A new line of 1-to-100-A ultra-fast-recovery diode chips allows hybrid manufacturers to obtain circuit performance previously obtainable only with packaged devices, according to Solid State Devices. The HSR and HVE chip families are processed with Epion ion-implantation techniques to give 9-to-90-ns reverse-recovery times—about 10 times faster than conventional devices. The HSR Series are 20-to-150-V-peak reverse-voltage chips with 1 through 100-A forward-current capabilities. Maximum reverse-recovery times are 9 to 75 ns. Maximum full-cycle average forward-voltage drop is 450-mV, and maximum instantaneous forward-voltage drop is 900-mV. Leakage currents range from 50 μ A for the 1-A units to 500 μ A for the 100-A devices. Maximum surge currents are 10 times greater than rated currents on the 100-A units and 50 times greater on the 1-A devices. The HVE Series chips have peak reverse voltages ranging from 200 to 600 V with the same rated currents, leakage and maximum-surge currents as the HSR chips. Reverse recovery times are 15 to 90 ns. Maximum average forward-voltage drop is 500 mV, and maximum instantaneous forward-voltage drop is 1.2 V.

CIRCLE NO. 356

Filler

It wasn't a miracle, Joyce Lekas of Tektronix informs us, when sharks formed a clear-passage corridor for the patent attorney swimming ashore from his sinking boat. It was professional courtesy.

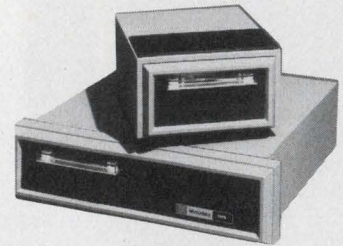
THIS TIME
MICRODATA
HAS GONE TOO FAR!

THEIR OEM PERIPHERALS WERE UNFAIR BEFORE. BUT LODESTAR IS TOO MUCH! NOW THEY'VE FOUND A WAY TO PUT 10 MEGABYTES ON A 3M-TYPE CARTRIDGE. 6400 BPI ON 1/4 INCH TAPE!

TALK ABOUT UNFAIR COMPETITION! THAT'S TWICE THE CAPACITY OF MY BEST 3M CARTRIDGE DRIVES. AND LODESTAR IS PLUG AND SOFTWARE COMPATIBLE WITH STANDARD REEL-TO-REEL SYSTEMS.

EVEN AT THOSE HIGH DENSITIES, LODESTAR'S MTBF IS OVER 4000 HOURS. AND IT'S SO DARN COMPACT YOU CAN MOUNT TWO OF THEM IN 7 INCHES OF VERTICAL RACK SPACE. BOY, THEY DON'T MISS A TRICK.

I HOPE NONE OF MY OEM CUSTOMERS FIND OUT ABOUT THIS ONE!



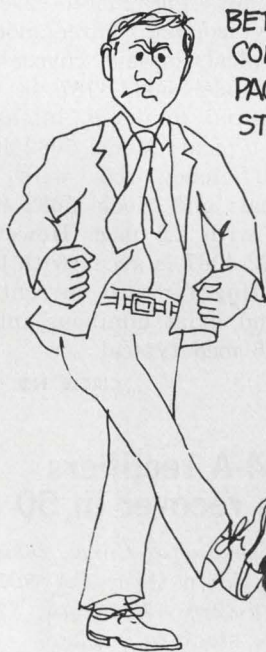
• Unformatted Storage Capacity: 11.5 megabytes at 6400 bpi • Recording Method: Serial, 4 tracks • Transfer Rate: 192 KHz at 6400 bpi • Full Tape Write: 10 minutes • Full Tape Read: 8 minutes, bi-directional • Error Rate: less than 1 bit in 1×10^8 • MTBF: over 4000 hours • MTTR: less than 1/2 hour • Size: mechanism, data and motion electronics, 5"H x 8"W x 11"D; optional single or dual drive rack mount version with formatter and power supply, 7"H x 17"W x 12"D.

REFLEX? HERE'S MY REFLEX!
IT'S INCREDIBLE! NOW MICRODATA'S
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BUSINESS!

THIS NEW REFLEX DRIVE HAS THE
RELIABILITY OF FIXED MEDIA AND
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AT A LOWER COST PER BIT THAN ANY-
THING ELSE ON THE MARKET.

THEY'VE CUT ACCESS TIME WITH FASTER
HEAD POSITIONING, FASTER ROTATION
AND TWO HEADS PER SURFACE. THERE'S
EVEN A FIXED HEAD-PER-TRACK OPTION.

YOU'D THINK THAT WOULD BE ENOUGH.
BUT NOT FOR MICRODATA, THEY LOVE
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STORAGE MODULE. BETTER RELIABILITY.
BETTER PERFORMANCE.
COMPACT 7-INCH RACK MOUNT
PACKAGE. IT JUST NEVER
STOPS.



MY ONLY HOPE IS MAYBE
THEY CAN'T DELIVER.

Sorry, Chuck, we're taking orders right
now. OEM's should call or write
directly to Microdata Corporation,
P.O. Box 19501, Irvine, California 92713,
Telephone: 714/540-6730.



- Unformatted Storage Capacity: 12.5, 37.6 or 62.7 megabytes • Bit Density: 5,636 bits/inch • Data Transfer Rate: 7.08 MHz • Rotation Speed: 2964 rpm
- Track Density: 300 tpi • Position Time: 30 msec avg. • Track-to-Track Position Time: 6 msec • Error Rate: Recoverable, 1 bit in 1×10^{10} bits; Nonrecoverable, 1 bit in 1×10^{13} bits • MTBF: 6500 hrs.
- Size: 7"H x 17"W x 28"D.

Microdata

Microdata Corporation, 17481 Red Hill Avenue, Irvine, CA 92714,
Telephone: 714/540-6730. TWX: 910-595-1764.

FOR IMMEDIATE USE CIRCLE NUMBER 114
FOR INFORMATION ONLY CIRCLE NUMBER 115

Fast recovery rectifiers handle to 30 A



TRW Power Semiconductor, 14520
Aviation Blvd., Lawndale, CA
90260. (213) 679-4561. \$2.48: 1N-
3899, \$3.10: 1N3909 (100-999);
stock.

Two series of fast-recovery power rectifiers feature peak-inverse voltages of 50 to 400 V. Series 1N3899 through 1N3903 has an average forward current of 20 A and a reverse-recovery time of 200 ns maximum. The operating temperature range is -65 to 150 C. The 1N3909 through 1N3913 series also has a reverse-recovery time of 200 ns maximum, but an average forward current of 30 A. Both series are JEDEC registered.

CIRCLE NO. 357

Voltage regulators provide low impedance



Semtech Corp., 652 Mitchell Rd.,
Newbury Park, CA 91320. (213)
628-5392. \$6.55 (100 up); stock.

Mini-stud, types MY6.8 through MY120—a series of voltage regulators—offers low dynamic impedance and good efficiency as voltage regulators. The units also are suited for use as transient-voltage suppressors. Encased in Metoxilite, which makes the units hermetic and rugged, they can handle peak pulse power of 30 W at nominal voltages from 6.8 to 120 V ($\pm 5\%$). The temperature coefficient of the regulators is 0.05 to $0.10\%/^{\circ}\text{C}$.

CIRCLE NO. 358

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Computer Products, Inc., is the world's leading manufacturer of encapsulated power supplies. And we owe it all to you, for recognizing the value of:

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 **Computer Products, Inc.**



1400 NW 70 Street, Fort Lauderdale, Florida 33309 (305) 974-5500, TWX (510) 956-9895.

CIRCLE NUMBER 116

Gulton's New Quiet Non-Impact Thermal Numeric Printer

Featuring...ultra quiet operation...seven columns of numbers or six columns of numbers with \pm sign...fast paper roll loading...up to four line per second print rate...complete with interface electronics...compatible with all popular digital panel meters.



Write or call for detailed catalog.

gulton®

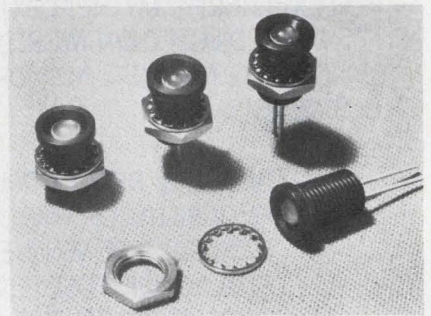
Measurement & Control Systems Division
Gulton Industries Inc., East Greenwich, Rhode Island 02818
401-884-6800 • TWX 710-387-1500

CIRCLE NUMBER 117

Introducing Gulton's answer to noisy, complicated mechanical printers. The NP-7 panel-mounting printer requires only one moving part, the paper advance motor, which sends the paper silently beneath a non-impact thermal print head. You'll be pleased at the price, too.

DISCRETE SEMICONDUCTORS

LED lamps sealed in metal case



Hewlett-Packard, 1501 Page Mill Rd., Palo Alto, CA 94304. (415) 493-1501. \$15.55: 4787; \$17: the other models; (10-99); stock.

In four colors, these hermetically sealed solid-state lamps are designed for high-reliability applications and for protection against RFI panel leakage. The lamps are easily mounted by drilling a 0.323-in. hole (P drill). Mounting hardware includes a lockwasher and hex nut. The metal case is electrically isolated. Three models have a typical forward current of 20 mA. Model 5082-4787 is red with an axial luminous intensity of 1 mcd typical; Model 5082-4687 is high-efficiency red, with 2.5 mcd typical; and Model 5082-4587 is yellow with 2.5 mcd. However, Model 5082-4987 is green with typical operating forward current of 25 mA and axial luminous intensity of 1.6 mcd typical.

CIRCLE NO. 359

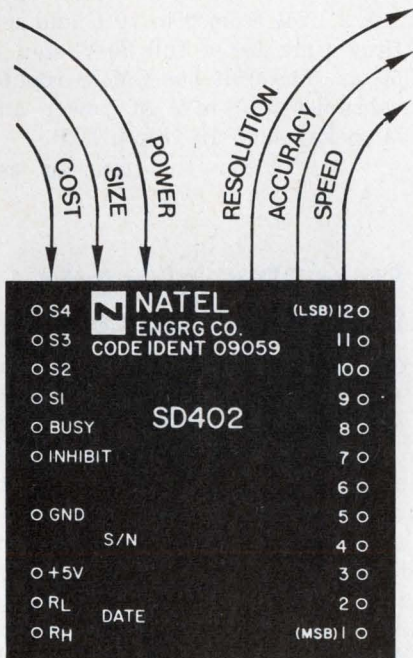
3 and 4-A rectifiers reverse recover in 50 ns

Microsemiconductor Corp., 2830 S. Fairview, Santa Ana, CA 92704. (714) 979-8220. \$5.20 to \$7.34 (100-499); stock to 2 wks.

Fast, high-voltage 3 and 4-A rectifiers, designated MX2130 to 2160 and MY3130 to 3160, handle from 300 to 600 V. Reverse recovery times for all of these miniature glass-package units is typically 50 ns. The units are hermetically sealed in hard glass cases, are metallurgically bonded and are voidless. Leads are solderable silver, markings are solvent resistant and the cathode band is a contrasting color.

CIRCLE NO. 360

Compact 12-bit s/d converter cuts size, weight by 50%



Natel Engineering, 8954 Mason Ave., Canoga Park, CA 91306. (213) 882-9620. See text: stock to 45 days.

Not only does the SD402 synchro-digital converter offer 12-bit resolution, but it does so at half the size and price of its 12-bit competitors. Developed by Natel Engineering, the unit measures 2.625 x 2.625 x 0.42 in. and costs only \$199 in single-unit quantities. It is also, reportedly, the first s/d that can operate from a single +5-V supply.

The s/d converter uses a continuous tracking circuit in a Type II servo loop to eliminate lag and zero-velocity error at input rates of up to 8000°/s. Over-all accuracy of the converter checks in at ±15 arc minutes and holds for tracking rates of up to 10,800°/s.

Even though the converter weighs just 3 oz, all inputs are transformer-isolated, and both synchro and resolver inputs are accepted. The standard SD402 is designed for 400-Hz signals and handles 11.8 or 90-V rms for synchro in-

puts, 11.8, 26 or 90-V rms for resolver inputs, and 26 or 115-V rms for the reference input. The reference input has an impedance of 100 kΩ. For 60-Hz operation, a separate transformer module (\$50) is required.

The 12-bit digital output is constantly available, except during the converter-update period (indicated by a converter-busy signal). Updating can be prevented by applying a ZERO to the inhibit line, and the converter can be kept in the hold-mode as long as the ZERO remains on the inhibit line.

Some of the SD402's competitors feature higher tracking rates and less power consumption for a price.

The SDC1700 12-bit converter from Analog Devices, Norwood, MA, has an accuracy of ±8.5 arc minutes and a tracking rate of 12,960°/s. It does, however, require ±15 and +5-V supplies and costs \$365. But even though the SDC-1700 from Analog Devices requires three supplies, it does draw less power—only 1.1 W vs 1.5 W for the Natel SD402.

Recently introduced hybrid converters, series HSDC-10, from ILC Data Device Corp., Bohemia, NY, provide tracking rates of 36,000°/s and are even smaller than the Natel SD402. However, these hybrids are only 10-bit single-package units and require +15 and +5-V supplies. And they cost \$345. For 12-bit resolution, DDC has larger modules in its 522/622 series that start at \$395.

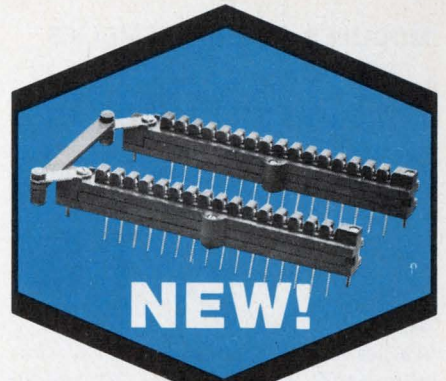
In addition to its commercial SD402, Natel offers a militarized version that operates over a -55 to +105 C range and costs \$299 (1 to 24 pieces), as well as 14 and 16-bit converters with slightly larger packages.

Natel Analog Devices ILC Data Device Corp.

CIRCLE NO. 301

CIRCLE NO. 302

CIRCLE NO. 303



TEXT TOOL AXIAL LEAD ZIP STRIPS

Get zero insertion pressure operation at "plug-in" socket prices!

The new line of TEXT TOOL axial lead ZIP STRIPS offers easy, convenient zero insertion pressure operation at "plug-in" socket prices!

That's right. The per-position cost of a 16 position axial lead ZIP STRIP featuring zero insertion pressure is competitive with that of currently available conventional "plug-in" sockets. And, ZIP STRIPS are designed for testing and aging of all axial or radial lead devices (diodes, capacitors, resistors, etc.) with lead diameters from .015 to .040 inches.

The ZIP STRIP combines all the features of TEXT TOOL's other zero insertion pressure sockets, virtually eliminates mechanical rejects and has a typical life of 25,000 to 50,000 insertions.

In addition, a unique design allows ZIP STRIP contacts to literally wrap themselves around device leads to prevent their "walking out." This is especially important in applications where ZIP STRIPS are subjected to oven vibration or where they are mounted in an inverted position.

The mechanical action of the ZIP STRIP is the utmost in simplicity. This feature, coupled with a unique system of ramps and bevels to guide the devices, makes it ideally suited for rapid loading and unloading by either hand or mechanical means.

ZIP STRIPS are available in either polysulfone (150°C) or torlon (200°C) to meet specific test or aging requirements.

Detailed information on these and other products from TEXT TOOL . . . IC, MSI and LSI sockets and carriers, power semiconductor test sockets, and custom versions . . . is available from your nearest TEXT TOOL sales representative or the factory direct.



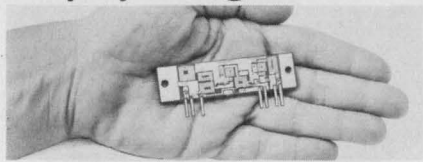
PRODUCTS, INC.

1410 W. Pioneer Drive • Irving, Texas 75061
214/259-2676

CIRCLE NUMBER 118

MODULES & SUBASSEMBLIES

Vhf amplifier modules simplify design



Ampere Electronic Corp., Hicksville, NY 11802. (516) 931-6200. \$52.90 (1-9); stock.

The BGY36 amplifier module, operating at 148 to 174 MHz, delivers better than 18 W with a drive power of under 150 mW. It contains internal matching networks for broadband operation. The amplifier therefore remains stable into a 3:1 VSWR, any phase. VSWRs of up to 50:1, any phase, cause no damage, for heat-sink temperatures up to 70 C. A similar unit (BGY32) operates at 68 to 88 MHz; both connect to 12.5 V.

CIRCLE NO. 361

Nonlatch multiplying d/a is self-contained

Micro Networks, 324 Clark St., Worcester, MA 01606. (617) 852-5400. \$59 (1-25); 3 wks.

The MN3100 four-quadrant multiplying d/a converter is a self-contained, hermetically sealed unit, ready to use. It includes an internal op amp and laser-trimmed resistors, and is guaranteed not to latch up. Linearity is better than $\pm 1/2$ LSB from 0 to 70 C and settling time for a full 20-V step is 50 μ s. The unit has CMOS inputs, consumes 210 mW of power and is packaged in an 18-pin DIP.

CIRCLE NO. 362

Need answers on rechargeable power sources?



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800-433-2684
in Texas 800-792-8767

Call our Hot Idea-Hotline toll-free and we'll help you design a nickel-cadmium sealed cell power package to fit your specific needs. In addition, we'll give you hard facts on sizes, ampere hours, configurations, prices, delivery. Chances are, all the applications we've done on hand tools, appliances, calculators, toys, and communication equipment will provide some short cuts for you. Call us. We'll deliver. Marathon Battery Company, P.O. Box 8233, Waco, Texas 76710. A division of Marathon Manufacturing Company.

marathon battery company



CIRCLE NUMBER 119

Store 3D display data from a microprocessor

Optical Electronics Inc., P.O. Box 11140, Tucson, AZ 85734. (602) 624-8358. \$261 (10-29 qty); stock.

The 6711 interfaces with standard 8-bit microprocessors and its recirculating memory stores 256 three-dimensional points, with 8-bit resolution. The device provides three analog outputs representing each of the three mutually perpendicular axes and may be hard-wired directly to the company's Model 6114, 3-D display-generator module. A μ P accesses the 6711 as a memory location. The module connects to a μ P's 8-bit data bus, or an 8-bit data-output port, and two address lines. In addition the unit requires a strobe or read/write command and sends the μ P an execution bit when it is ready to receive a data byte. Programs can be furnished for the F-8, 8080A, 6800, 2650, 1802 and SC/MP μ Ps. Interfacing details are also available showing exact connections to the various evaluation kits that use these microprocessors. The module operates from standard μ P power (+5 V at 300 mA and -12 to -15 V at 100 mA). It outputs analog currents of ± 1 mA max. Data can be written in at random or at any rate up to 1.2 kHz. Information is read-out at 300 kHz. Internal address-counters can be incremented by the μ P or left to free run. These address counters simplify addressing by the μ P.

CIRCLE NO. 363

NEW SIMPSON

SERIES 2850 DIGITAL PANEL METER



NOW... at the right price...
a single DPM for popular
domestic and IEC/DIN cutouts



STANDARD CUTOUT
1.682" x 3.622"
(42.72 mm x 92 mm)



IEC/DIN CUTOUT
1.77" x 3.622"
(45 mm x 92 mm)



OTHER DOMESTIC CUTOUT
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(42.72 mm x 99.57 mm)

- 3½ digit readout
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- BCD output is standard
- Input/output edge connector included
- Highly reliable LSI circuitry
- Choice of 120/240 VAC, 50-400 Hz or 5 VDC operation
- OEM quantity prices available upon request.

ORDER FROM YOUR ELECTRONICS DISTRIBUTOR

Model 2850 120/240 VAC input; 0.55" planar gas discharge display complete with panel mounting clips, edge connector and manual. **\$138**

Model 2851 5 VDC input, 0.55" planar gas discharge display complete with panel mounting clips, edge connector and manual. **\$138**

Model 2852 120/240 VAC input, 0.43" LED display complete with panel mounting clips, edge connector and manual. **\$138**

Model 2853 5 VDC input, 0.43" LED display complete with panel mounting clips, edge connector and manual. **\$138**

STOCK DC CURRENT RANGES: 20 & 200 μ A; 2, 20 & 200 mA
STOCK DC VOLTAGE RANGES: 200 mV; 2, 20 & 200 V
OTHER RANGES ON SPECIAL ORDER



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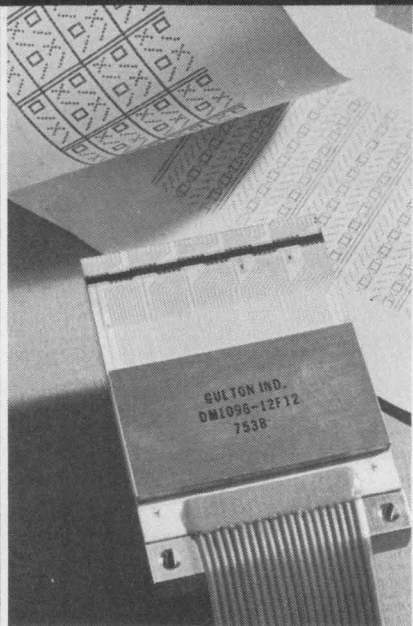
CIRCLE NUMBER 120

KATY INDUSTRIES



INDUSTRIAL
EQUIPMENT
GROUP

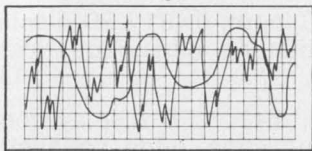
Print Analog/ Graphics Data the easy way



with the versatile
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CIRCLE NUMBER 121

MODULES & SUBASSEMBLIES

10-to-12-bit a/d blends speed and price

Burr-Brown, International Airport Industrial Park, P.O. Box 11400, Tucson, AZ 85734. (602) 294-1431. See text; stock.

If you don't need hermeticity and very-low drift, the ADC84, a new high-speed 10 and 12-bit a/d converter, is said to offer savings over similar units. This converter module comes with built-in clock, comparator, reference and input buffer-amplifier. Conversion times for the ADC84 are 10 μ s for 12 bits and 6 μ s for 10 bits. You can select from analog input ranges of ± 2.5 , ± 5 , ± 10 , 0 to +5 or 0 to +10 V. Linearity error is less than $\pm 0.012\%$ ($\pm 1/2$ LSB) for 12-bits and $\pm 0.048\%$ ($\pm 1/2$ LSB) for 10 bits. Gain and offset errors can be externally trimmed to zero. The converter is guaranteed to be monotonic and to have no missing codes over the operating range of 0 to +70 C. Its gain drift is ± 30 ppm/ $^{\circ}$ C max. Parallel-digital outputs are available in the following codes: complementary-bipolar-offset binary (COB), complementary two's-complement (CTC) and complementary straight-binary (CSB). CSB and COB codes are also available in serial form. Corresponding clock and status signals are provided. All digital input and output signals are DTL/TTL compatible. The module comes in a 32-pin ceramic dual-in-line package. Price for the 12-bit ADC84KG-12 is \$119 (1-24), \$103 (25-99) and \$96 (100-249). The 10-bit ADC84KG-10 is \$100 (1-24), \$96 (25-99) and \$89 (100-249).

CIRCLE NO. 472

Intrusion alarm listens for suspicious sounds

Mountain West Alarm Co., 4215 N. 16th St., Phoenix, AZ 85016. (602) 263-8831.

An electronic decision-maker can select intrusion sounds from normal noises. The A-18 uses existing public address, paging or background-music speakers to monitor protected space. Sounds of intrusion such as breaking glass, hammer blows or footsteps cause the output relay to operate.

CIRCLE NO. 473

S/d adjusts itself to frequency and voltage

Transmagnetics, 210 Adams Blvd., Farmingdale, NY 11735. (516) 293-3100. \$640 (1-4 qty); stock-to-4 wk.

The 1651-03, a 14-bit tracking synchro-to-digital converter, automatically senses and adjusts its operation to input frequencies of 50/60 or 400 Hz and reference voltages of 26 or 115-V rms. Line-to-line reference voltages of 11.8 or 90-V rms are available. Accuracy is ± 4 arc min over the temperature range; models for 0 to +70 or -55 to +85 C operation as well as hermetically sealed and hi-rel units are available. Tracking rate goes up to 16 rps without jitter and the converter has full transformer isolation. It is claimed that the unit will work with 98% of the synchros now on the market. The converter measures $3.13 \times 3.63 \times 0.82$ in.

CIRCLE NO. 474

Drive capacitive loads with 1-kV op amp

Burleigh Instruments, Inc., 100 Despatch Dr., Box 270, East Rochester, NY 14445. (716) 586-7930. \$435; stock to 4 wk.

The PZ-70 can drive large-capacitance or low-impedance loads to the unit's full output voltage capability of 1 kV. Its 20-mA-rms (60 mA-peak) current capability is said to make it the fastest high-voltage dc op amp available today. It features a slew rate of 5 mV/s while its small-signal bandwidth is 5 kHz. Noise and ripple are less than 30-mV rms. This inverting amplifier has a 0-to-200 continuously adjustable gain and a dc-bias adjust of 0 to +1000 V. A fast-acting current-limit automatically shuts the instrument down if its output current exceeds 20 mA rms. A LED indicates that the limit circuit has been activated. A current-limit reset pushbutton is standard. BNC connectors are standard for the direct high-voltage output and the monitor output ($\div 100$). A suitable high-voltage connector is also available. A digital-readout is optional. The rack-mountable unit is $17 \times 3.75 \times 10.5$ in.

CIRCLE NO. 475

The Raytheon 2900 family gains five new members

Whereas: Raytheon is the established alternate source for the Am2901 and Am2909, (franchised distributors stocked), and,

Whereas: Raytheon brought you RAYASM, the powerful micro-assembler available on the NCSS computer network,

Now Therefore: Raytheon announces five additional 2900 family components, giving us a total of seven, To Wit:

2901 A 4-bit Microprocessor Slice—the fastest, most powerful LSTTL microprocessor in the world. With its cycle-saving two-address architecture, the 2901's speed can't be touched.

2905 A 4-bit Bus Transceiver— general purpose open collector bus interface device. Data to the 100 milliamper bus drivers is provided by a 4-bit register with a two-way multiplexer at its inputs. Data from the bus receiver may be held in the 4-bit receiver latch on its way to the three state receiver outputs.

2906 A 4-bit Bus Transceiver with parity —is equivalent to the 2905 but with the addition of an on-chip parity generator/checker.

2907 A 4-bit Bus Transceiver—similar to the 2906 with the two-way multiplexer at the input to the bus driver register elimi-

nated to allow the device to be packaged in the space saving 20-pin DIP.

2909 A Microprogram Sequencer—that can branch anywhere in memory, perform sub-routines, then return with up to four levels of sub-routine nesting. The device is a cascable 4-bit slice which allows addressing of up to 4K words of microprogram with three devices.

2918 A General Purpose 4-bit Register—with two sets of outputs: TTL and three state. This useful combination can reduce your package count for those status, command, and instruction registers which must drive both your control logic and a data bus.

93415 A 1024 × 1-bit Fully Decoded Random Access Memory—for your high-speed data and control stores.

Raytheon LSI is on the move. More 2900 family components soon to come include PROM's, sequencers, look-ahead carry generators, additional RAM's, and other goodies now in process.

For complete details, contact your local distributor or Raytheon Company, Semiconductor Division, Dept. 2900, 350 Ellis Street, Mountain View, CA 94042, (415) 968-9211.

Am 2900 SOLD & SUPPORTED HERE



SEMICONDUCTOR DIVISION

CIRCLE NUMBER 122

FVCs aren't fussy about input shape

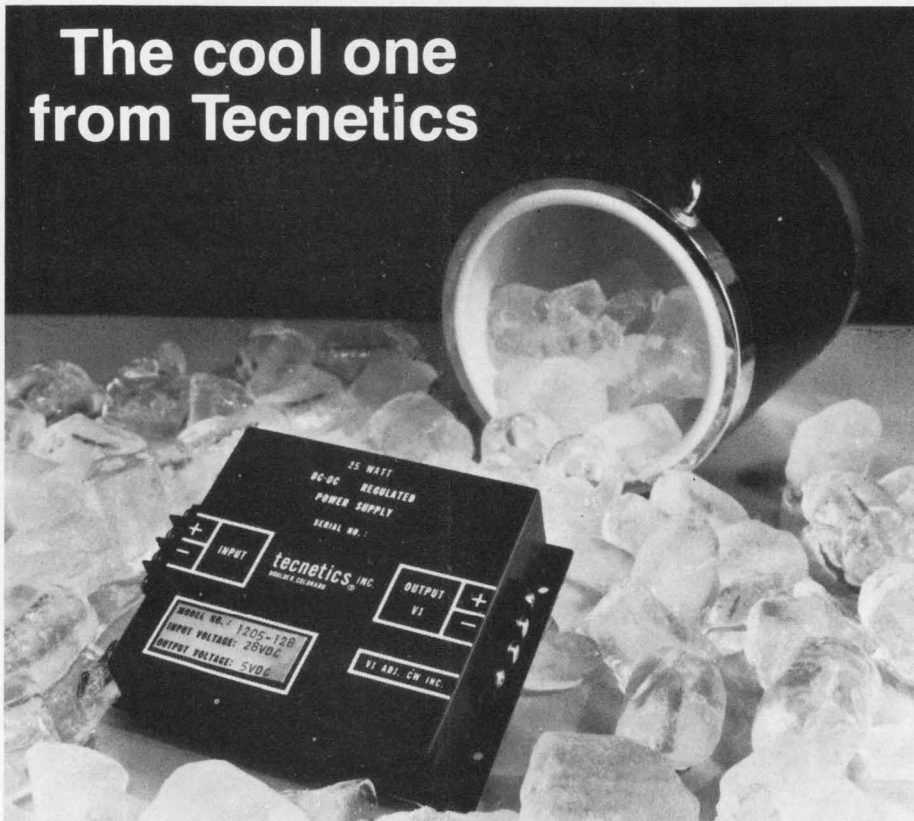
Dynamic Measurements, 6 Lowell Ave., Winchester, MA 01890. (617) 729-7870. Under \$40; 10 days.

The 9001 frequency-to-voltage converters accept ragged input

waveforms without pulse-shaping. Internal timing makes them insensitive to variations in input-waveform duty cycle. They offer standard input-frequency ranges of 100, 20 and 10 kHz, with all units factory-trimmed within 0.4% (max) of full-scale. Typical linearity is within 0.01%, and peak ripple is typically less than 25 mV. Gain tempo is 100 ppm-max. All models operate from a single +15-V supply.

CIRCLE NO. 364

The cool one from Tecnetics



55% efficiency in a 25 watt DC to DC Converter

Why pay for useless heat when you want power? That's the philosophy behind the new high efficiency 1200 Series 25 volt regulated converter from Tecnetics.

With efficiency as high as 55% at full load under normal conditions, an integral heat sink, improved circuitry and a black anodized aluminum case, this converter operates within a range of -20°C ambient to +100°C case temperature.

Available with a single output, this series features full input-output isolation to 500VDC allowing the user to change polarity and prevent ground loops. Compact size and sturdy barrier strip terminals make this the perfect converter for a wide

variety of military, industrial, aerospace and telecommunication applications.

For more information on the 1200, and hundreds of other power supplies, write for our 26 page catalog.

SPECIFICATIONS: 1200 Series 25 watt DC to DC converter

Inputs: 12 ± 2VDC to 48 ± 6VDC
 Outputs: 12, 24, 28 and 48VDC
 Dimensions: 5" x 4.1" x 1.25" (typ)
 Weight: 16 oz.
 Price: Single Output - \$198.00

tecnetics® The Power Conversion Specialists P.O. Box 910,
 1625 Range Street, Boulder, Colorado 80302 (303) 442-3837 TWX 910-940-3246

CIRCLE NUMBER 123

You choose input code with this micro-TTE

Telenetics, 4120 Birch St., Suite 109, Newport Beach, CA 92660. (714) 752-6363. \$28 (1000 qty); stock to 4 wk.

The 7603-01 telephone-tone encoder (TTE), a 32-pin dual-in-line hybrid, is 0.3 × 0.9 × 1.8-in. You get standard telephone dual-tone multiple-frequency (DTMF) outputs from three logic-selectable input codes: 1-of-16 lines, 2-of-8 lines in a row-column keyboard-type matrix, or parallel binary. The device can be hardwired to generate a four-or-eight-digit telephone number on command. Either a dedicated-line or the input data itself actuates the automatic dialing feature. Positive station-identification can be established for individual stations, seeking access to a computer bank, reporting alarms or sharing a communications voice-channel. Applications for the encoder range from manual-keyboard entry (for standard telephone service) to automatic alarms, repertory dialers, point-of-sale terminals and mobile-telephone signaling. This low-voltage PMOS device uses 3 to 8 V with a non-operating current-drain of 500 μA. Signal-frequency stability over temperature and time is controlled by a quartz oscillator. Harmonic distortion is less than 1%.

CIRCLE NO. 365

Analog multiplexer settles in 3 μs

Teledyne Philbrick, Allied Dr. at Rte. 128, Dedham, MA 02026. (617) 329-1600. \$125 (unit qty).

Model 4550 16-channel analog multiplexer contains digital input buffers, decoder logic, analog switches, and an output buffer amplifier—all in a single package. The multiplexer accepts an input voltage range of ±10 V and has an output accuracy of ±0.01%. The input is overvoltage protected even with no supply voltage to the unit. Digital inputs are buffered with Schmitt-trigger logic and have an overvoltage capability of ±19 V. Output settling time for a 20-V step to ±1 mV is 3 μs maximum, including a 1-μs switching time.

CIRCLE NO. 366

Ise introduces five new ways to make the competition turn green.

Your competition probably already thinks they're using the perfect display in whatever it is they make. Let them keep thinking it. While you prove them wrong with a new Itron display. They're designed to make the competition turn green. Which also happens to be the color of the segments.

All 17 of them on the 17-digit Itron. All 5 on the FG-512A1. Next comes an Alfa-Numerical Itron. A Linear-Analog Itron. And a Digital Clock Itron. Five ways to be heartless if you put a little heart into it.

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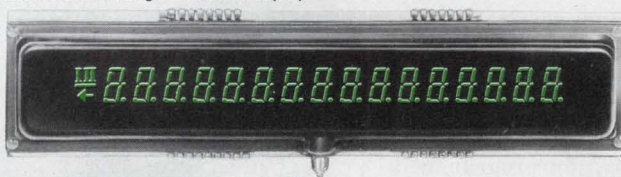
Alfa-Numerical Display



FG209M2

ef = 10V
ec = eb = 40Vp-p
ic = 10mA-p-p
ib = 8mA-p-p
Wd. 205 mm
Lg. 40 mm
Segment 9 mm

Instruments & Large Calculator Display



FG179F2

ef = 7V
ec = eb = 35Vp-p
ic = 7mA-p-p
ib = 5.5mA-p-p
Wd. 170 mm
Lg. 40 mm
Segment 9.5 mm

Instruments & Terminal Units Display



FG512A1

ef = 3.5V
ec = eb = 24Vp-p
ic = 4mA-p-p
ib = 3mA-p-p
Wd. 100 mm
Lg. 40 mm
Segment 12 mm

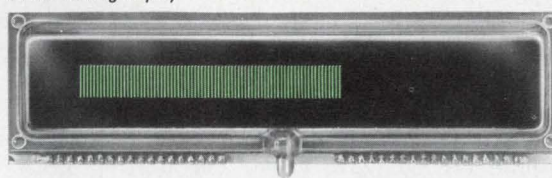
Digital Clock Display



FG425A1

ef = 5.5V
ec = eb = 35Vp-p
ic = 8mA-p-p
ib = 6.5mA-p-p
Wd. 140 mm
Lg. 59 mm
Segment 25 mm

Linear Analog Display



FG120S1

ef = 5.5V
ec = eb = 35Vp-p
ic = 4mA-p-p
ib = 0.2mA-p-p
Wd. 140 mm
Lg. 40 mm
Segment 8 mm

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Texas Instruments SR-56



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PC-100 Lock down printer; for a hard copy of your results; step by step listing of programs, or "debugging" programs. The PC-100 printer may be used with the SR-56 or SR-52.

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CIRCLE NUMBER 125

DATA PROCESSING

**Portable programmer
has personality**



Pro-Log Corp., 852 Airport Rd., Monterey, CA 93940. (408) 372-4593. \$995.

A series-92 PROM programmer, weighing 15 lb, consists of the M920 master control unit and a plug in PROM personality module, packaged in an attache case. Using the same personality modules as the company's earlier series 90 PROM programmer, this system can program all major MOS or bipolar PROMs. Prices for personality modules range from \$350 to \$550. The Series 92 features a 20-mA current loop and is compatible with any terminal, computer or microprocessor development system having this interface. You can use this system to program, list, duplicate and verify PROMs. The duplicate function is controlled by a single pushbutton. Run and fail lights indicate machine status and whether or not a PROM has been successfully programmed. PROMs are mounted into the unit via quick-load, zero-insertion-force sockets. Options include an RS232 interface, a parallel interface and an ultraviolet erase light.

CIRCLE NO. 367

**Data set transmits
over one mile**

Versitron, Inc., 6310 Chillum Pl., Washington, DC 20011. (202) 882-8464. \$544.

A data set accepts serial data and transmits that data over one mile of four-wire cable. The unit is called the Nodem, because it is "not a modem." The Nodem generates a balanced-current signal at synchronous or asynchronous rates up to 19.2 kbit/s.

CIRCLE NO. 368

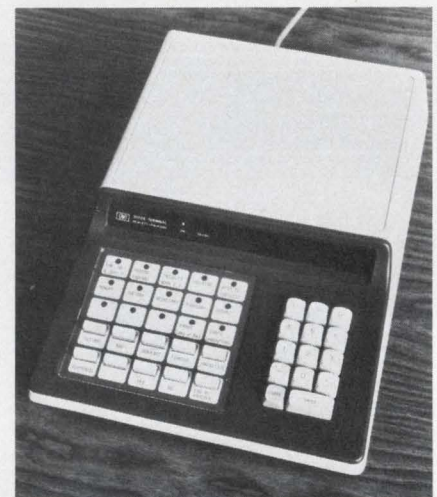
**Label reader senses
a change in color**

Scientific Technology, Inc., 1201 San Antonio Rd., Mountain View, CA 94043. (415) 965-0910. \$169; 2 wk.

A color label sensor, the Model 8010 Omnimark, uses a multi-colored solid-state light source and matched detector. The unit can detect all colors including green or blue. In operation, a background color reference is established from the surface under inspection. When the color changes as the unit scans, an output is generated. Two separate outputs are provided, one indicating a change from a dark background to a light mark and one from light to dark. Each output is a 5-V digital signal. The sensor-head size of the Model 8010 is 35 × 74 × 48.25 mm.

CIRCLE NO. 369

**Numeric-data terminals
can be tailored**



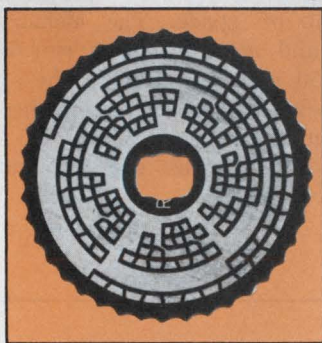
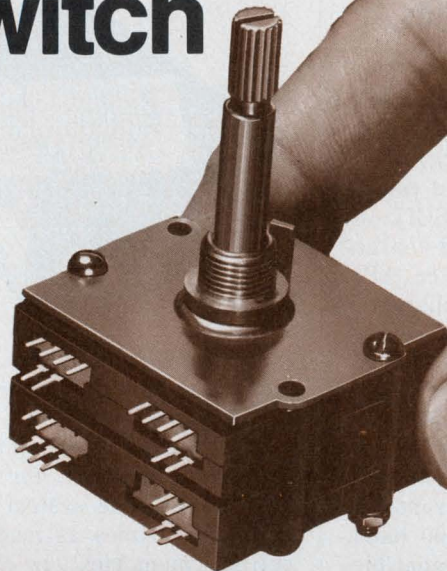
Hewlett-Packard, 1501 Page Mill Rd., Palo Alto, CA 94304. (415) 493-1501. 10-up prices: \$1308 (3070A); \$1143 (3071A).

The 3070A and 3071A numeric-data entry terminals have a set of keys and LED indicators that can be labeled by the user to match special computer programs. The 3070A operates with the manufacturer's computers, and the 3071A connects to other type computers. Both models have numeric-only keypads and 16-digit displays. The 3070A can also connect to an industry-standard bus, the HPIB. The terminals weigh 10.3 lb and measure 10.9 × 4.6 × 15.7 in.

CIRCLE NO. 370

New unique design OAK rotary switch

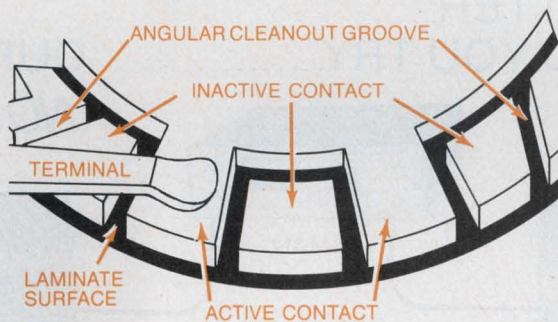
Accurate.
Dependable.
Long life.
Up to 60 positions.
Logic programmable.
Low cost.



OAK ROTOR DESIGN

The Oak Communicator Series switch features a patent-applied-for rotor design for long term contact registry and integrity. Programming is accomplished on a metal-clad, laminated rotor of exclusive construction.

High dependability is assured because the stationary wiping contacts never touch the insulation surface. Instead, they move from electrically live to electrically inactive metal surfaces. Tracking is eliminated due to Oak's exclusive clean-out grooves and rotor circuit design. In addition erosion or the formation of particles between contact and insulation surface is drastically reduced.



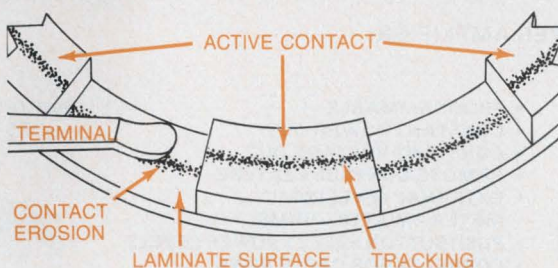
Intermittent opens or shorts are almost impossible.

Complex wiring problems are eliminated, because all switching logic, wiring and contact arrangements are programmed within the factory-assembled switch.

Small size (1.665 x 1.5 x 0.4), simple construction, accurate registration and low cost permit the Oak Communicator Series to be adapted to almost any application.

For additional information and specifications, contact your nearest Oak sales office or call 815-459-5000.

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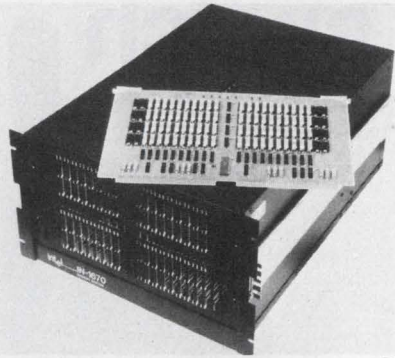
CRT terminal handles APL characters

Hewlett-Packard, 1501 Page Mill Rd., Palo Alto, CA 94304. (415) 493-1501. \$4100 (single qty).

The 2641A CRT terminal can be switched from APL to ASCII operation. It offers a full 28-character APL set, a 64-character APL overstrike set and a 64-character upper-case Roman set that can be optionally expanded to 128 characters. The terminal's CRT displays the complete APL overstruck characters. It operates either in an asynchronous or synchronous (bi-sync) mode at selectable transmission rates from 110 to 4800 baud. The unit is RS232C-compatible, and transmits synchronous ASCII data point-to-point in character or block mode. A multipoint polling option allows as many as 32 terminals to be connected on the same line. The unit's 5 x 10-in. display has a 24-line by 80-column format.

CIRCLE NO. 371

Memory system requires 1/4 the space of others



Intel Memory Systems, 1302 N. Mathilda Ave., Sunnyvale, CA 94086. (408) 734-8102.

The in-1670 offers up to 4 Mbyte of add-on memory for the DEC PDP-11/70. The system is said to offer four times as much as competing memories in the same amount of space. The memory's cycle and access periods run 750 and 550 ns, respectively. The system includes error correction checking and error logging circuits. All single-bit failures are automatically corrected.

CIRCLE NO. 372

Optical bar-code reader observes from 0.5 in.

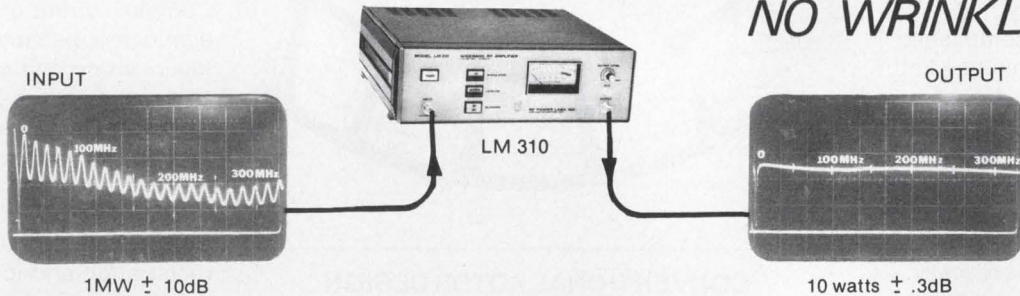
Identicon Corp., One Kenwood Circle, Franklin, MA 02038. (617) 528-6500. \$400 (single qty).

The Model 515 reads codes printed on badges or envelopes. It is available in two versions, one reading at a distance of 0.25 in., the other at 0.5 in. from the reader's face to the label. The depth of field is greater than 0.125 in. The units resolve bar-to-bar spacings down to 0.008 in. The Model 515 uses a large-area silicon photodetector and a diamond-shaped reading aperture, so that the signal is integrated over 0.3 to 0.36 in. of bar length. This allows the reader to ignore voids in dark bars and spots in white bars. The optical system is sealed by a hard-surface sapphire window. The internal light source consists of infrared LEDs operating at 900 nm. Output is a 100-mV signal at a dynamic impedance of less than 100 Ω. Bandwidth is in excess of 20 kHz. Both gain and offset are adjustable.

CIRCLE NO. 373

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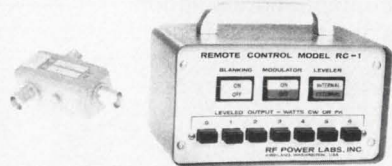
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Paper-tape reader connects to the PDP-8A

Forte Technology, Inc., 15 Strathmore Rd., Natick, MA 01760. (617) 655-5885. \$1195; 30 days.

The Model 400 paper-tape reader connects to the DEC PDP-8A computer. It is interfaced with DEC software codes by an eight-word interface. Six additional words and flags remain on the interface for other data input requirements. The system includes a 150 char/s photoelectric reader, a power supply, cabinet, cable, and the eight-word interface board.

CIRCLE NO. 374

Programmer also simulates PROMs



Electro Design, Inc., 8141 Engineer Rd., San Diego, CA 92111. (714) 277-2471. \$3000; 60 days.

The ED6000 simulates and programs TTL-compatible PROMs. The instrument consists of an addressable simulator, a cassette-tape unit and a programmer. Data come either from a hex keyboard having address and data LED readouts, an 8-bit data bus, RS-232 or current-loop driver. A switch controls data transfer between the ED6000 and external circuits through a plug-in cable connected to a 16 to 24 pin socket. Address incrementing is either automatic or manual. Data are accessible in 4-bit increments.

CIRCLE NO. 375

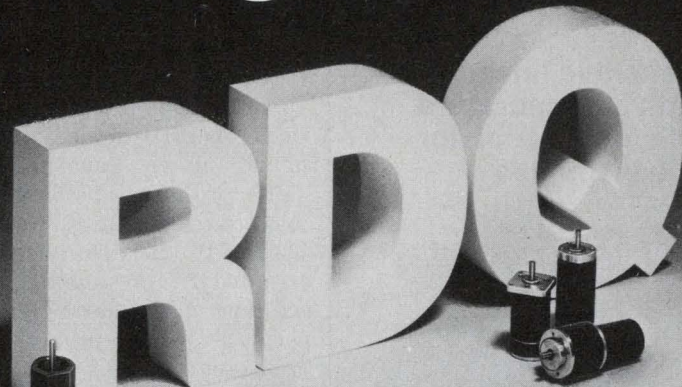
Acoustic-coupler kit fits TI's 733 terminal

Omnitec Corp., 2405 S. 70 St., Phoenix, AZ 85034. (602) 258-8244. \$289.32 (1 up); stock.

An acoustic-coupler kit enables Texas Instruments' Model 733 terminal to communicate over phone lines. The kit, called the Model 1733, is installed in 10 minutes. All parts, including modem card, muff assembly and hardware are included.

CIRCLE NO. 376

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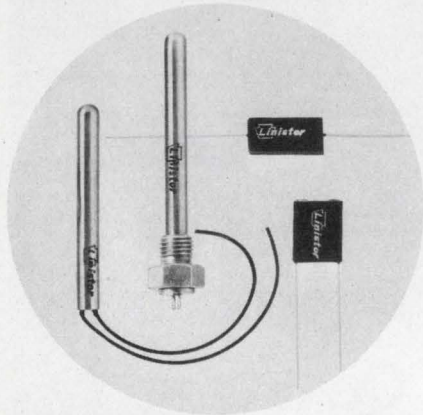


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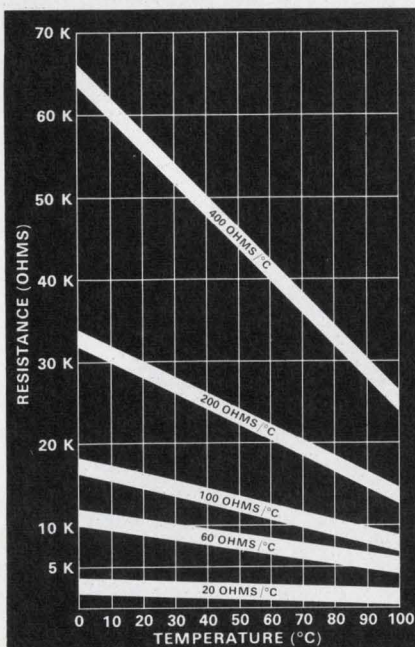
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CIRCLE NUMBER 129

DATA PROCESSING

Computer-in-a-cable drives four tape units

Computer Automation, Inc., 18651 Von Karman, Irvine, CA 92713. (714) 833-8830. \$300.

A parallel-interface magnetic-tape intelligent cable (MTIC) drives up to four phase-encoded (PE) or nonreturn-to-zero (NRZ) magnetic-tape units. The MTIC is used with the manufacturer's distributed I/O system and an external-tape formatter. The unit incorporates microprogrammed control using a self-contained processor that supports standard magnetic tape-drive control functions. The functions include transfer, device protocol, device status monitoring and interrupt generation. The control processor is embedded in a 6-ft cable near the tape formatter, and mounts to any flat surface by screws or adhesive. The formatter is compatible with standard tape speeds up to 75 in./s, with densities from 200 to 1600 char/in., and with seven or nine tracks.

CIRCLE NO. 377

Interface unit relays data at 1-Mbaud rate

Computrol Corp., Berkshire Industrial Park, Bethel, CT 06801. (203) 792-4060. \$2840; 120 days.

The Model CCI-4000 transmits data over coaxial cable at a 1 megabaud rate. The unit connects to a 16 or 32 bit-per-word computer, or peripherals. Up to 64 CCI-4000s, each having a unique address, can connect to one cable. The unit accepts data in the form of two 16-peripherals. Up to 64 CCI-4000s, bit words, then serializes these data and formats them into a 32-bit word. Current drivers couple the serial data into the coaxial cable. In a network, one computer initiates data transmission through its own CCI-4000. When another unit recognizes its address it transfers the received data to its own associated computer. Optional peripheral-driver boards can also plug into a CCI-4000. One board drives eight individually-addressable peripherals and costs \$795. Up to five peripheral-driver boards may be installed in a CCI-4000.

CIRCLE NO. 378

Printer head moves under software control



Practical Automation Inc., Trap Falls Rd., Shelton, CT 06484. (203) 929-5381. \$200-up (single qty); 6 wk.

The DMTP-6 series printer makes the ASCII set of 64 characters. The printer-head movement is under software control. Both the pitch of 8, 10 or 12 character/in. and character enhancement can be programmed. Characters are formed by a 7 × 5 needle matrix that forms characters with dimensions of 0.110 × 0.08 in. Three models of the series take rolls of paper having widths of 3.438, 6 or 8 in. Other models accept fanfold paper. The units print, on ordinary paper, one to five copies. The paper advances with a programmable motor or ratchet mechanism, depending on model. The effective print rate is 120 char/s. Input is via eight-bit parallel characters, through serial RS-232C or 20-mA current loop.

CIRCLE NO. 379

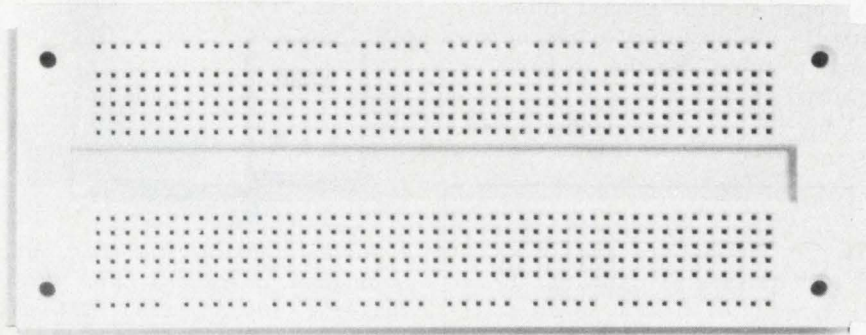
Minicomputer has a standard adapter port

General Robotics Corp., 57 N. Main St., Hartford, WI 53027. (414) 673-6800. \$4995 (5-9); 30-45 days.

The GRC11/03 central processor has the DEC LSI-11 microcomputer module, and a PDP-11 Unibus adapter port. The GRC11/03 includes the extended instruction set, floating-point arithmetic, 20-k words of RAM, memory addressing capacity of 512-k words and a serial I/O module with switch selectable data rates. It also has a pseudo switch register accessible with software or ODT, and eight additional dual-height module slots.

CIRCLE NO. 380

Solderless breadboards easily handle 600-mil DIPs



Continental Specialties Corp., 44 Kendall St., P.O. Box 1942, New Haven, CT 06509. (203) 624-3103. Unit-qty prices: \$9.95 (300); \$10.95 (600); stock.

Solderless breadboards never seem to have enough tie points when you design circuits with 600-mil wide DIPs. To solve this prob-

lem, Continental Specialties developed the Experimentor 600, a solderless breadboard with 550 tie points and 600-mil center spacing.

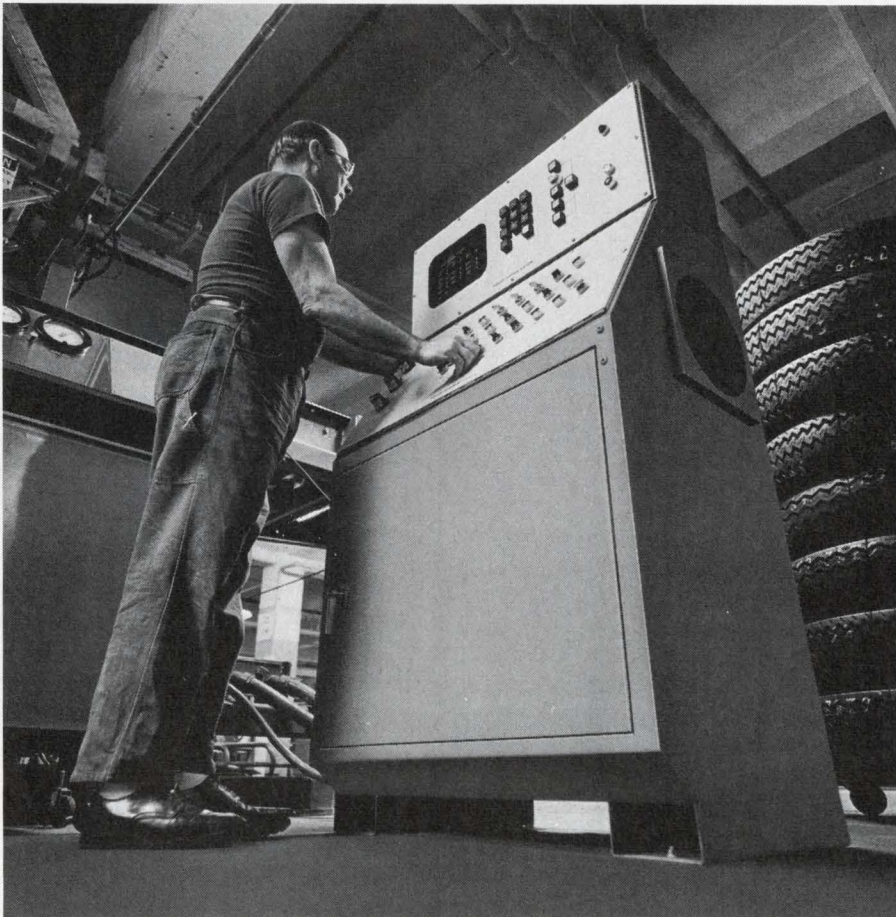
Although many of the older 300-mil center solderless breadboards offered at least as many tie points, about 30 to 50% of these points were of no use since the 600-mil-

wide DIPs covered them. On the old sockets only one or two tie points for each DIP lead were available; with the Experimentor 600, four points for each pin are available.

There are two versions of Continental Specialties' breadboard available: the Experimentor 600 and the Experimentor 300. Both have a thickness of 0.375 in. and a length of 6 in., but the 600 has a width of 2.4 in. while the 300 is only 2.1 in. wide. The 300 has a 0.3-in.-wide center channel and the 600, a 0.6-in.-wide channel.

Sockets can be snapped together and mixed or matched to provide optimum configurations for any circuit breadboard. Both models also have two 40-point power busses.

CIRCLE NO. 310



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 ELECTRICAL ENCLOSURES

CIRCLE NUMBER 130

PACKAGING & MATERIALS

Thermocouple connector features small size

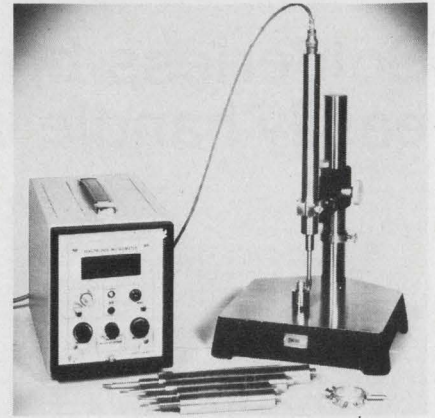
Omega Engineering, Inc., Box 4047, Stamford, CT 06907. (203) 359-1660. \$3.70 per pair (1-10); stock.

The SMP series of thermocouple connectors is claimed to be the smallest quick-disconnect thermocouple connector available. The

series comes in 10 different thermocouple calibrations, including tungsten-rhenium. Each connector consists of male and female mates, with insulation of glass-filled nylon. The connector takes fine-gauge thermocouple wires and protection tubes. Tube clamps are not required because each male connector is supplied with several different-sized brass bushings to which protection tubes can be soldered or braised.

CIRCLE NO. 381

Digital micrometer resolves 0.0001 in.



Columbia Laboratories, Inc., Macdade Blvd. & Bullens Lane, Woodlyn, PA 19094. (215) 532-9464. See text.

The CM-400-D digital micrometer displays displacement data directly in inches. It permits the operator to resolve changes in displacement to ± 0.0001 in. Front-panel indicators monitor the status of the control circuitry, warn of over, within or under a set tolerance reading. System accuracy is 0.25 to 1.0%, full scale, depending on the transducer used. It can be interfaced with computers or remote data printout systems. A front-panel potentiometer provides a $\pm 2\%$ full-scale vernier adjustment to calibrate the system to standard gauge-block references. For \$1295 you get the readout unit, one transducer, stand, mounting adaptors and test points.

CIRCLE NO. 382

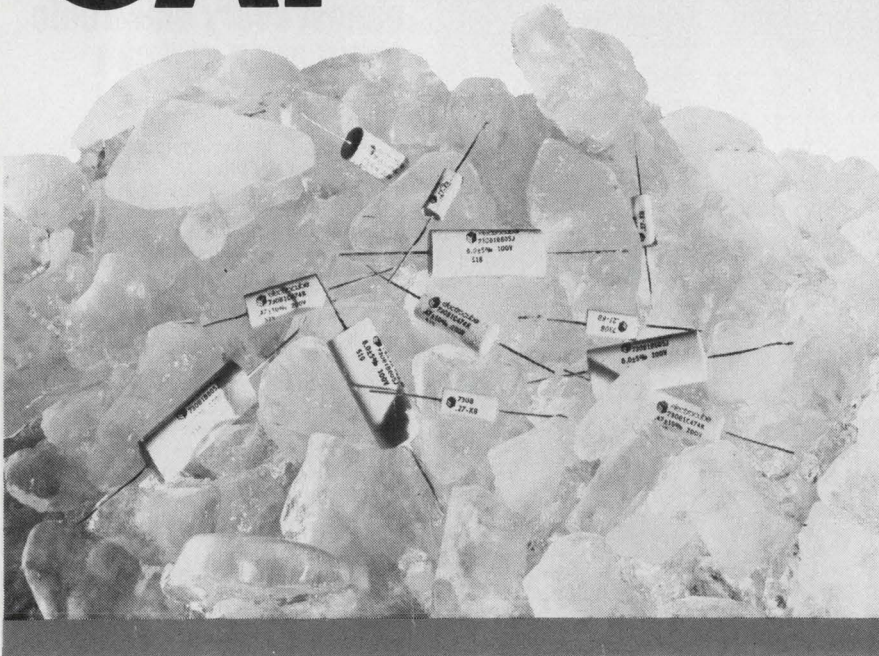
electrocube capacitors

...in new combination plastic film models, offer extremely low temperature coefficients in a miniature 100 and 200 VDC line. This unique combination material results in a lower priced capacitor than the polycarbonate units now used in low TC applications. For higher voltage units, consult the factory. Get complete information on these unique capacitors from Electrocube, 1710 So. Del Mar Ave., San Gabriel, CA 91776; (213) 573-3300.

FREE...data file on request



COOL CAP



... also available in REEL PACKAGING.

Paper-like ceramic resists 2300 F

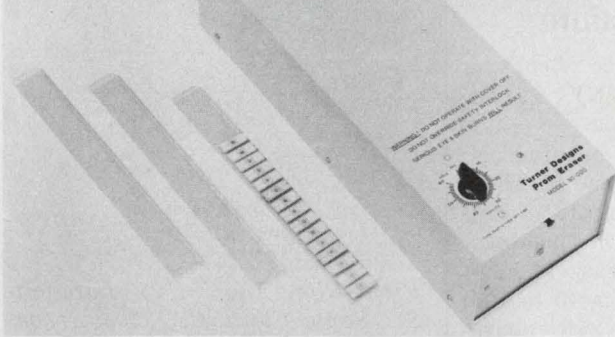
Cotronics Corp., 5008 Ave M, Brooklyn, NY 11234. (212) 531-9376. Prices: \$122 (0.02 in., 400 ft²), \$126 (0.04 in., 250 ft²), \$124 (0.08 in., 120 ft²).

The 300 series of ceramic paper has a melting point of 3200 F. The paper can be used to 2300 F. It is made from high-purity refractory fibers containing no asbestos. It can be cut with ordinary hand scissors and formed into complex shapes. The ceramic paper can be folded, wrapped or rolled. The paper comes in thicknesses of 0.020, 0.040 and 0.080 in. Rolls of the material are 24 in. wide.

CIRCLE NO. 383

CIRCLE NUMBER 131

PROM ERASER



Designed specifically to deliver a calibrated dose of ultraviolet at the correct wavelength and intensity to assure long-term data retention. Tested by leading manufacturers of EPROMs, it meets data-sheet requirements of Intel, National, AMD, AMI, Mostek and others.

- SAFE - Operator protected against uv and ozone
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- CONVENIENT - Metal-tray loading
- FLEXIBLE - One to 60 PROMS per cycle
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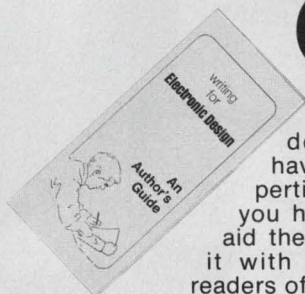
Write or call for further data, or to order

TURNER DESIGNS
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 Mountain View, CA 94043
 415/965-9800

CIRCLE NUMBER 132

AUTHOR'S GUIDE



If you've solved a tricky design problem, if you have developed special expertise in a specific area, if you have information that will aid the design process... share it with your fellow engineer-readers of *Electronic Design*.

Articles you have authored not only raise your own professional status, but help build your company image as well. The readers benefit, your company benefits.

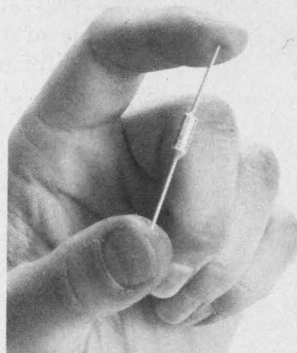
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It's easy to write for *Electronic Design*, but it's often hard to get started. Send for your copy of our Author's Guide today.

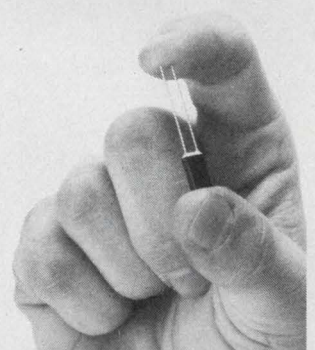
Circle No.
250

Want A Safer Product And Lower Manufacturing Costs Too?

On the one hand choose the **MICROTEMP®** thermal cutoff



On the other hand, don't overlook the new **PICOTEMP** thermal cutoff



A reliable, accurate easy to install, "one shot" thermal limiter.

- temperature tolerance— $\pm 1.7^{\circ}\text{C}$.
- temperature ratings— 58° to 242°C . (136° to 468°F .)
- current capacity—up to 30 amps at 240 VAC.
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- economical
- easy to install—assorted terminations, mounting packages and insulations available.
- Recognized under the Component Program of Underwriters' Laboratories, Inc. UL File #E40667A. CSA approved. BSI Certificate #5041 approved. Recognized by MITI and VDE. Military approval.

Used where installation or space restrictions rule out MICROTEMP® thermal cutoffs.

- temperature tolerance— $+0^{\circ}\text{C}$.— -3.3°C .
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- compact—.236" x .389" x .087".104" (exclusive of leads).
- economical
- Package is completely insulated, leads are 26 gauge silver plated wire.
- Recognized under the Component Program of Underwriters' Laboratories, Inc. UL File #40667A. MITI approved. CSA approved.

Both devices are completely sealed against the atmosphere. Because of their unique design and construction, they won't derate. And they're unaffected by age or extended use. You not only get positive, yet low cost protection against malfunctions in circuits and components caused by equipment failure or user abuse, but you eliminate costly and unnecessary service calls caused by nuisance tripping.

PICOTEMP or MICROTEMP? Which is best? Depends on your needs. Tell us about them.



MICRO DEVICES



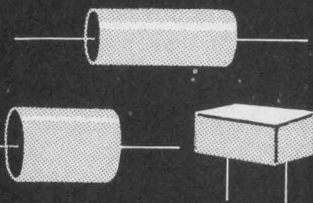
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 DAYTON OH 45439 513-294-0581

CIRCLE NUMBER 133



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CIRCLE NUMBER 135

PACKAGING & MATERIALS

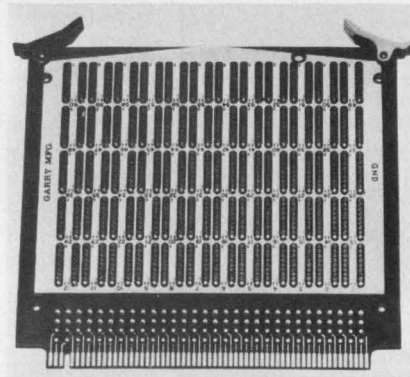
High voltage bushings operate in a vacuum

Ceramaseal, Inc., New Lebanon Center, New York, NY 12126. (518) 794-7800. See text.

A line of insulating bushings is specified for high-vacuum use. They leak at a rate less than 1×10^{-9} atm/cc/s of helium. The bushings are open-ended with gaskets having voltage ratings from 10 to 100 kV rms. Flashover is 25% above rated voltage, and all units leak less than 5 pC. The bushings operate continuously at 150 C and intermittently to 200 C. They have either porcelain insulation and stainless steel conductors, or high-alumina ceramic with nickel-iron conductors. For the 50-kV bushing, part no. 947-B-9373-1, the 10-up price is \$38.

CIRCLE NO. 384

DIP-socket board has a card-edge connector

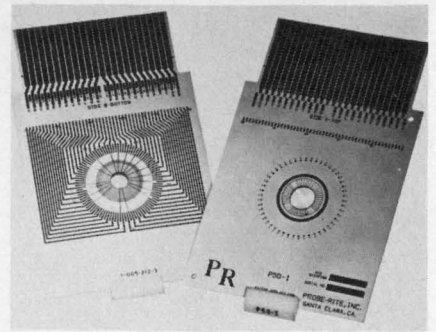


Garry Mfg. Co., 1010 Jersey Ave., New Brunswick, NJ 08902. (201) 545-2424. \$120 (1-4); 2-4 wk.

A series of wire-wrappable boards comes with 60 DIP positions and a 61-pin card-edge connector. Designated the EP120 series, the boards are constructed of 0.125-in. glass epoxy. The boards also have 2-oz solder-plated copper voltage and ground planes. Options include one, two, or three-level wrapped-wire posts, 14 or 16-pin positions, and voltage and ground sockets. Each DIP position can be provided with a socket for a decoupling capacitor. The socket terminals may have 10, 30, 40 or 100 μ m. of gold plating, over 50 or 100 μ m. of ductile nickel plating.

CIRCLE NO. 385

PC cards hold up to 50 wafer probes



Probe-Rite, Inc., 2725 Lafayette St., Santa Clara, CA 95050. (408) 249-1255. See text; stock to 2 wk.

The P50 probe-card series holds semiconductor-wafer probing and holding fixtures. The series contains four basic cards and each card holds 50 individual probe points. The P50 series cards are fabricated on white laminate for photon shielding. They contain die stepping, serialization and product identification. Either 48-pin or 110-pin card-edge connectors are available. You may also build your own card to accept three types of wafer-probe point assemblies. Prices run \$18 for a blank card to \$300 for a complete assembly.

CIRCLE NO. 386

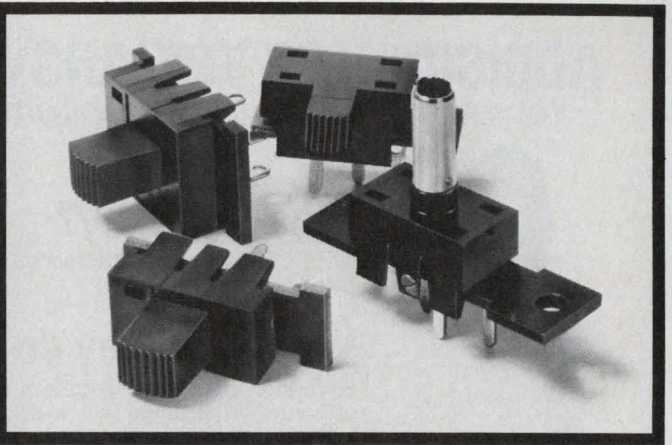
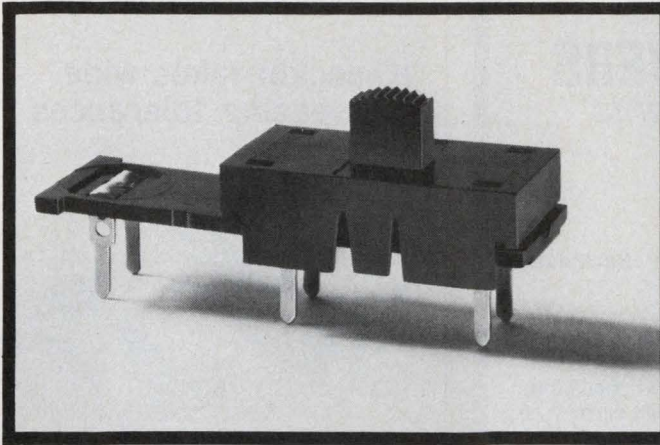
Kit contains 17 types of epoxies



Tra-Con Inc., Resin Systems Div., 55 North St., Medford, MA 02155. (617) 391-5550. \$25 (single qty).

The 51-piece EpoxyLab kit contains 17 different epoxy adhesives. The assortment includes fast curing, thixotropic, heat resistant, rigid, low outgassing, steel filled, flexible, high dielectric, low density, low viscosity, high impact, and clear epoxies. Each adhesive comes in an individual package that contains resin and hardener.

CIRCLE NO. 387



We've come out of our shell and gone into isolation with our new SL line.

UID just introduced the most versatile and cost-efficient line of slide switches available: the new Shell-less SL switches. Star of the SL line is our RF isolation switch, FCC-tested and approved in a video game under TV-199. But UID's Shell-less SL switches are practical choices for any installation where rugged, durable, high-quality slide switches are required.

UID's SL series has no metal shell, resulting in reduced stray radiation. And since the Shell-less switch weighs about 60% less, you'll save on shipping costs. Our SL's have a tough, self-lubricating nylon construction that meets 94V-2 Flammability specs, and also meets UL 1054 and the new UL impact standards for portable

appliances. The SL's highly-conductive silver-plated contacts provide a life of over 10,000 cycles. Positive detenting provides a reassuring quality "feel."

For more information and a free sample, come out of your shell and write or call Sal Mucario, UID Electronics Division, AMF Incorporated, 4105 Pembroke Road, Hollywood, Florida 33021. Telephone (305) 981-1211.



CIRCLE NUMBER 136

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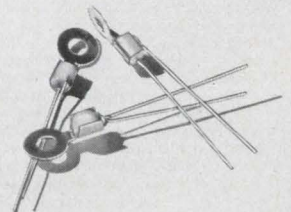
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CIRCLE NUMBER 137

ELECTRONIC DESIGN 24, November 22, 1976

semiconductor overload protection... murata's posistors® make it simple

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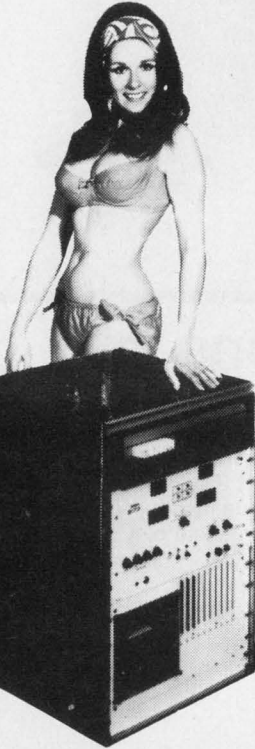
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CIRCLE NUMBER 138

225

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CIRCLE NUMBER 139

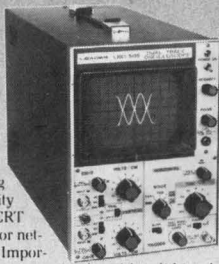
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your lowest priced DUAL TRACE 5" SCOPE. SYNC'S TO 35 MHz

COMPLETE PRICE
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Accurate operation is the key and error-free results your bonus! With this unique 5" dual chan/dual trace scope you can test b & w, color, audio or CB circuits. The advanced design lets you read between ranges in any position as easily as you can with analog VTVM's or VOM's. Features high reliability PC board construction; a high intensity CRT with excellent contrast; and special attenuator networks for proper pulse shape and stability. Important plus features are: Automatic X-Y, separate or simult. sweep mode display for ch 1 & 2 . . . alternate, chopped, auto or norm trigger; including pre-set TV-V and TV-H comp.; direct RF signal input to 100 MHz; and X5 sweep mag. to 100nanosec. The LBO-506A not only performs every test with accuracy and minimal chance for error, it also checks delay lines and stereo amplification . . . checks for proper color burst phase and fly-back pulse arrival . . . and, you'll use it for any and all measurements to test color circuitry stage by stage. Whatever your needs, the LBO-506A offers solid dependability; and easy-to-use operation!



Includes all accessories... worth \$45 and more!

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- Automatic Trig.
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- DC to 10MHz Bandwidth: Sync's to 35MHz.
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LEADER
Instruments Corp.

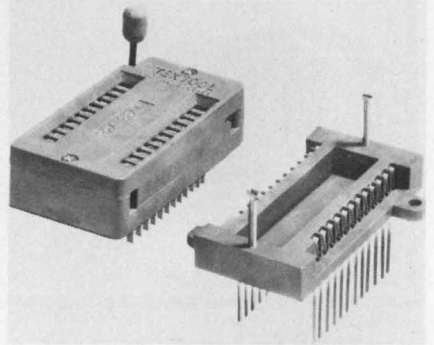
Tests More . . . Tests Better . . . for Less.

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CIRCLE NUMBER 140

PACKAGING & MATERIALS

IC socket takes wide pin-spacing tolerances

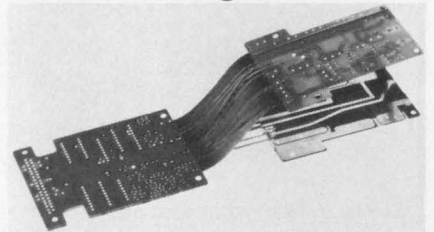


Textool Products, Inc., 1410 W. Pioneer Drive, Irving, TX 75061. (214) 259-2676. Socket, \$2.93-\$5.74; receptacle, \$4.98-\$9.41 (100-up).

The Zip Dip II series consists of disposable zero-insertion-force sockets that plug into chassis mounted receptacles. Each socket features an enlarged entry that accepts a wide range of pin spacing. The IC pins may vary ± 0.13 in. from the nominal row spacings of 0.3 to 0.6 in. Contacts in the rows are spaced in increments of 0.1 in. Sockets are available for ICs with 14 to 40 pins. The socket has a typical life of 25,000 to 50,000 IC insertions. A built-in "stop" ensures that the locking handle can't be overstressed. Top mounted assembly screws facilitate replacing worn internal parts.

CIRCLE NO. 388

PC board is either flexible or rigid



Schöeller and Co., Elektronik GmbH 3552 Wetter, Postfach 20, West Germany.

A multilayer circuit board, called Multiflex, can be made partly rigid and partly flexible. The Multiflex circuits contain flexible printed wiring inside a rigid multilayer PC board. The flexible layer extends beyond the rigid material to provide electrical connections to other PC boards, connectors and controls.

CIRCLE NO. 389

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For computer applications,
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CIRCLE NUMBER 141

Design better equipment

OEM servo recorder

Esterline Angus original equipment Miniservo® recorder gives more design freedom. The basic unit lists at just \$320, with generous quantity discounts available. Your customers benefit from reliable simplicity, easy use, and state-of-the-art. Nationwide repair network backs every unit.

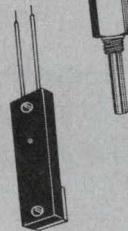
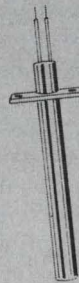
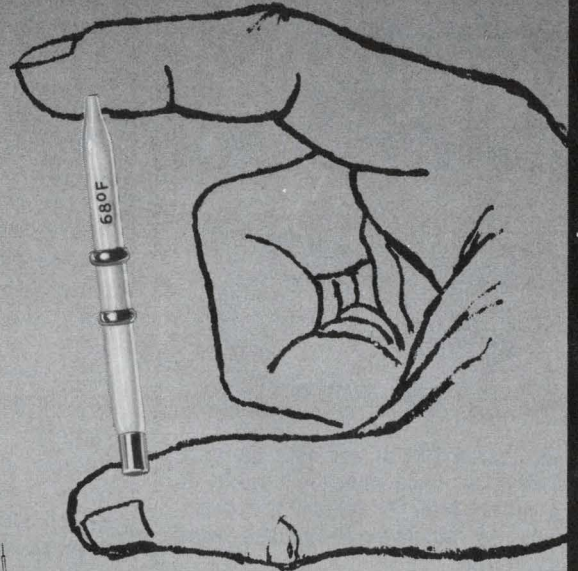
Short specifications: 100 mm-wide Z-fold or rolled servo chart recorder with 100 MVDC (10 MV optional) and 4 chart drive choices, 0.5 sec. response, $\pm 0.5\%$ accuracy, disposable ink/pen cartridge. Request Bulletin F612. Esterline Angus Instrument Corp., P.O. Box 24000, Indianapolis, IN 46224, Tel. 317-244-7611.



CIRCLE NUMBER 142

ELECTRONIC DESIGN 24, November 22, 1976

it's so simple



why didn't I think of this thermostat?

More and more engineers are asking themselves that question when they see and learn of the advantages of using P.S.G.'s Mercury and Solid State Thermostats.

ACCURACY	$\pm .05^{\circ} \text{C}$ to 2°C
DIFFERENTIAL	$.05^{\circ} \text{C}$ to 10°C
SHOCK	100 G
VIBRATION	20G at 2000 cycles per second
LOAD	5 M.A. to 5 amps
SIZE	length 5/16 and up - diameter 3/32 and larger

All types of mountings. Simple, no moving parts and they are low cost, ranging from \$2.10 each up (depending on model and quantity).

We find it simple to solve temperature control problems. Let us have yours.

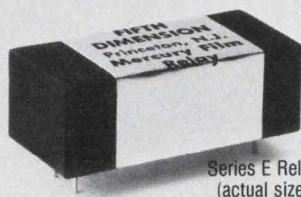


PSG Industries, Inc.
MANUFACTURER OF PRECISION THERMO AND ELECTRONIC CONTROLS
1225 Tunnel Road, Perkasie, Pa. 18944



CIRCLE NUMBER 143

1 Relay Miss every 2-Billion Cycles



Series E Relay
(actual size)

We tested 129 of our new Series E Relays at loads from dry circuits to 3 Amps. After 35-billion operations, only 10 single-cycle misses were monitored.

Series E Relays offer:

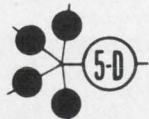
- Indefinite life
- No contact bounce
- Operation in all positions
- Contacts stable to ± 0.015 ohms over life
- Reliability at dry circuit or power loads
- Self-healing contacts
- Hermetically sealed contacts
- 1250V rms contact breakdown
- Low cost



LC2 Switch Capsule
(actual size)

Series E Relay uses a rugged LC2 welded capsule rather than a fragile glass reed switch. This patented design holds a film of mercury securely to the metal walls of the capsule. With every operation, the mercury film renews the switch contacts. You get the reliability of mercury relays, but with complete freedom of mounting orientation. LC2 welded capsule reliability is proven by hundreds-of-thousands of units in the field, as well as billions of cycles under stringent laboratory conditions.

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Princeton, N.J. 08540
Tel: (609) 452-1200

CIRCLE NUMBER 144

INTEGRATED CIRCUITS

Digital clock circuits provide six functions

Intersil, 10900 N. Tantau Ave., Cupertino, CA 95014. (408) 996-5000. Die prices: \$6.20 (100-up); stock.

Two digital clock circuits, the ICM7210 and ICM7210A, offer 4-digit displays and six-function capabilities. The 7210A can drive liquid crystal displays to read out hours, minutes, day, date, month and seconds. It has a perpetual calendar that needs resetting only once every four years. The ICM7210, in addition to all of the 7210A's features, provides outputs for AM/PM annunciators. Both circuits contain an oscillator, frequency divider, alphanumeric decoder, voltage multiplier, voltage doubler/tripler and 32-Hz display drivers. The only external components required for a complete system are a display, one 1.5-V silver-oxide battery, a trimming capacitor, two spst switches, and two or three external capacitors for the voltage doubler/tripler. Power consumption with the display off is 2 μ A typical. Both circuits are guaranteed to operate over a -10 to $+60$ C range.

CIRCLE NO. 390

8-decade counter drives BCD & 7-segment units

LSI Computer Systems, 22 Cain Dr., Plainview, NY 11803. (516) 293-3850. \$8.15 (100-up); stock to 6 wks.

A cascadable eight-decade up-counter, the LS7030, can operate from dc to 5 MHz. All counter outputs are latched and data are available in multiplexed BCD and seven-segment format. Digit strobes are guardbanded so they occur totally within valid BCD data times. The multiplexed scan counter may be driven by an external clock or by an on-chip oscillator whose frequency is 500 kHz. The on-chip oscillator frequency can be reduced by adding an external capacitor. Leading zero blanking is used to make the display readable. The circuit operates from a single power supply, between 5 and +18 V and is supplied in a 40-pin DIP.

CIRCLE NO. 391

Sampler kit contains 13 interface circuits

Standard Microsystems, 35 Marcus Blvd., Hauppauge, NY 11787. (516) 273-3100. \$99; stock.

To aid the designer of computer peripheral equipment, Standard Microsystems has developed a sampler kit of 13 MOS LSI interface circuits. Included in the kit are three UARTs, one USRT, one dual baud-rate generator, one single baud-rate generator, two keyboard encoders, one general interface controller, two character generators and two quad programmable static shift registers. All device data sheets, along with the ICs, are housed in a looseleaf binder.

CIRCLE NO. 392

Three-terminal regulator series has 7 fixed units

Texas Instruments, P.O. Box 5012, Dallas, TX 75222. (214) 238-2011. \$1.38 (100-up); stock.

The 7800 and 7900 series of three-terminal positive regulators are available with seven fixed output voltages. Ranging from 5 to 24 V, the regulators are designed for use in logic systems, instrumentation, hi-fi and other solid-state applications. They are pin-for-pin equivalent to the Fairchild 7800 and 7900 series. The units are housed in plastic TO-220 packages. Regulator features include internal thermal-overload protection, output transistor safe area protection and internal short-circuit current limit.

CIRCLE NO. 393

IC timer has delays of microseconds to hours

Micro Components Corp., 99 Bald Hill Rd., Cranston, RI 02920. (401) 463-6000. Less than 50¢ (OEM qty.); stock.

The MCC-555 timer circuit, available in a standard 8-lead DIP, acts as either a time delay (monostable mode) or as an oscillator (astable mode). All input-output terminals are TTL/DTL compatible. Resettable time delays ranging from microseconds to hours can be accurately obtained over the single power supply range from 5 to 15 V. The output of the MCC-555 can either sink or source up to 200 mA.

CIRCLE NO. 394

New Low Cost TIME CODE GENERATOR/READER



Time Code Reader \$890.
Generator/Reader \$1265.

The new LOW COST Series 9000 Time Code Units generate and read serial IRIG Time Codes used in analog magnetic tape instrumentation, hard wire transmission and telemetry systems. In addition, they provide buffered parallel BCD outputs, TTL compatible, for digital storage devices and computer inputs. Options include Multi-code units, Day-of-Year Calendars and Millisecond BCD outputs.

Write or call Chrono-log Corporation, 2 West Park Road, Havertown, Pa. 19083, (215) 853-1130



CIRCLE NUMBER 145

PHOTO ETCHTM PRINTED CIRCUIT KIT Makes circuits **THREE WAYS**

- 1 FULL SCALE ARTWORK MASTER
- 2 MAGAZINE ART ILLUSTRATION → FILM POSITIVE → NEGATIVE → DEVELOPED PHOTO RESIST IMAGE ON COPPER CLAD CIRCUIT BOARD → ETCHED CIRCUIT BOARD
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from original art or a printed page.

KIT CONTAINS 5" x 6" steel printing frame 4 sheets 5" x 6" photocopy film, yellow filter, chemicals for 1 pint film developer and 1 pint film fixer, 5" x 6" copper clad board, 3" x 4 1/2" copper clad board, spray can of photo etch resist, 1 pint resist developer, 2 sheets 8 1/2" x 11" layout film, 1 roll 1/16" printed circuit tape, 1 roll 1/32" printed circuit tape, 8 sheets dry transfer direct etch PC patterns including pads, transistors, round can and flat pack ICs, DIP-ICs, edge card connectors, lines, circles, jogs, etc. 1/4 lb anhydrous ferric chloride to make 1 pint etchant, instructions.

ER-4 COMPLETE PHOTO ETCH SET \$26.95
ER-2 PC patterns and tapes—refill 3.95
ER-3 1/4 pound dry etchant—refill 1.49
ER-5 6 sheets photocopy film—refill 3.95
ER-6 Film process chemicals—refill 1.95
ER-7 Photo resist spray, 2.5 oz.—refill 2.95
ER-8 Resist developer, 16 oz. can—refill 2.95

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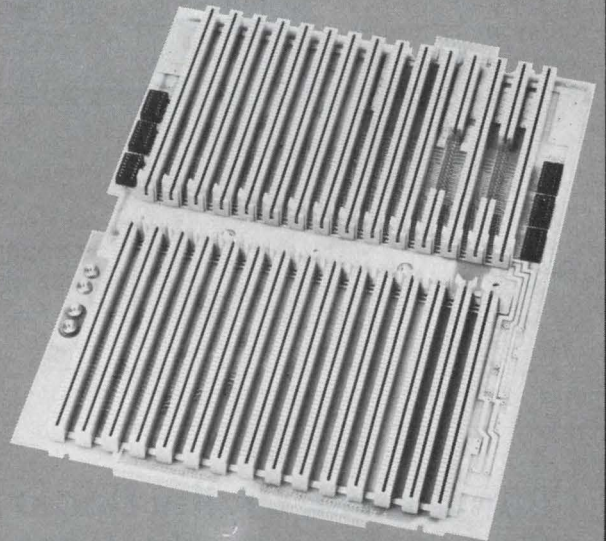
CIRCLE NUMBER 146

ELECTRONIC DESIGN 24, November 22, 1976

FABRI-PAKTM

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NATIONAL CONNECTOR DIVISION

9210 Science Ctr. Drive/Minneapolis, MN 55428/(612) 533-3533

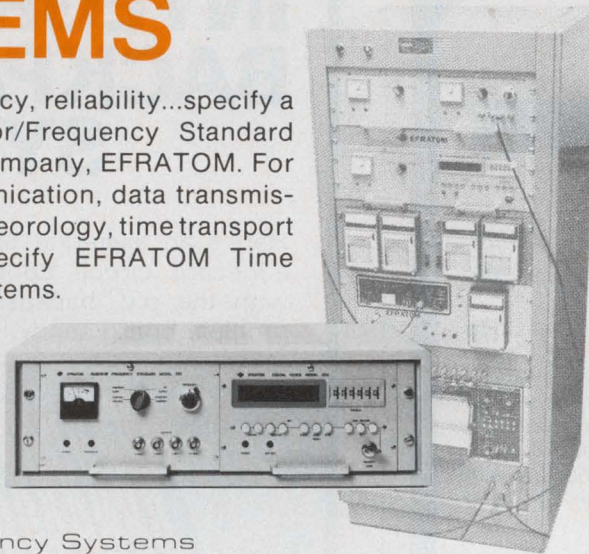
CIRCLE NUMBER 147

229

Rubidium TIME/FREQUENCY SYSTEMS

For stability, accuracy, reliability...specify a Rubidium Oscillator/Frequency Standard from the leading company, EFRATOM. For navigation, communication, data transmission, television, meteorology, time transport lab equipment...specify EFRATOM Time and Frequency Systems.

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3303 HARBOR BLVD., SUITE E1-E2
COSTA MESA, CALIFORNIA 92626
(714) 556-1620 • TWX 685-635

CIRCLE NUMBER 148

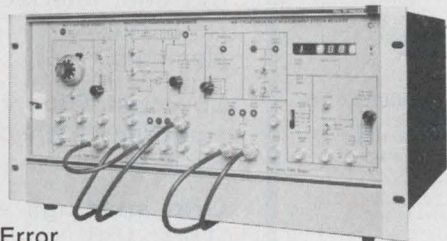
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TRANSMITTER . . . DC to 75 MHz. Six pseudo-random codes with frame sync and clock. RZ and NRZ formats. Encode/decode modes.

RECEIVER . . . Automatic synchronization to received code. Bit error rate, block error rate (10, 100, 1000 bits), burst error LED. Four-digit LED counter. Phase adjust and phase/amplitude LED indicators.

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INC

11 Esquire Road, North Billerica, Mass. 01862 Tel: (617) 667-3874

CIRCLE NUMBER 149

INTEGRATED CIRCUITS

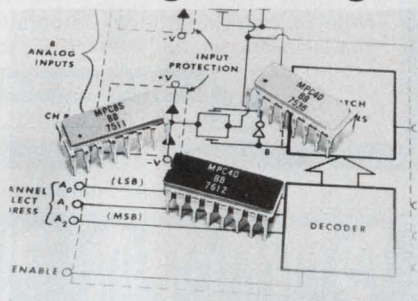
Low cost ARLS works with 75-ns clock

Fairchild Bipolar Memory, 464 Ellis St., Mountain View, CA 94042. (415) 962-3816. \$12 (100-up); stock.

An arithmetic logic register stack (ARLS), the 9405A, operates with a 75-ns clock period. It is claimed to be 30 ns faster than guaranteed operating times of the nearest competitive circuits. The 9405A has a two-address architecture, in which addresses are multiplexed to achieve cost advantages that make the circuit the industry's lowest priced four-bit slice, the company claims.

CIRCLE NO. 395

Analog multiplexers handle big overvoltages



Burr-Brown, International Airport Industrial Park, P.O. Box 11400, Tucson, AZ 85734. (602) 294-1431. \$10 (100-up); stock.

Monolithic analog multiplexers, the MPC4D and MPC8S, provide input overvoltage protection of up to 20 V above either supply. Channel interaction is eliminated during overvoltage conditions and also during power loss. In addition, the CMOS construction keeps the power dissipation to only 7.5 mW standby and 15 mW operating at 100 kHz. The MPC4D is a 4-channel differential input/output multiplexer and the MPC8S is a single-ended 8-channel device. Both units have access times of 500 ns typical, sampling rates to 200 kHz, and accuracies compatible with 12-bit converter systems. The multiplexers have break-before-make switching to protect input sources. Off-channel isolation is 65 dB typical. The supply range spans ± 5 to ± 20 V and the input/output range is equal to the supply voltage.

CIRCLE NO. 396

A/D and D/A Converters... Call the Can-Do Company



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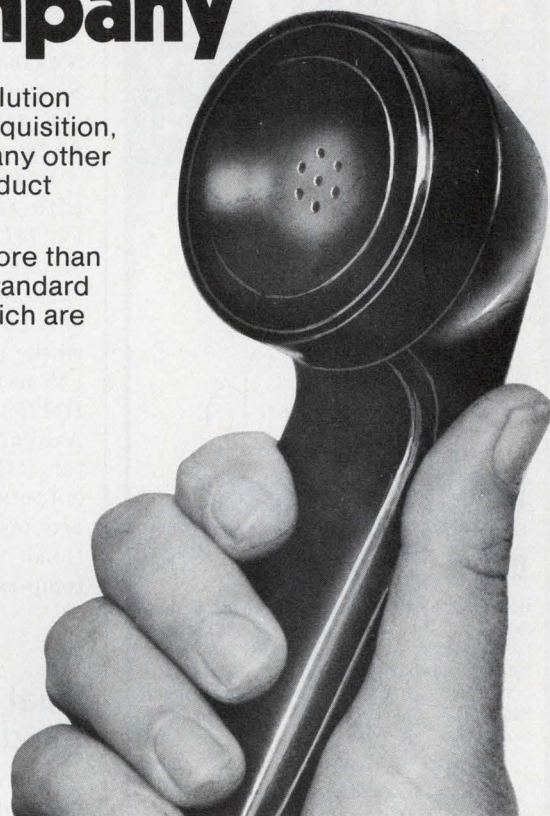
Mil-Spec needs. And we've solved a lot of engineering design problems that others tend to stay away from.

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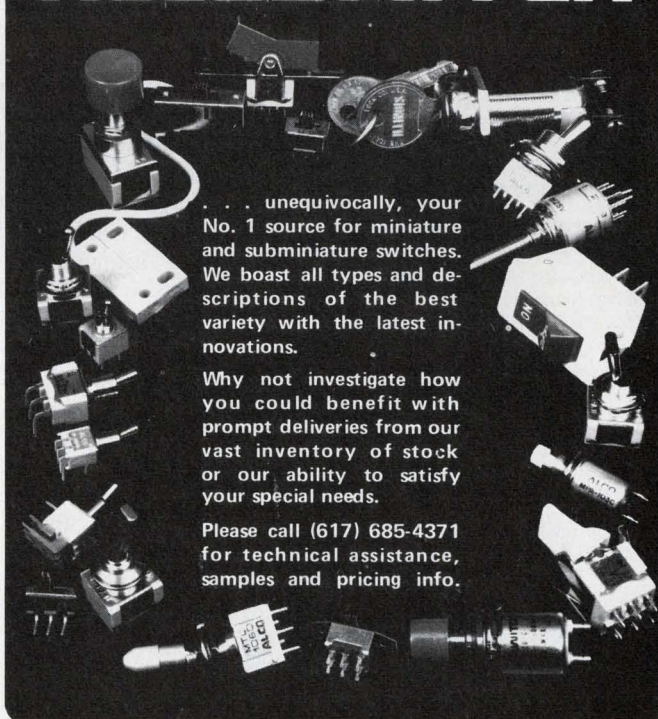
BODINE
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COMPANY

Bodine Electric Company, 2500 W. Bradley Place, Chicago, IL 60618.

CIRCLE NUMBER 151

ELECTRONIC DESIGN 24, November 22, 1976

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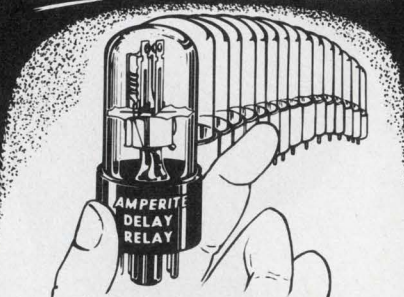
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CIRCLE NUMBER 152

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New! LONG DELAYS

240 & 300 Sec.

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Write for Bulletin No. LD-73.



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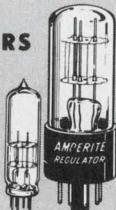
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Automatically keeps current and voltage at a definite value. For AC or DC... Hermetically sealed, rugged, vibration-resistant, compact, most inexpensive.

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Telephone: 201 UNION 4-9503

In Canada: Atlas Electronics, Ltd.,
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CIRCLE NUMBER 153

INTEGRATED CIRCUITS

Bipolar RAMs dissipate only 125 mW but are fast

National Semiconductor, 2900 Semiconductor Dr., Santa Clara, CA 95051. (408) 737-5832. From \$3.73 (100-up) stock.

Low-power bipolar memories with full military capabilities, the DM74LS289 and 74LS189, can handle 16 four-bit words. The random-access memories require only 25 mA maximum input current while maintaining the high speed (35 ns) of the older DM5489D and DM7599D, which they replace. Available with either open-collector (DM74LS289) or three-state outputs (DM74LS189), the RAMs are ideal for scratch-pad applications. Both commercial and MIL-temp-range versions are available.

CIRCLE NO. 397

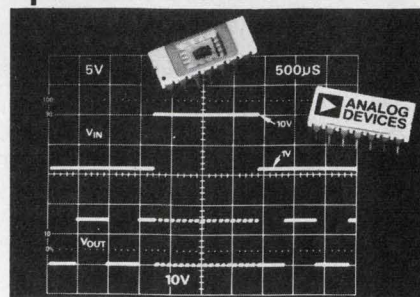
Dual memory drivers handle up to 600 mA

Fairchild Camera & Instrument, 464 Ellis St., Mountain View, CA 94042. (415) 962-3816. From \$2.62 (100-up); stock.

Dual memory drivers, the 55/75326 and 55/75327, can sink or source up to 600 mA and operate from a 5-V supply. The 55326 and 75326 can only sink 600 mA. Their output-transistor base current can be increased by connecting an external resistor. Each output collector is protected from voltage surges during inductive switching by a clamp diode in parallel with an internal pull-up resistor. The 55327 and 75327 memory switches can source or sink up to 600 mA, and operate from one 5-V supply and one 4.5-to-24-V supply. Each switch can function either as a sink driver or source driver. An internal base-drive resistor is available on the chip, and can be used by connecting two pins externally. All memory drivers are available in either ceramic DIPs (55326DM, 55327DM) or military flatpacks (55326FM, 55327FM) for operation over the military temperature range. For commercial use these circuits are available in both ceramic (75326DC, 75327DC) and plastic (75326PC, 75327PC) DIPs.

CIRCLE NO. 398

Monolithic v/f converter operates from 5 to 36 V



Analog Devices, Rte. 1 Industrial Park, P.O. Box 280, Norwood, MA 02062. (617) 329-4700. 100-up prices: \$9.50 (J), \$13.75 (K); \$19.50 (S); stock.

Able to operate from a single 5-to-36-V supply, the AD537 series of voltage-to-frequency converters have typical nonlinearity of 0.05% at 10 kHz. The single-chip converter requires only a single external RC network to set up any full-scale frequency up to 100 kHz and any full-scale input voltage up to +30 V. The converter maintains its linearity even down at low frequencies (0.001 Hz). Over-all tempo of the v/f converter is typically ± 30 ppm/ $^{\circ}\text{C}$. A temperature proportional output, scaled to 1 mV/ $^{\circ}\text{K}$, permits the AD537 to also be used as a temperature to frequency converter. The output of the v/f converter is a square wave that can drive up to 20 TTL loads. Quiescent-current drain of the AD537 is only 1.2 mA. On the input is a low drift ($1 \mu\text{V}/^{\circ}\text{C}$) amplifier that has a 250 M Ω input impedance. There are three versions of the 14-pin-DIP-housed unit: The AD537J, K and S. The J and K are specified for 0-to-70-C operation and the S for -55 to $+125$ C.

CIRCLE NO. 399

4-k static RAMs run from only a 5-V source

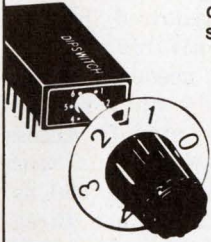
Electronic Memories & Magnetics Corp., 12621 Chadron Ave., Hawthorne, CA 90250. (213) 644-9881. \$15.10 (100-up); stock.

Two 4-k static RAMs, the 4801 and 4804, use only one 5-V power source. The devices are configured as $1 \text{ k} \times 4$ and $4 \text{ k} \times 1$, and both are housed in 18-pin packages. Typical device power at room temperature is 225 mW. Maximum access and cycle time is 450 ns, even at 70 C.

CIRCLE NO. 403

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CIRCLE NUMBER 154

• Uses Encoder MOS ROM • 7 "LED" test feature • 4 Modes

• 63-Key keyboard

Lowest price Keyboard and Encoder kit we've seen. General purpose ASCII keyboard for data terminal applications. Could be used for TV, RTTY, Code Transmission, Altair and other Mini Computers, etc. Utilizes 2-key rollover MOS memory allowing encoded outputs to be strobed out as each key is depressed. Uses double side pc board, Electronic shift lock, not mechanical on keyboard. Keyswitches, one integral assembly not individual keys. Keyboard: 63 keys (49 encoded keys). 4 mode: normal, shift and control. 3 internal function keys: shift, leach side of board, shift lock and control. 3 functions: Key Break, Here Is, Repeat. 7 additional functions (can be assigned by user).

Electrical specs: voltage requirements plus 5 volts and minus 12 volts, 200mw, negative or positive logic output, jumper selectable. Output connector. On the PC board we have a NEW KEYBOARD TEST FEATURE 7 LEDs! These LEDs display visually the ASCII code for the depressed key. TTL compatible. Kit includes: 63 key keyboard, pc board, ROM, 7 LEDs, resistors, capacitors, TTL IC's and SOCKETS. We include diagram and wiring instructions, ROM code. Wt. 3 lbs. Size overall: 13 x 5 1/2 x 2".

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• Double Outputs — standard sided ASCII 7 bits PC board plus strobe

• Bit 5 shifted

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PRECISION

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□ 50	□ 1K	□ 25K
□ 100	□ 2.0K	□ 50K
□ 200	□ 2.5K	□ 100K
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Fall-Winter CATALOG

CIRCLE NUMBER 155

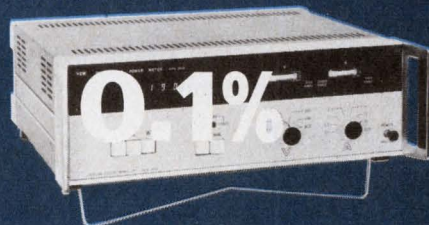
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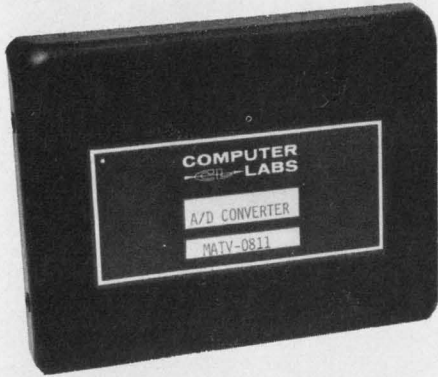
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CIRCLE NUMBER 156

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A perfect pair of A/D & D/A Converters for color TV digitization, time-base correction, and frame sync applications.

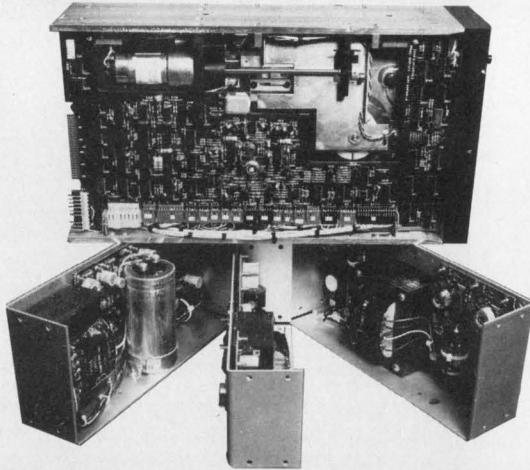
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CIRCLE NUMBER 158

INTEGRATED CIRCUITS

CMOS RAMs require only 50 nW/bit

American Microsystems, 3800 Homestead Rd., Santa Clara, CA 95051. (408) 246-0330. From \$15.25 (100-up); stock.

The S5101 family of CMOS RAMs is organized as 256×4 . Standby power required by the RAMs is only 50 nW/bit and only a +5-V supply is needed. The devices are completely static and require no refresh signal. Access time of the 5101s is 450 ns, with other versions available at 650 ns. Outputs of the RAMs are three-state. With the device deselected, current drawn is either 10 or 140 μ A, depending on the model. Units are available with guaranteed data retention at power-supply voltages as low as +2 V. The RAMs are housed in 22-pin plastic or ceramic DIPs.

CIRCLE NO. 404

8-bit registers have new package

Advanced Micro Devices, 901 Thompson Pl., Sunnyvale, CA 94086. (408) 732-2400. From \$4.30 (100-up); stock.

Three new high-speed low-power eight-bit registers come in a new 20-pin configuration. These low-power, serial-in/parallel-out universal shift-registers are available with either synchronous-or-asynchronous-clear modes and three-state outputs. The low-power Schottky devices (Am25LS23, Am25LS299 and Am154/74LS299) offer four modes of operation—hold (store), shift left, shift right and load data. The Am25LS23 has a synchronous clear function while the Am25LS299 has an asynchronous clear. Both devices have a typical shift frequency of 50 MHz. The Am54/74LS299—pin compatible with a like-numbered TI unit—is a reduced-performance version of the Am25LS299. All three circuits are available in molded and hermetic DIP packages, and are specified for operation over the commercial and military temperature ranges. They undergo 100-percent processing to the requirements of MIL-STD-883.

CIRCLE NO. 405

Big Little DMM

You get bench-size accuracy and performance with our new, hand held, 3½-digit VOM. It's in a class by itself.



- Highly readable, field-effect LCD
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CIRCLE NUMBER 159

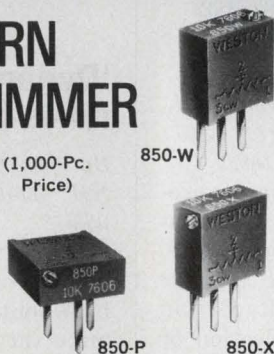
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CIRCLE NUMBER 160

ELECTRONIC DESIGN 24, November 22, 1976

ENGINEERS & DESIGNERS

Kearfott's success and stability offers a continuing pattern of growth—yours and ours!

KEARFOTT's long and continuing role as an innovator and leader in aerospace navigation and computer technology has never been more filled with promise than it is today.

Career opportunities are available for experienced engineers who can participate in advanced development work on challenging avionic projects such as F-16, MRAALS, Space Shuttle, TALONS and others. Our current backlog of assignments offers excellent career advancement opportunities and long-term stability.

If you're seeking new challenges and steady growth with a highly successful organization, where your contributions are recognized, let's get together.

Immediate positions available in the following areas:

LOGIC DESIGNERS

Opportunities involving sequential, high-speed and I/O interface logic and microprocessor applications in digital, signal processing, communication and aerospace systems. Familiarity with MS1/LS1 desirable. Requires several years experience in progressively more challenging logic design. BS/MSEE.

MAGNETIC MEMORY DESIGN ENGINEER

Needs extensive background in core memory organization, circuits and magnetics, and familiarity with logic design. Experience in the design of precise high current, high frequency digital circuits essential. BS/MSEE.

COMPUTER ENGINEER

Requires BS/MSEE and 10 years diversified experience in design & application of digital computers to airborne applications; customer liaison experience; ability to formulate responses to customer requirements as well as satisfactory execution of contractor requirements in a computer development program.

SIGNAL PROCESSING ENGINEERS

Involves analysis and design of Signal Processing-Digital Communications Equipment for avionics plus TDMA and ICNI applications. Requires BSEE degree, Master's preferred, plus 2-5 years experience in communications theory, digital filters, coding theory, signal processing techniques, A/J analysis, error correction, phase locked loops, and related digital and RF hardware design.

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Requires BS/MSEE and 2-5 years experience with the development of FORTRAN programs to simulate electronic systems for signal processing of RF, Baseband, noise, etc.

Additional openings for experienced, degreed engineers in the following areas:

- ANALOG CIRCUIT DESIGN
- COMPUTER SYSTEMS DESIGN
- AIRBORNE ELECTRONIC PACKAGING
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Please forward resume specifying position for which you are applying, and include salary requirements, to: **D. DeGennaro, Singer Co., 1150 McBride Avenue, Little Falls, New Jersey 07424.**

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CIRCLE NUMBER 161

MILITARY
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Accuracy

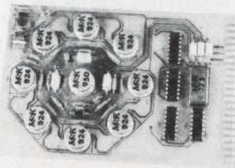
Speed

Size

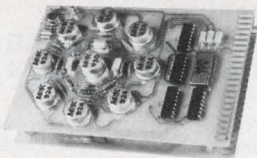
Repairability

Military

Temp. Range
-55°C to +125°C



- 4 Bit/50 nSec; Low Cost
- Ideal for Radar Scan Converters
- Holds Absolute Accuracy Over Temperatures
- Tracks a 10 MHz Analog Input



- 9 Bit/200 nSec.
- < 2 Bit Drift Over Temperature
- Insensitive to Clock Frequency

For Further Information Call or Write
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Pickard Drive, Syracuse, New York 13211
Tel. 315-455-7077

CIRCLE NUMBER 162

POWER SOURCES

μP supplies in unit qty at high qty prices

Deltron Inc., Wissahickon Ave., North Wales, PA 19454. (215) 699-9261. \$77: MPS-1, \$88: MPS-2 (unit qty); stock.

The MPS Series μP power supplies are now UL recognized. Deltron's MPS series is interchangeable with Lambda's MPU series and sells for less than half the price. Two models are available: Model MPS-1 is rated 5 V dc at 3 A, 12 V dc at 0.6 A and 9 to 12 V dc at 0.6 A or 5 V dc at 0.38 A; Model MPS-2 is rated at 5 V dc at 7 A, 12 V dc at 1 A and 9 V dc at 1.2 A or 5 V dc at 0.75 A. Both units are mechanically interchangeable with other competitive units, and are covered by a full one-year warranty.

CIRCLE NO. 406

Module watches the input line

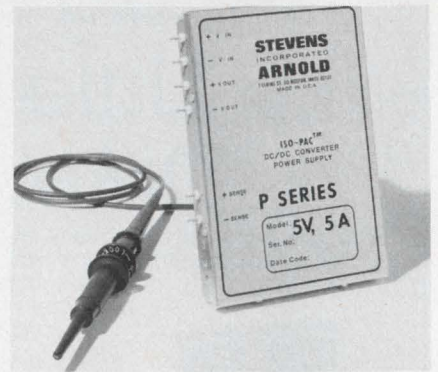


Calex Mfg., 3305 Vincent Rd., Pleasant Hill, CA 94523. (415) 932-3911. \$49; stock to 2 wk.

The Model 829 Linesensor protects equipment against "brown-out" and overvoltage conditions. The module monitors the average value of an ac line voltage and provides a logic-level indication of the out-of-tolerance condition. Also, the unit is sensitive to sudden drops in line voltage. The nominal input is 115 V, 50 to 440 Hz. Other power sources are not needed—the module operates from the line voltage being monitored. Its comparator output is isolated from the input by means of a phototransistor (Model 829T) or by a set of relay contacts (Model 829R).

CIRCLE NO. 407

Dc/dc converter outputs regulated to 0.2%



Stevens-Arnold Inc., 7 Elkins St., South Boston, MA 02127. (617) 268-1170. \$160.00 (1-9); stock to 6 wks.

Single-output 25-W low-noise isolated and regulated dc/dc converter modules, the P Series, accepts input levels of 12, 24 or 48 V dc and supplies dc outputs of 5 V, 5 A; 6 V, 4 A; 8 V, 3 A; 12 V, 2 A; or 15 V, 1.6 A. Regulation is ±0.2% max. Output setting accuracy is typically ±0.5%; average voltage is ±0.01%/°C; and stability is ±0.05%/24 h. Sense leads are also provided for point-of-load regulation and the reduction of IR-voltage losses normally experienced when delivering amperes of load current. Power transfer efficiency is 65%; isolation is 1 × 10⁹ Ω min at 500 V dc min; wideband noise is 40 mV pk-pk over a 5-Hz-to-20-MHz bandwidth; and converter switching frequency is 20 kHz and inaudible.

CIRCLE NO. 408

'Dynamic Variac' fakes brownouts

Berman Corp., Box 1043, Nashua, NH 03060. (603) 888-1300. 2-3 wks.

Why would anybody want a power source that produces mini-brownouts on purpose? To determine the "ride-through" capability of your product, of course. The PLM103 will deliberately drop from one to 999 half-cycles of line power, if you simply set the desired number on thumbwheel switches. Both manual and automatic operation (0.3 to 5 Hz) are provided. When used in conjunction with the Model CT-50 current transformer, surge current values and waveforms can be measured.

CIRCLE NO. 409



Tenney finds 25 year old working Chamber!

Dick Wagner, Chief Engineer The Triplett Corporation, leading manufacturers of test instruments and panel meters, Bluffton, Ohio accepts contest prize from Bob Schiffman Executive Vice President of Tenney.

In 1951 Triplett ordered two chambers (models TH10 a humidity chamber and 12T-85200 a programmed -85°F chamber) both having mechanical refrigeration and both still in daily operation.

Proof positive of Tenney's quality, reliability and durability.

Shouldn't you also rely on the oldest and largest manufacturer of environmental equipment?



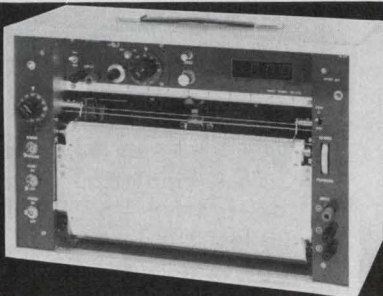
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747

CIRCLE NUMBER 163

MODEL SP-G11 SPEEDEX RECORDER

Model SP-G11 is equipped with a built-in A/D converter in addition to common analog recorder functions. Since output terminals are also provided. It can be readily used in computation and for connection to a printer or paper tape punch.



FEATURES

1. Digital output terminal (10-bit binary or 3-digit BCD)
2. External clock terminal permits chart drive by external clock.

SPECIFICATIONS

1. Chart width 250mm
2. Pen speed 0.8 secs full scale
3. Measurement voltage 0.5, 1, 5, 10, 50, 100, 500mV, 1, 5, 10, 50, 100V full scale
4. Chart speed 10, 20, 50, 100, 300, 600mm/hr
20, 50, 100, 300, 600mm/min
5. Digital output (A or B) A...10-bit binary full scale at 1000 digit.
1 digit 0.1%
B...3-digits BCD $10^2 10^1 10^0$ full scale 999

Please write us on your letterhead for detailed information.

Riken Denshi Co., Ltd.

5-5-2, Yutenji, Meguro-ku, Tokyo, Japan.
TEL: 711-6656 TELEX: 0246-8107

CIRCLE NUMBER 164

ELECTRONIC DESIGN 24, November 22, 1976

Meet the "low cost" Bowmar TP-3120 Thermal Printer

Available off-the-shelf, the new Bowmar TP-3120 thermal printer does a lot more than many of the others for a lot less. With a speed of 1.07 lines per second, this quiet printer continues to maintain its economical advantage by using low-cost, high contrast, non-smear paper. Small in size and cost, yet big in capabilities, it's equipped with such Bowmar quality features as 12 position, dual read-out standard connector, right or left justification and 5x5 matrix design. Other highlights of the new Bowmar TP-3120 include:

- 18-Column Alpha/Numeric Printout
- 29.4 Characters Per Second
- Low Power Consumption
- MOS Compatible
- Immediate Delivery

So if you're looking for a better and less expensive way to meet your thermal print-out needs, just send us the completed coupon and we'll send you full and detailed information on Bowmar's new "low cost" TP-3120 thermal printer by return mail.



Please send me full information on Bowmar TP-3120 Thermal Printer.

Name _____

Company _____

Street _____

City _____

State _____ Zip _____

Mail to: Bowmar Instrument Corp.
Dept. ED, 8000 Bluffton Road
Fort Wayne, IN 46809



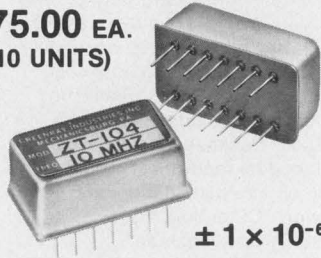
Bowmar

CIRCLE NUMBER 165

237

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\$75.00 EA.
(10 UNITS)



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MODEL ZT - 104
TTL COMPATIBLE
10 MHZ

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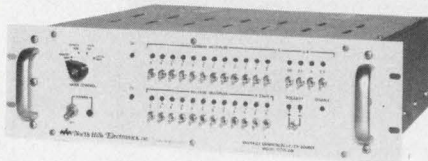
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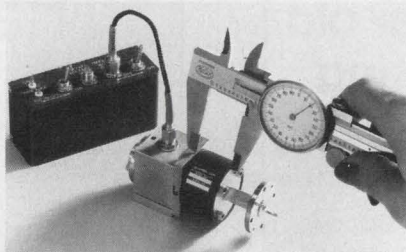
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CIRCLE NUMBER 167

MICROWAVES & LASERS

VCOs to replace reflex klystrons



Hughes Aircraft Co., Electron Dynamics Div., 3100 W. Lomita Blvd., Torrance, CA 90509. (213) 534-2121. \$1550 up; 30 days.

Voltage-controlled oscillators of the 414XXH series cover 26.5 to 110 GHz with up to 100 mW at the lower, 50 mW at the higher frequencies. The Impatt oscillators perform comparably to reflex klystrons, with the advantages of smaller size and lower voltages. Longer life is also claimed. Inputs range from 20 to 50 V dc at 500 mA max, the tuning voltage for 100-MHz deviation is 0 to 10 V. Six frequency ranges are available: Ka, Q, U, V, E and W-band. In addition to the cavity-mounted Impatt diode, the units are supplied with in integrated isolator, attached regulator, and heat-sink stand.

CIRCLE NO. 410

Broadband isolators span 2 to 8 GHz

Western Microwaves, 1260 Birchwood Dr., Sunnyvale, CA 94086. (408) 734-1631. \$450 (1 to 9); 30 days.

Covering a frequency range of 2 to 8 GHz, the PMI-2280 series of broadband isolators can handle loads of up to 10 W cw. There are three models available: one unit spans 2 to 2.2 GHz; the next, 2.2 to 6 GHz; and the last, 6 to 8 GHz. Isolation losses are 20 dB for the first two models and 17 dB for the last unit. Insertion losses are 1.25, 1.1 and 1.3 dB, respectively, and the VSWR stays at 1.3:1 for all three models. All isolators have an operating range of 0 to 55 C and measure $3.23 \times 2.08 \times 1.08$ in. (excluding connectors, which are SMA female).

CIRCLE NO. 411

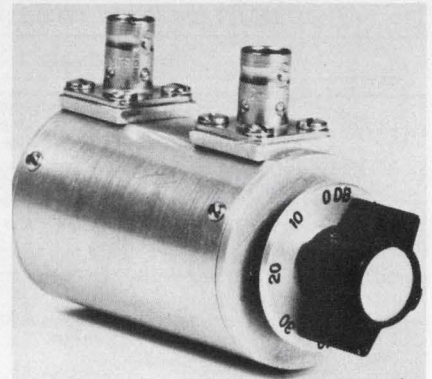
Bandpass filters use YIG tuning at 20 MHz/mA

Syston-Donner, Advanced Components Div., 735 Palomar Dr., Sunnyvale, CA 94086. (408) 735-9660. From \$700 to \$1200; stock.

YIG-tuned reciprocal bandpass filters are available in two, three, four, or dual two-stage versions. The SDYF-4000 series covers seven frequency bands from 0.5 through 26.5 GHz. Typical characteristics include an insertion loss of 1 dB (or less) per stage, basic 3-dB bandwidth varying from 3% at 500 MHz to 0.3% at 18 GHz and a skirt selectivity of 6 dB/octave per stage. Typical tuning sensitivity is 20 MHz/mA, while the tuning rate is less than 10 ms/frequency band. Standard packages are 1.45 in. and 1.7 in. cubes, with a maximum weight of 9 and 17 oz, respectively.

CIRCLE NO. 412

Rotary attenuators span 2-GHz range



Kay Elemetrics, 12 Maple Ave., Pine Brook, NJ 07058. (201) 227-2000. \$109; 15 days.

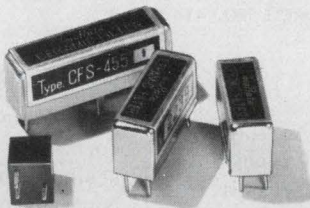
These miniature rotary attenuators provide VSWRs of less than 1.3 to 1 and insertion losses of less than 0.5 dB over a 2-GHz frequency range. Repeatability over time comes from the use of printed circuits and self-cleaning rotary-switch action. All units take 2.5 in. of panel depth and weigh less than 10 oz. Models 502A (50 Ω) and 530A (75- Ω) provide 0-to-70-dB attenuation in 10-dB steps. Models 500A (50 Ω) and 510A (75 Ω) provide up to 10-dB of switchable attenuation in 1-dB steps. Models 1/500A (50 Ω) and 1/510 (75 Ω) provide fine-decimal step-attenuation control.

CIRCLE NO. 413

selectivity you can count on!

Murata Piezoelectric I.F. Filters for Communication Systems.

Marine, Amateur, Public Service, Citizens Band . . . Murata has a miniature piezoelectric ceramic I.F. filter that can provide the long-term selectivity, stability and performance you need, even under the most adverse environmental conditions. Ladder filters, series resonators, interstage coupling filters in a variety of I.F. frequencies and with dozens of selectivity curves are included in the line. Write for our complete technical information package, today.

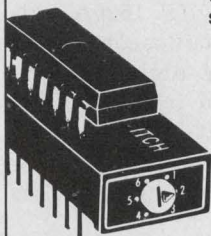


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CIRCLE NUMBER 168

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- 1 if savings board space is important, you can piggyback an IC right onto **DIPSWITCH**.
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- 3 if multilayered boards are part of your design, **DIPSWITCH**'s .230" profile is about half anybody else's. You can stack as close as 1/4".
- 4 if you need special switch closure programming, **DIPSWITCH**'s six independent cams can be factory assembled to perform your programming.

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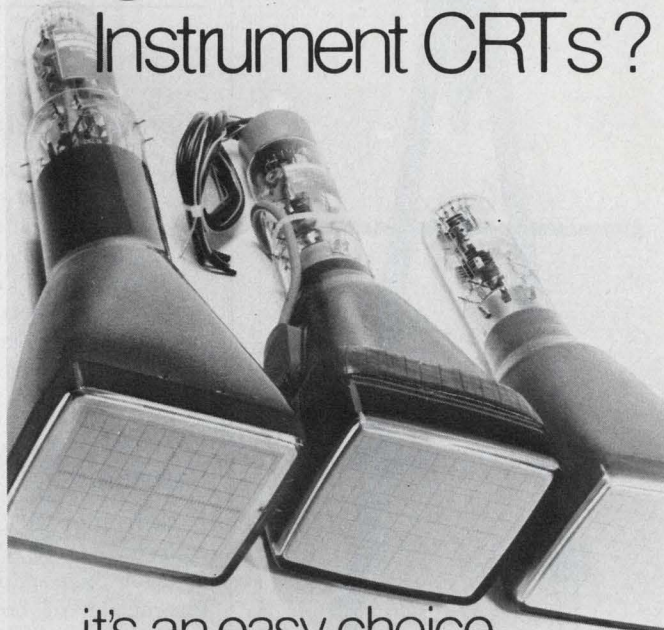


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CIRCLE NUMBER 169

ELECTRONIC DESIGN 24, November 22, 1976

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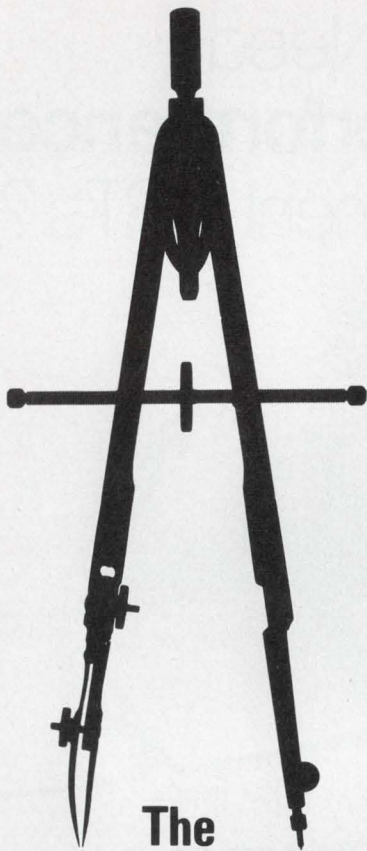
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CIRCLE NUMBER 170



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- To make diligent efforts to ensure the accuracy of editorial matter.
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- To encourage our readers as responsible members of our business community to report to us misleading or fraudulent advertising.
- To refuse any advertisement deemed to be misleading or fraudulent.

This statement of accuracy has appeared in every issue of *Electronic Design*, from the very first one. Staff members are imbued with it, from their very first day.

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Application Notes

Microwave detectors

The *Narda Probe* describes the physical properties of semiconductor diodes, their application in microwave detectors and typical characteristics and trade-offs required in selecting detectors for system and bench applications. Narda Microwave, Plainview, NY

CIRCLE NO. 414

Capacitors

"Effect of DC Life on the Discharge Life of Pulse Capacitors," a seven-page paper, discusses the interaction of both dc and pulsed conditions and the effect of different types of power supplies on capacitor life. Capacitor Specialists, Escondido, CA

CIRCLE NO. 415

Liquid-crystal displays

"Basic Guide to the New Liquid-Crystal Displays," a 20-pager, traces the development of liquid-crystal technology from 1888 to the present day. Advantages and disadvantages of field-effect LCDs vs dynamic scattering LCDs are discussed. Shelly Associates, Irvine, CA

CIRCLE NO. 416

Terminal blocks

How to select terminal blocks is covered in an eight-page brochure. Cogenel Inc./Entrelec Div., Elmsford, NY

CIRCLE NO. 417

Conversion counters

"New Digital Techniques Applied to Rate Measurement" describes recipromatic computation principle and basic operation of time-interval conversion counters and their applications. Orbit Controls, Cheltenham, Glos GL51 8PL, England.

CIRCLE NO. 418

GaAs FETs

New techniques of circuit design and device handling required when designing with gallium-arsenide field-effect transistors at microwave frequencies are covered in a 12-page brochure. Plessey Microsystems, Irvine, CA

CIRCLE NO. 419

Op amp parameters

Three application bulletins detail op-amp, log-amp and power-supply parameters and their measurements. Teledyne Philbrick, Dedham, MA

CIRCLE NO. 420

Uhf amplifiers

Designs for four high-performance uhf amplifiers are described in a paper. The paper contains construction hints, photos of the circuits, schematics and parts list. Communications Transistor, San Carlos, CA

CIRCLE NO. 421

Filters

The effective use of filters in signal-processing systems is given in *The Application of Filters to Analog and Digital Signal Processing*, a 24-page handbook. Rockland Systems, West Nyack, NY

CIRCLE NO. 422

Pattern analyzer

The use of the HP 1620A pattern analyzer in oscilloscope-based troubleshooting of digital instruments is described in an application note. Hewlett-Packard, Palo Alto, CA

CIRCLE NO. 423

Power amplifiers

"Add Power to your Network Analyzer," a four-page brochure, demonstrates how linear power amplifiers permit network analyzers to measure complex impedance of high-power components over the 100-MHz-to-12-GHz frequency range. Microwave Power Devices, Plainview, NY

CIRCLE NO. 424

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CIRCLE NUMBER 172

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- 200 to 12,000 RPM or FPM (up to 100,000 with harmonics)

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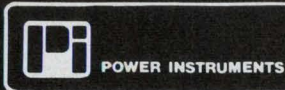
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CIRCLE NUMBER 173

ELECTRONIC DESIGN 24, November 22, 1976



FAST BASIC I begins where Hewlett-Packard left off.

FAST BASIC I is the most powerful general-purpose ROM ever developed for the HP 9830A/B.*

With 28 statements, commands and functions, it brings the machine language up to big system level.

Consider this. Array manipulations can now be executed **hundreds** of times faster than a '30 with a MAT ROM, and **thousands** of times faster than the basic machine. If your machine has mass memory, FAST BASIC I provides equally important system enhancements.

But don't take our word for it! Try this amazing ROM for yourself completely free of charge. Just mail the coupon and you will promptly receive FAST BASIC I for your own evaluation. After 30 days, if you do not want to purchase it, return it and you have no further obligation whatsoever. Otherwise remit \$675 (the full purchase price) and keep your '30 running **FAST BASIC**.

*a product of Hewlett-Packard.



Infotek Systems

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(213) 966-7431 • TWX 910-584-1812

Infotek Systems
P. O. Box 1436
Covina, CA 91722

ED

Please rush FAST BASIC I to me free of charge. If I do not want to purchase it after using it for 30 days, I will return it to you at your expense.

Name (Please Print) _____

Company _____

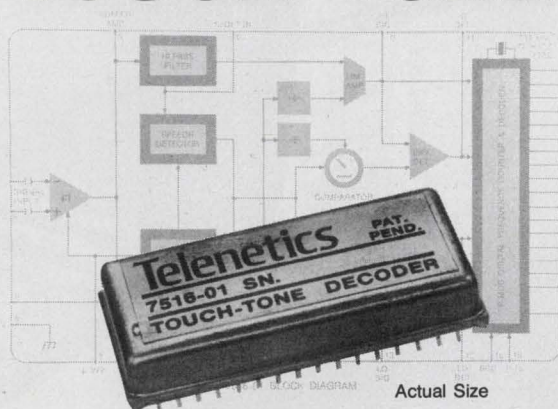
Address _____

City/State/Zip _____

Position _____ Serial No. _____
of my 9830 _____

CIRCLE NUMBER 174

TOUCH-TONE*



Telenetics' 7516-01 is a complete Touch-Tone Decoder in a 1/2 cubic inch, 32 pin DIP. Telephone Standard 2-of-8 tones are received, processed and decoded into discrete 1-of-16 or BCD (plus strobe) outputs. Input signal ranges -22 to +4 dBm with a balanced, capacitively coupled, 50 K Ω impedance. Operating voltage range is 8 to 28V dc (single supply); temperature range -30 to 70°C.

Telenetics 7516-01 gives you one-tenth the size at one-third the cost of comparable Touch-Tone Receivers. Telenetics also offers these other devices:

- 7603 Touch-Tone Encoders
- 7511 Address Selector
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LINEAR POWER AMPLIFIER 10-1000 MHz · 1 Watt



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*"... well-organized, extremely well written ...
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IEEE Transactions

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Samuel D. Stearns

This is an ideal master handbook on today's signal processing procedures and systems, containing recent advances, new design material, and a comparison between continual and digital systems that's extremely helpful to newcomers to the field. Featuring a foreword by Richard Hamming, the book contains a review of linear analysis; sample-data systems; analog-to-digital and digital-to-analog conversion; the discrete Fourier transform and the fast Fourier transform algorithm; spectral computations; non-recursive and recursive digital systems; computer simulation of continual systems; analog and digital filter designs, and more. 288 pages

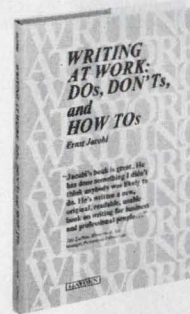
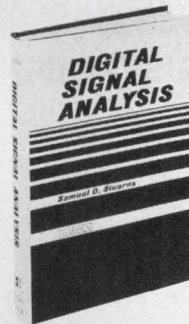
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Evaluation Samples

Temperature recorders

Miniature, self-contained $\pm 1\%$ accuracy temperature recorders are easily applied to electronic components and can be read at a glance. As each indicator is exposed to heat exceeding its calibrated temperature, it turns permanently and irreversibly black. Maximum thickness is 0.01 in. William Wahl Corp., Temp-Plate Div.

CIRCLE NO. 425

Lever handle

The J60 lever handle is an actuator option for many of C&K's subminiature switches. The support bracket provides a longer life-span for this switch option by virtually absorbing all of the actuation stress. C&K Components.

CIRCLE NO. 426

Heat sinks

Low-wattage aluminum semiconductor heat sinks are available in a sample kit. Aavid Engineering.

CIRCLE NO. 427

Synchro clamps

Synchro clamps are quick releasing, self-locking and instant nulling. The clamps' integral stops permit their position to be felt in the locked and unlocked positions. They lock and unlock simply with a half-turn of the screw. Timber-Top.

CIRCLE NO. 428

Metal bellows

Miniature metal bellows are used in a variety of industrial applications. Specifications and dimensions for the "Workhorse Bellows" are: O.D., 0.250 in.; I.D., 0.150 in.; wall thickness, 0.0012 in.; 22 active convolutions; spring rate of 3.3 lb/in.; compression capability of 0.179 in. and a pressure rating of 185 psi. Servometer.

CIRCLE NO. 429

Design Aids

Control panels

"Control Panel Layout Design Guide" discusses such design considerations as operator requirements, environmental considerations, manual controls, visual displays and maintainability, as well as the use of color in panel and control housing, coding and illumination. Micro Switch.

CIRCLE NO. 430

Washers

Flat, shoulder and finishing washers designed to be used with threaded and unthreaded fasteners as spacers, insulators, seats, shims, seals and bearings are listed on a wall chart. Sherman Metal Works.

CIRCLE NO. 431

Triacs and SCRs

A 32-page cross-reference guide indicates the RCA types recommended as replacements for more than 2100 triacs and silicon controlled rectifiers. RCA.

CIRCLE NO. 432

IC sockets

A fold-out easy-to-read selection chart shows each group of Cambion IC sockets. Detailed dimensional drawings as well as part numbers are included. Cambridge Thermionic.

CIRCLE NO. 433

Component parts

Nylon, acetal, polyester and phenolic parts for use in product assemblies are shown in a 16-page design guide. Sample parts are available. Security Plastics.

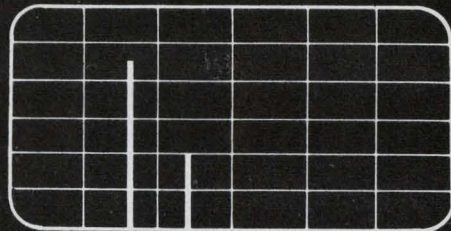
CIRCLE NO. 434

Relays

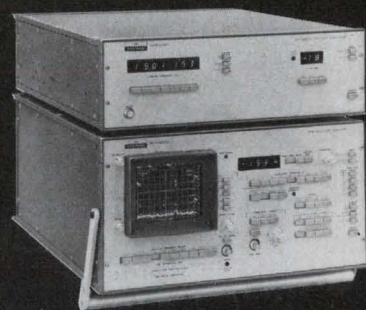
An 18-page relay selection guide provides an easy reference for selecting and specifying the right relay for a particular application. Arrow-M.

CIRCLE NO. 435

Q. How do you resolve two signals spaced 1 Hz apart at 2 MHz?



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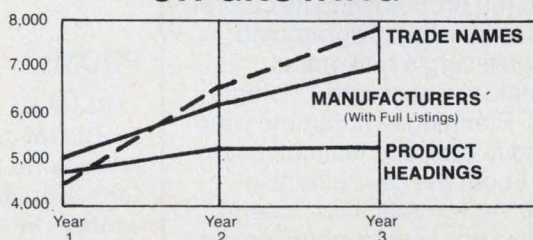
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CIRCLE NUMBER 179

New Literature

TIME DELAY RELAYS



Time-delay relays

A 28-page time-delay catalog includes application data, descriptions of delay functions, a glossary of terms and complete specifications, selection guide and dimensional drawings. Magnecraft Electric, Chicago, IL

CIRCLE NO. 436

Computing system

The 2200 portable computing system is described in a four-page brochure. The brochure discusses a variety of optional features and peripherals, and photos and specifications illustrate the capabilities of this system. Wang Laboratories, Tewksbury, MA

CIRCLE NO. 437

PROMs

Features that make TI's Schottky PROM family a low-cost, highly reliable, space-saving solution for system designers are described in a four-page brochure. Texas Instruments, Dallas, TX

CIRCLE NO. 438

Fluoropolymers

Properties and performance of Tefzel fluoropolymers as wire insulation are listed in a 12-page guide. Dupont, Wilmington, DE

CIRCLE NO. 439

Circular connectors

Standard circular connectors designed to MIL-C-5015 are highlighted in a 32-page brochure. ITT Cannon Electric, Santa Ana, CA

CIRCLE NO. 440

Switches

Photos, line drawings, specifications and ordering information on over 300 switches are contained in a 24-page catalog. Chicago Switch, Chicago, IL

CIRCLE NO. 441

Minicomputer

Complete specifications of the GA-16/440 16-bit systems and OEM minicomputer are detailed in a 24-page brochure. Hardware features and options are covered. General Automation, Anaheim, CA

CIRCLE NO. 442

Industrial switches

A well-illustrated, 256-page publication describes position sensing and manual switches designed for pilot duty industrial applications. The catalog is organized into three sections: no-touch position sensing controls; electromechanical position sensing switches and manually operated controls. Micro Switch, Freeport, IL

CIRCLE NO. 443

Security equipment

An informative 64-page guide to alarm equipment application includes alarm system discussion, installation procedures and detailed connection diagrams. Mountain West Alarm Supply, Phoenix, AZ

CIRCLE NO. 444

Linear circuit tester

Testing methods for a wide variety of op amps, comparators, voltage followers and regulators plus other linear ICs are described in a 10-page brochure. The tests are defined and illustrated in block diagrams. GenRad, Concord, MA

CIRCLE NO. 445

Rechargeable batteries

Rechargeable nickel-cadmium batteries are described in a 14-page Microprocessor Battery Selector Guide. The guide explains the phenomena of voltage depression—memory—and cell reversal. General Electric, Battery Dept., Gainesville, FL

CIRCLE NO. 446

Connectors

Circular electrical/electronic connectors are covered in a 32-page catalog. The catalog outlines 11 series of connectors and includes military specifications and configuration drawings as well as accessories. Malco, Montgomeryville, PA

CIRCLE NO. 447

Sealed relays

Engineering specifications, outline drawings and mounting information on sealed relays are provided in a 16-page catalog. Arrow-M, Mountainside, NJ

CIRCLE NO. 448

Transistors or chips

Npn small signal transistors or chips are described in a series of six data sheets. Sprague Electric, North Adams, MA

CIRCLE NO. 449

Programmable controllers

Photos, system descriptions and schematics highlight a 12-page programmable-controller catalog. Allen-Bradley, Cleveland, OH

CIRCLE NO. 450

Voltage regulators

A Voltage Regulator Handbook places special emphasis on design techniques. The handbook starts with the basics of power-supply design and covers transformer specification, rectifier circuits and how to specify them, filtering and load effects. To buy this handbook, send \$3 (CA residents add 6% sales tax) to the Marketing Services Dept., National Semiconductor, 2900 Semiconductor Dr., Santa Clara, CA 95051.

INQUIRE DIRECT

SCR power supplies

Specifications and pricing information on single and three-phase SCR power supplies, ranging from 50 to 10,000 W, are given in a 14-page catalog. Electronic Measurements, Neptune, NJ

CIRCLE NO. 451

μ P controller system

The EPTAK microprocessor controller system—designed for process control, machine control and other applications calling for advanced programmable control—is described in an eight-page brochure. Eagle Signal, Davenport, IA

CIRCLE NO. 452

Rental program

A new leasing/rental/installment purchase program offered by the 3M Industrial Electrical Products Div. is described in an eight-page brochure. 3M, St. Paul, MN

CIRCLE NO. 453

Ironless rotor dc motor

An illustrated bulletin shows the 9904 120 12601 series of 12-V-dc ironless rotor motors. A specification chart provides essential operating characteristics. North American Philips Controls, Cheshire, CT

CIRCLE NO. 454

μ C development system

A four-page brochure describes the Servant-8 microcomputer development system. Logical Services, Mountain View, CA

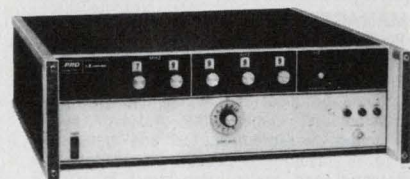
CIRCLE NO. 455

Data-conversion components

A 288-page engineering product handbook contains information on the following products: a/d and d/a converters, sample-holds, analog multiplexers, op amps, power supplies, dc-dc converters, DPMs, digital panel printers, digital panel instruments, data-logging instruments, data-acquisition systems and computer analog I/O systems. Datel Systems, Canton MA

CIRCLE NO. 456

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CIRCLE NUMBER 180

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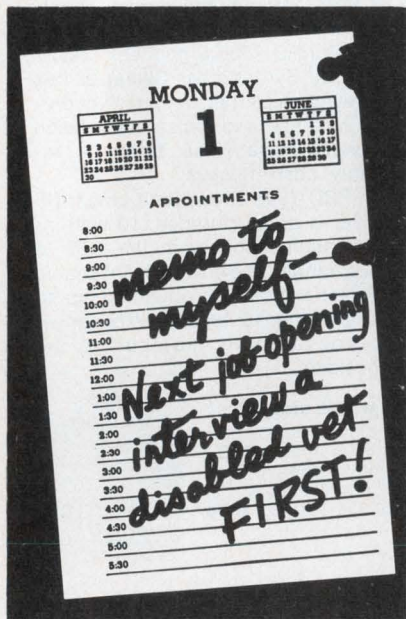
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Bulletin Board

Vishay now stocks its S102-type Bulk Metal precision resistors in all the standard values outlined by the MIL-R-55182 0.5% resistor tables. The resistors are available either immediately from stock or within 10 days at reduced prices.

CIRCLE NO. 457

Fairchild has set a new pricing range for its 5-V, logic-powered DPMs. Prices for the Model 32 3-1/2-digit meters are \$75 (1-49), \$71 (50-99), and \$67 (100-up). Pricing for the Model 42 4-1/2-digit meters are \$119, \$110 and \$99 for the same quantity ranges.

CIRCLE NO. 458

Intech/Function Modules has introduced the A-733J, a multiple-function mathematical module, which is a direct replacement for Analog Devices' 433J. The A-733J is priced at \$70 (1-24).

CIRCLE NO. 459

Biomation has reduced prices for its Model 810-D logic analyzer and 810-D accessories. The 810-D has been reduced from \$1995 to \$1495. Probes for the 810-D have been reduced to \$100.

CIRCLE NO. 460

Electro Corp. has redesigned its line of 5/8-in. thread magnetic sensors. The improvements include integral connector designs, improved magnetic efficiency, a uniform monolithic encapsulation method and fewer internal components.

CIRCLE NO. 461

Monolithic Systems has reduced the price on its fully hardware and software compatible PDP-11, including the 11/04, MONO-STORE® VII add-in memory system. Single quantity prices are \$795 for 4 k × 16, \$1075 for an 8 k × 16 and \$1350 for a 12 k × 16 system.

CIRCLE NO. 463

Vendors Report

Annual and interim reports can provide much more than financial position information. They often include the first public disclosure of new products, new techniques and new directions of our vendors and customers. Further, they often contain superb analyses of segments of industry that a company serves.

Selected companies with recent reports are listed here with their main electronic products or services. For a copy, circle the indicated number.

Indian Head. Utilities and communication products, metal and automotive products; containers and microfilm.

CIRCLE NO. 464

Milton Roy. Industrial and health-care products.

CIRCLE NO. 465

RCA. Electronic consumer products and services; broadcasting; communications; solid-state components; government business and R&D.

CIRCLE NO. 466

Hoffman Electronics. Airborne navigation systems; military and civilian communications systems and multimedia education systems.

CIRCLE NO. 467

Technicon. Automated instruments and systems for analysis of blood and serum.

CIRCLE NO. 468

Philip A. Hunt Chemical Corp. Chemicals used in image-forming processes.

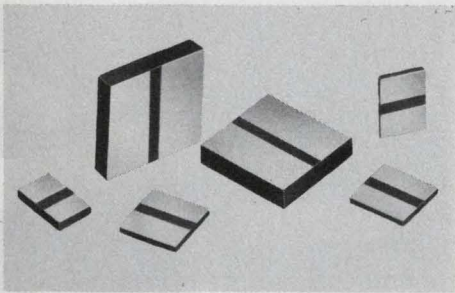
CIRCLE NO. 469

Dynascan. CB radios, precision test equipment and radio remote control systems.

CIRCLE NO. 470

Bliss & Laughlin Industries. Metal products.

CIRCLE NO. 471



CERAMIC CHIP CAPACITORS. SPLIT-CHIP, is a new concept in ceramic chip capacitor technology. These new units have two broad electrodes on one face and eliminate conventional wrap-around end terminations. This new concept provides lower cost and easier assembly. SPLIT-CHIPS are available in five standard sizes from .040" x .030" to .130" x .090" and .015" thick and in all popular dielectrics and capacitance ranges. **JOHANSON DIELECTRICS, INC.**, Box 6456, Burbank, Ca. 91510 213-848-4465

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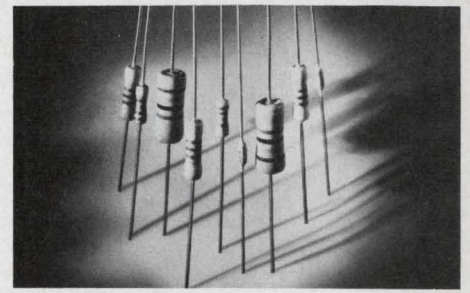
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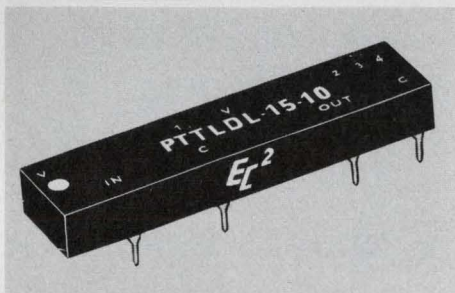
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RCA FLAMEPROOF FILM RESISTORS. Design engineers prefer them because they won't flame or short under the most severe conditions. These resistors have a 2% tolerance, and are available in 1/4 watt, 1/2 watt, 1 watt, and 2 watt ratings. Resistance values range from 10 Ohms to 1.5 Megohms, depending on wattage rating. 475 film resistors to choose from. **RCA Distributor & Special Products Division, Sales Promotion Services**, Cherry Hill, N. J. 08101.

FILM RESISTORS

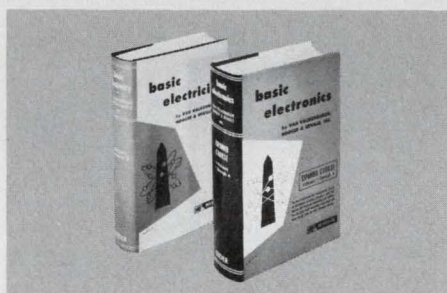
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EC²s new Digitally Programmable T²L Logic Delay lines feature Schottky T²L input and output; 15 models with time delays to a max of 255ns; 16 delay steps available with 1ns, 2ns, 3ns, 5 ns, 10 ns or 16ns resolution; propagation delays fully compensated; 32-pin dip package (.250 high); 4ns max rise time on all delays; 10 T²L fanout; programming by remote switching or automatically by computer-generated data. **Engineered Components Company**, P.O. Box Y, San Luis Obispo, Ca. 93406 (805) 544-3800

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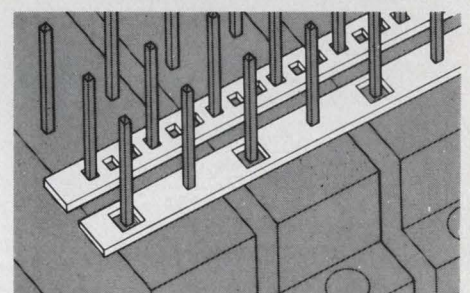
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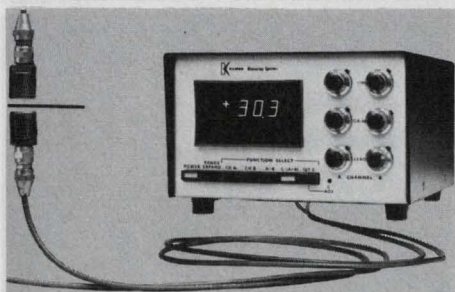
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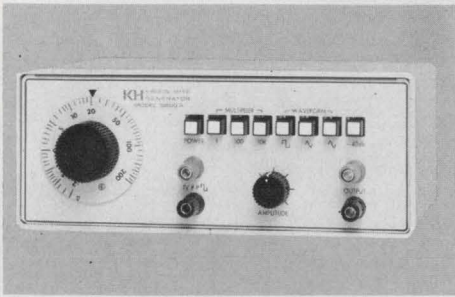
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MEMODYNE INCREMENTAL LOW POWER DATA LOGGER Model 2221, is ideal for remote or unattended collection of sporadic measurements. Features 16 channels, 0 to +10 volt analog input, 12 bit resolution, over 2 megabit capacity per 300 foot cassette. Standby current is less than 50 microamps. Available for line or battery operation. Unit price is \$1670.00. **Memodyne Corporation**, 385 Elliott Street, Newton Upper Falls, Massachusetts, 02164. (617) 527-6600.

LOW POWER DATA LOGGER

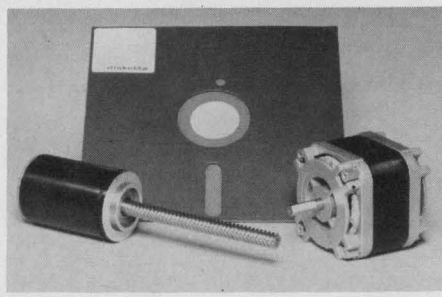
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Krohn-Hite Model 5800A function generator, budget priced at \$245, offers sine, square and triangle waveforms over a range of 0.2 Hz to 2 MHz. Distortion is typically less than 0.3%. Simple 1000:1 frequency tuning dial. Pushbutton controls. 50-ohm output adjustable from 5 mv pk-to-pk to 15 volts. Auxiliary 1-volt pk-to-pk square wave output. Stock delivery. KROHN-HITE, AVON INDUST. PARK, AVON, MA 02322

FUNCTION GENERATOR

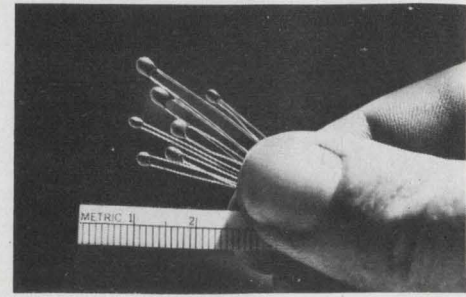
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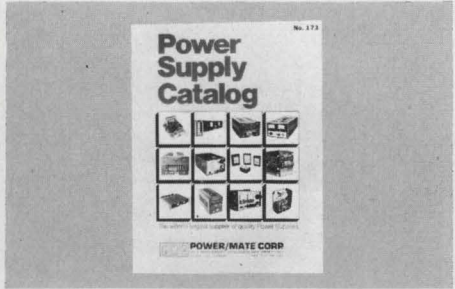
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Chip Thermistors with leads and coating are highly reliable, exceptionally predictable, low cost components with small and miniature dimensions more compatible with modern circuit design. R @ 25°C 30 ohms to 3 meg ohms, tolerances ± 10% to ± 1%. Curved matched interchangeables ± 1°C to ± .3°C. Point matched interchangeables for temperature control R, to ± 1%. **WESTERN THERMISTOR Corporation**, 403 Via El Centro, Oceanside, CA 92054. (714) 433-4484.

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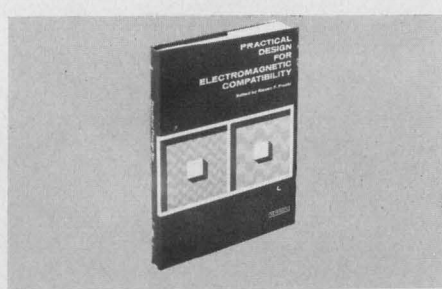
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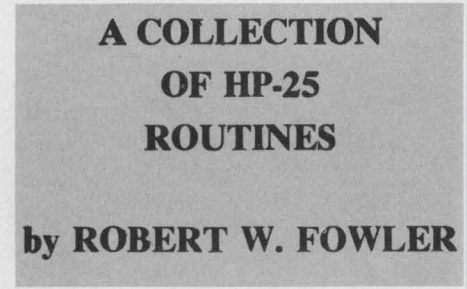
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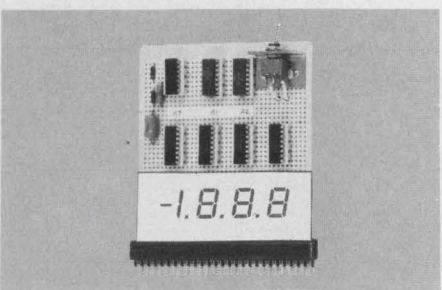
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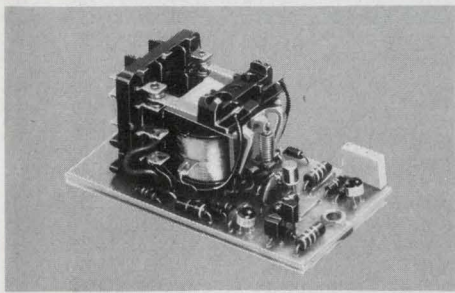
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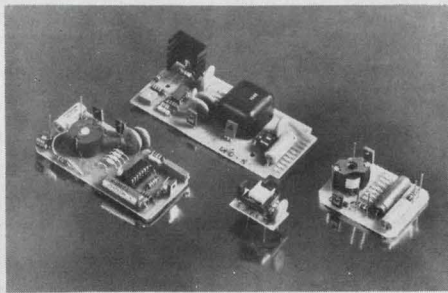
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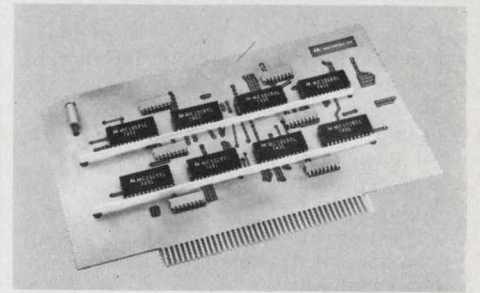
229



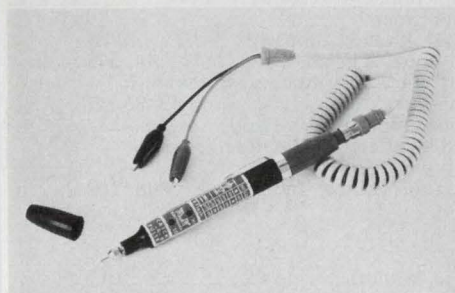
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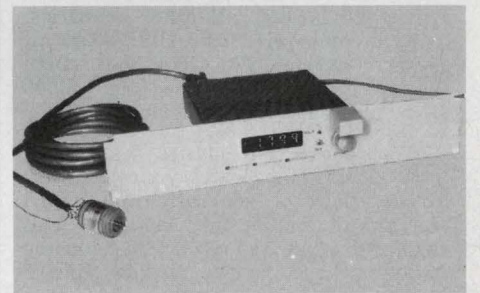
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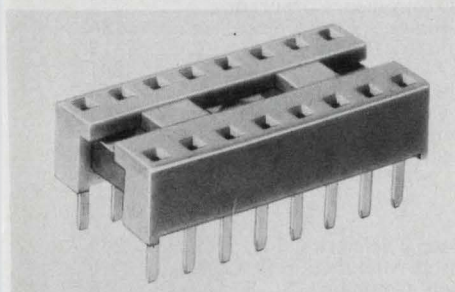
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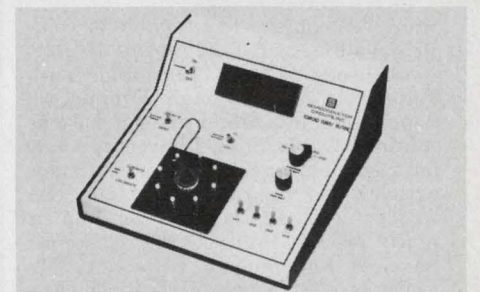
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Advertiser's Index

Advertiser	Page	Advertiser	Page
A P Products Incorporated.....	202	Edison Electronics, A McGraw Edison Company Division.....	233, 239
AMF, VID Electronics.....	225	Efratom California, Inc.....	230
AMP, Incorporated.....	74, 75	Electrocube Corp.....	222
AVR Electronics.....	251	Electronic Design ..144D, 180, 223, 256	
Accutronics, A Hammond Corporation Company.....	157	Electronic Molding Corporation.....	142
Acopian Corp.....	48C	Endicott Coil Co., Inc.....	251
Addison Division of Murihead Inc.....	226	Engineered Components Company.....	249
Advanced Micro Devices.....	193	Esterline Angus Instrument Corporation.....	227
Alco Electronic Products, Inc.....	231		
Allen Bradley Co.....	48A		
Amperite Co.....	232		
Analog Devices, Inc.....	150		
Arnold Magnetics Corp.....	200		
Arrow-M Corp.....	182		
B & K Products of Dynascan Corporation.....	144	Fabri-Tek, National Connector Division.....	229
BEI Electronics Inc.....	241	Fifth Dimension, Inc.....	228
Beckman Instruments, Inc. Helipot Division.....	15	Fowler, Robert.....	250
Belden Corporation.....	149	Frequency & Time Systems.....	190
Biomation.....	18, 19		
Bodine Electric Company.....	231		
Bourns, Inc., Trimpot Products Division.....	Cover II		
Bowmar Instrument Corporation.....	237		
Brown, W. A.....	128A-B		
Bud Radio, Inc.....	122, 123		
Bunker-Ramo, Amphenol Connector Division.....	Cover III		
Burr-Brown Research Corporation.....	185		
CPS, Inc.....	231	GTE Automatic Electric.....	177
Capital Calculator Company.....	216	General Electric Company, Semiconductor Products Department.....	39
CELCO (Constantine Engineering Laboratories Company).....	49	General Radio Company.....	144A
Cherry Electrical Products Corp.....	139	Gold Book, The.....	48H, 244, 245
Chrono-Log Corp.....	229	Gould Inc., Instruments Systems Division.....	81, 83, 85, 87
Computer Automation, Inc.....	16A-H	Greenray Industries, Inc.....	238
Computer Conversion Corp.....	251	Guardian Electric Manufacturing Company.....	48D
Computer Labs, Inc.....	234	Gulton Industries, Inc.....	208, 212
Computer Products, Inc.....	208		
Constantine Engineering Laboratories Company (CELCO).....	49		
Continental Specialties Corporation.....	128		
Control Data Corporation.....	40		
Dale Electronics, Inc.....	101	Hansen Manufacturing Co.....	103
Dana Laboratories, Inc.....	196	Harris PRD Electronics.....	246, 247
Data Display Products.....	28	Harris Semiconductor, A Division of Harris Corporation.....	188, 189
Data General Corporation.....	117	Harwil Co.....	249
Data I/O Corporation.....	17	Hayden Book Co., Inc.....	176A-B, 180, 181, 242, 249
Data Precision Corporation.....	24, 25	Heinemann Electric Company.....	119
Datak Corporation, The.....	229	Hewlett-Packard	65, 66, 67, 82, 94, 95
Datel Systems, Inc.....	46	Hoffman Engineering Company.....	221
Delco Electronics, Division of General Motors Corporation.....	158, 159	Houston Instruments, A Division of Bausch & Lomb.....	42
Dialight, A North American Philips Company.....	127	Hughes Aircraft Company, Connecting Devices.....	41
Digital Broadcast Systems.....	48B		
Digital Equipment Corporation.....	8, 9		
DuMont Electronics Corporation.....	239		
ECD Corp.....	120	ISE Electronics Corporation.....	215
EECO.....	23	ITT Pomona Electronics.....	186
EMI Technology.....	93	Illuminated Products Co.....	7
EMR Telemetry, Weston Instruments, Inc.....	243	Infotek Systems.....	241
Eastern Air Devices.....	250	Instrumentation Survey Card.....	112A-B
		Intel Corporation.....	4, 5, 32A-F
		Instrument Specialties Company.....	179
		Intertec Data Systems.....	34
		Johanson Dielectrics, Inc.....	249
		Johanson Manufacturing Corp.....	6
		Johnson Company, E. F.....	16
		Kaman Sciences Corp.....	249
		Keithley Instruments, Inc.....	58, 59
		Kennedy Corporation, M. S.....	236
		Keystone Carbon Company.....	220
		Krohn-Hite Corporation.....	250
		Leader Instruments Corp.....	226

Advertiser Page

Licon, Division of Illinois Tool Works, Inc.143

3M Company 48
 Mallory Capacitor Company.....199
 Marathon Battery Company.....210
 Marconi Instruments 10
 Memodyne Corporation249
 Mepeco/Electra, Inc.174, 175
 Micro Devices Corp.....223
 Microdata Corporation206, 207
 Micropac Industries, Inc.....225
 Microswitch, A Division of Honeywell121
 Mini-Circuits Laboratory, A Division of Scientific Components Corp. 2
 *Molex, Incorporated208B-C
 Monsanto Company 43
 Motorola Semiconductor Products, Inc.26, 27, 44, 45
 MuRata Corporation of America225, 239

NEC Microcomputers, Inc.....12,13
 Nichicon America Corporation.....102
 Nicolet Instrument Corporation109, 110, 111, 112
 North American Philips Controls Corp.198
 North Hills Electronics Inc.....238
 Nuclitudes242

Oak Industries, Inc.....217

PPG Industries, Inc.....187
 PSG Industries, Inc.....227
 *Philips Electronic Components and Materials 10
 *Philips Industries208D
 Philips Test & Measuring Instruments, Inc. 14
 Plessey Semiconductors ...*12, *13, 151
 Poly Paks Inc.....233
 Potter & Brumfield, Division of AMF, Incorporated173, 251
 Power Instruments241
 Power/Mate Corp.250
 Power One, Inc.....234
 Precision Monolithics, Incorporated.....171
 Pyrofilm Corporation138

RCA Distributor & Special Products Division, Sales Promotion Services.....249
 RCA Electro Optics.....145
 RCA Solid State.....Cover IV
 RCL Electronics, Inc.....11
 R. F. Power Labs, Inc.218
 Raytheon Company, Submarine Signal Division204
 Raytheon Semiconductor213
 Rental Electronics, Inc.48G
 Reticon203
 *Rifa of Sweden 14
 Riken Denshi Co., Ltd.....237

Advertiser Page

Robinson Nugent, Incorporated48H
 Rogan Corporation135
 Rogers Corporation249, 251

*SE Labs (EMI) Limited.....208A
 Samtec251
 *Schoeller & Co.....14
 Semiconductor Circuits, Inc.....251
 Semtech Corporation113
 Servo-Tek Products Company.....219
 Simpson Electric Company.....211
 Singer Company, The.....235
 Singer Company, Inc., Kearfott Division 84
 *Sodeco SAIA SA 15
 Sola Electric, Division of Sola Basic Industries134
 South Bay Cable Corp.....227
 Sprague Electric Company.....33
 Squires Electronics249
 Stacoswitch, A Staco Inc. Company.....202
 Standard Grigsby, Inc.....192
 Standard Condenser Corporation.....224
 Standard Power, Inc.....250
 Stanford Applied Engineering, Inc.129
 Stewart Warner Corporation.....197
 Syntronic Instruments, Inc.....191
 Systron-Donner32, 134

Tau-Tran, Inc.230
 Tecnetics, Inc.214
 Tektronix, Inc.20, 31
 Teledyne Philbrick 86
 Telenetics242
 Telonic Altair144C
 Tenney Engineering, Inc.....237
 Texscan Corporation195
 Textool Products, Inc.....209
 Thunder Scientific Corporation48E
 Triad/Utrad194
 Triplett Corporation169
 Turner Designs223

UCE250
 *U. S. Department of Commerce.....128D
 Unitrode Corporation201

Varo Semiconductor, Inc.166
 Viking Industries, Inc.37
 Viz Manufacturing Co.235

Wabash, Inc.167
 Wavetek San Diego, Inc. 1
 Western Thermistor Corporation250
 Weston Components235
 Weston Instruments, Inc.205
 Wintek Corporation250

Yokogawa Corporation of America*177, 233

Zivy & CIE SA, N.251

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Product Index

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Category	Page	IRN	Category	Page	IRN	Category	Page	IRN
Components			computing system (NL)	246	437	probes	184	324
CRT deflection yokes	49	35	controller, tape drive	220	377	pulse generator	196	338
CRT yokes	191	97	data set	216	368	pulse generators	82	42
CRTs	239	170	data transfer unit	220	378	recorder	237	164
capacitor	16	13	floppy-disc drive	40	28	recorder, strip-chart	42	30
capacitors (AN)	240	415	light sensors	216	369	scope	189	330
capacitors	6	5	memories	13	10	scope module	189	329
capacitors	102	51	memory, minicomputer	218	372	scope, storage	95	49
capacitors	222	131	minicomputer	220	380	scopes	226	140
capacitors	224	135	minicomputer (NL)	246	442	signal generator	186	326
capacitors, electrolytic	199	106	minis & micros	117	58	signal source	1	2
circuit breakers	119	59	numeric printers	208	117	spectrum analysis		
connectors (NL)	247	447	OEM peripherals	207	115	recorder	204	112
delay relays	232	153	paper tape reader	219	374	spectrum analyzer	243	177
filters	33	24	printer	220	379	stroboscope/tachometer	241	173
gearmotors	231	151	programmer, PROM	216	367	tester, telemetry bit	186	327
generator/reader	229	145	programmer, PROM	219	375	time/frequency systems	230	148
indicator lights	127	64	reader, bar code	218	373	timer/counters	14	282
industrial switches (NL)	246	443	terminal	34	25	wattmeters, portable	233	156
ironless rotor dc motor (NL)	247	454	terminals, data entry	216	370	word generator	184	325
logic switch	192	98	Discrete Semiconductors			Integrated Circuits		
motors	129	66	Darlingtons, high-voltage	159	81	converter, v/f	232	399
motors, gearmotors	219	128	diode chips	206	356	counter, eight-decade	228	391
posistors	227	141	LED lamps	208	359	drivers, memory	232	398
potentiometer	200	345	LED numerical displays	204	354	IC	234	405
potentiometer	202	347	rectifiers	204	350	ICs, interface	228	392
potentiometers	198	342	rectifiers	207	357	I ² L design kit	197	104
potentiometers	202	346	rectifiers	208	360	LSI	213	122
power transformers	194	100	rectifiers, Schottky-barrier	166	82	LSI	230	395
relays	228	144	regulators, voltage	207	358	memories bipolar	232	397
relays, amber	182	90	transistors, high voltage	204	355	memories, static	232	403
relays, time-delay	173	86	Instrumentation			multiplexers, CMOS	230	396
resistor DIPs	138	70	amplifier	196	339	PROMs	188	95
resistor networks	11	262	backplane test systems	226	139	PROMs (NL)	246	438
resistors, wire-wound	101	353	chart recorder, mini	183	321	prescalers	167	83
rotary switch	239	169	contact chatter checker	196	340	RAMs	193	99
steppers, PM	198	105	counter	183	320	RAMs, CMOS	234	404
switch	7	6	counters	192	335	reference voltage	171	85
switch, thumbwheel	23	17	DMM	144	74	regulators, voltage	228	393
switch, thumbwheel	198	341	DMM	189	331	tapped analog delay	203	111
switchers	27	20	DMM	190	333	timer, IC	228	394
switches	11	9	DMM	192	336	watch circuit, LED	228	390
switches	121	61	DMM	235	159	Microprocessor Design		
switches	202	109	DMM, portable	205	113	computer console	36	507
switches	231	152	DMMs	59	37	IC priority interrupt	36	508
switches, PB	143	73	DPM	184	322	microcomputer	35	506
switches, PB	200	344	DPMs	183	205	PROM eraser	223	132
switches, lighted	200	343	DPMs	211	120	PROM programmer	17	14
switches, rotary	217	126	DVM	196	103	software, 8080 μ P	38	510
switches, rotary	233	154	DVMs	32	23	time clock, μ P based	38	509
switches, thumbwheel	139	71	energy meter	184	304	μ C development system	5	286
thermal cutoffs	223	133	IC tester	192	334	μ P analyzer	134	67
thermistor assemblies	220	129	linear circuit tester (NL)	246	445	Microwaves & Lasers		
thermostats	227	143	logic analyzers	19	15	attenuators, rotary	238	413
transducer pressure	203	349	logic analyzers	184	323	filters, YIG-tuned	238	412
trimmers, cermet	235	160	logic card tester	189	328	isolators, broadband	238	411
trimmers, cermet	235	161	meter temp-pressure	190	332	oscillator, v.c.	238	410
XY positioner	203	348	multimeters	25	285	Modules & Subassemblies		
Data Processing			oscillograph, UV	194	337	a/d converter	212	472
acoustic coupler kit	219	376	oscilloscope, storage	31	289	alarm intrusion	212	473
CRT terminal	218	371	oscilloscope	109	56	amplifier	210	361
calculators	67	39	primary frequency			analog multiplexer	214	366
calculators	216	125	standard	190	96			
coaxial comm testing	230	149						
computers	16A-H	248						

Category	Page	IRN
comm. components	177	88
converter, a/d	236	162
converter, d/a	210	362
converter, dc-to-dc	214	123
converter, d/s	84	44
converters, f/v, v/f	86	46
converter, s/d	209	301
converters, a/d, d/a	234	157
data-conversion comp. (NL)	247	456
decoder	242	242
display interface	210	363
electro-optics	145	201
filters, i-f	239	168
freq. to voltage conv.	214	364
hybrid voltage regulators	225	137
LEDs	28	21
LEDs	43	31
modules	185	92
OEM servo recorder	227	142
op amp, HV	212	475
oscillators	157	79
oscillators	238	166
panel instruments	169	280
power amplifier	242	243
rf power amplifier	218	127
s/d converter	212	474
shaft encoder	241	172
surplus electronic equipment	233	155
thermal printer	237	165
touch tone encoder	214	365
Packaging & Materials		
backpanel system	229	147
backplane connections	48	34
beryllium-copper gaskets	179	89
breadboards, solderless	221	310
bushings	224	384
cable	225	138
cable assemblies	75	40
circuit evaluator	202	110
circular connectors (NL)	246	440
connections	41	29
connectors, thermocouple	222	381
digital micrometer	222	382
electronic glass	187	94
enclosure	221	130
enclosures	123	63
epoxy kit	224	387
fluoropolymers (NL)	246	439
kit, PC	229	146
knobs, dials	135	69
PC board	226	389
PC board connectors	37	26
PC card, wafer probe	224	386
packaging hardware	103	52
paper-like ceramic	222	383
socket card, DIP	224	385
socket, IC	226	388
sockets	128	65
sockets	142	72
test accessories	186	93
test chamber	237	163
wire, cable, cord	149	400

Category	Page	IRN
Power Sources		
converter, dc/dc	236	408
line voltage sensor	236	407
power conversion system	200	107
power line modifier	236	409
power sources	210	119
power supplies	134	68
power supplies	208	116
power supplies	234	158
power supplies, μ P	236	406
prog dc sources	238	167

new literature

circular connectors	246	440
computing system	246	437
connectors	247	447
data-conversion components	247	456
fluoropolymers	246	439
industrial switches	246	443
ironless-rotor dc motor	247	454
linear-circuit tester	246	445
minicomputer	246	442
PROMs	246	438
power supply catalog	15	12
programmable controllers	247	450
rechargeable batteries	247	446
rental program	247	453
SCR power supplies	247	451
sealed relays	247	448
security equipment	246	444
switches	246	441
time delay relays	246	436
transistors or chips	247	449
μ C development system	247	455
μ P controller system	247	452

application notes

capacitors	240	415
conversion counters	240	418
filters	240	422
GaAs FETs	240	419
liquid-crystal displays	240	416
microwave detectors	240	414
op-amp parameters	240	420
pattern analyzer	240	423
power amplifiers	240	424
terminal blocks	240	417
uhf amplifiers	240	421

design aids

component parts	243	434
control panels	243	430
IC sockets	243	433
relays	243	435
triacs and SCRs	243	432
washers	243	431

evaluation samples

heat sinks	243	427
lever handle	243	426
metal bellows	243	429
synchro clamps	243	428
temperature recorders	243	425

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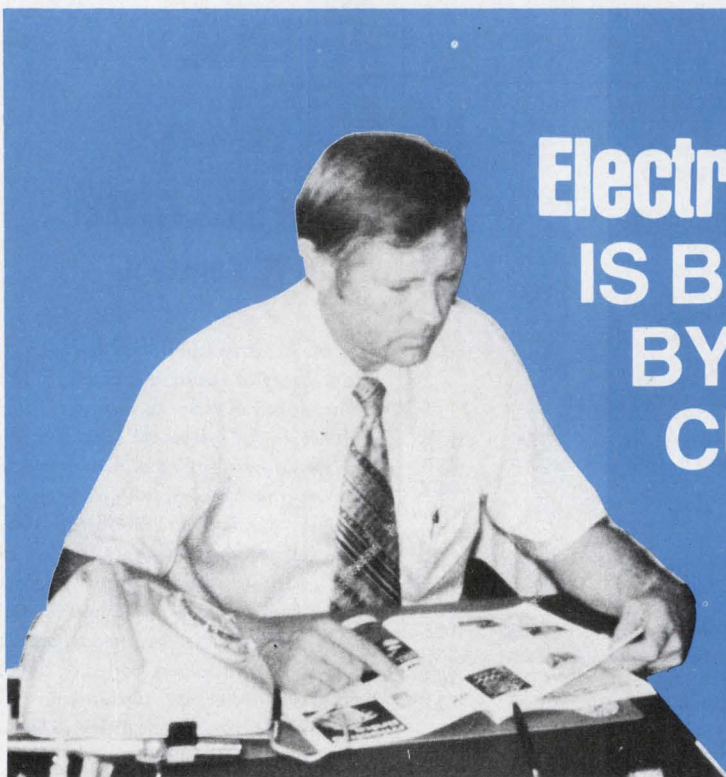


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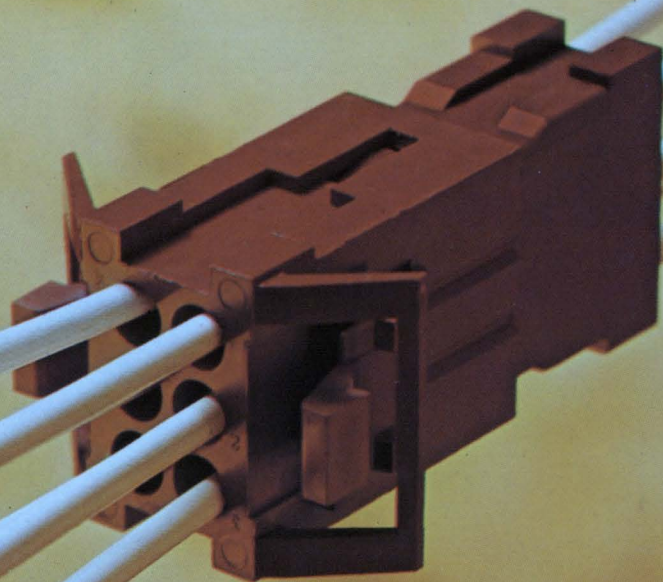
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